

**Total Maximum Daily Load of Sediment
in the Gwynns Falls Watershed,
Baltimore City and Baltimore County, Maryland**

FINAL



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Table of Contents

List of Figures i
List of Tables i
List of Abbreviations ii
EXECUTIVE SUMMARY iv
1.0 INTRODUCTION 1
2.0 SETTING AND WATER QUALITY DESCRIPTION 3
 2.1 General Setting 3
 2.1.1. Land Use..... 5
 2.2 Source Assessment 8
 2.2.1 Nonpoint Source Assessment 8
 2.2.2 Point Source Assessment..... 12
 2.2.3 Summary of Baseline Loads..... 13
 2.3 Water Quality Characterization 15
 2.4 Water Quality Impairment 19
3.0 TARGETED WATER QUALITY GOAL 21
4.0 TOTAL MAXIMUM DAILY LOADS AND SOURCE ALLOCATION..... 22
 4.1 Overview..... 22
 4.2 Analysis Framework 22
 4.3 Scenario Descriptions and Results..... 26
 4.4 Critical Condition and Seasonality 27
 4.5 TMDL Loading Caps..... 27
 4.6 Load Allocations Between Point and Nonpoint Sources..... 28
 4.7 Margin of Safety 31
 4.8 Summary of Total Maximum Daily Loads..... 32
5.0 ASSURANCE OF IMPLEMENTATION 33
REFERENCES 35
APPENDIX A – Watershed Characterization Data.....A1
APPENDIX B – MDE Permit InformationB1
APPENDIX C – Technical Approach Used to Generate Maximum Daily LoadsC1

List of Figures

Figure 1: Location Map of the Gwynns Falls Watershed in Baltimore City and Baltimore County, Maryland 4
Figure 2: Land Use of the Gwynns Falls Watershed 7
Figure 3: Percent Impervious vs. Percent Erosional Sediment Load Resultant from Streambank Erosion 12
Figure 4: Monitoring Stations in the Gwynns Falls Watershed 17
Figure 5: Gwynns Falls Watershed TMDL Segmentation 23
Figure C-1: Histogram of CBP River Segment Daily Simulation Results for the Gwynns Falls Watershed C5

List of Tables

Table ES-1: Gwynns Falls Baseline Sediment Loads (ton/yr) vi
Table ES-2 Gwynns Falls Average Annual TMDL of Sediment/Total Suspended Solids (ton/yr) vi
Table ES-3: Gwynns Falls Baseline Load, TMDL, and Total Reduction Percentage..... vii
Table 1: Land Use Percentage Distribution for the Gwynns Falls Watershed 6
Table 2: Summary of EOF Erosion Rate Calculations 9
Table 3: Gwynns Falls Baseline Sediment Loads (ton/yr) 13
Table 4: Detailed Baseline Sediment Budget Loads Within the Gwynns Falls Watershed 14
Table 5: Monitoring Stations in the Gwynns Falls Watershed 18
Table 6: Gwynns Falls Core/Trend Data 20
Table 7: Gwynns Falls Baseline Load and TMDL 28
Table 8: Gwynns Falls TMDL Reductions by Source Category 29
Table 9: Gwynns Falls TMDL Segment 1 Reductions by Source Category 29
Table 10: Gwynns Falls TMDL Segment 2 Reductions by Source Category 30
Table 11: Gwynns Falls Watershed Average Annual TMDL of Sediment/TSS (ton/yr) 32
Table 12: Gwynns Falls Maximum Daily Loads of Sediment/TSS (ton/day)..... 32
Table A-1: Reference Watersheds A1
Table B-1: Permit Summary B1
Table B-2: Municipal Permit Data..... B5
Table B-3: General Mine Permit Data B5
Table B-4: Stormwater Permits¹ B6

List of Abbreviations

| | |
|------------|--|
| BIBI | Benthic Index of Biotic Integrity |
| BIP | Buffer Incentive Program |
| BMP | Best Management Practices |
| BSID | Biological Stressor Identification |
| CBP P5 | Chesapeake Bay Program Phase 5 |
| CV | Coefficient of Variation |
| CWA | Clean Water Act |
| DNR | Maryland Department of Natural Resources |
| EOF | Edge-of-Field |
| EOS | Edge-of-Stream |
| EPA | Environmental Protection Agency |
| EPT | Ephemeroptera, Plecoptera, and Trichoptera |
| EPSC | Environmental Permit Service Center |
| ESD | Environmental Site Design |
| ETM | Enhanced Thematic Mapper |
| FDC | Flow Duration Curve |
| FIBI | Fish Index of Biologic Integrity |
| GIS | Geographic Information System |
| HSPF | Hydrological Simulation Program – FORTRAN |
| IBI | Index of Biotic Integrity |
| LA | Load Allocation |
| MAL | Minimum Allowable IBI Limit |
| MBSS | Maryland Biological Stream Survey |
| MD 8-Digit | Maryland 8-digit Watershed |
| MDE | Maryland Department of the Environment |
| MDL | Maximum Daily Load |
| MGD | Millions of Gallons per Day |
| mg/l | Milligrams per liter |
| MOS | Margin of Safety |
| MS4 | Municipal Separate Storm Sewer System |

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| | |
|--------|---|
| NPDES | National Pollutant Discharge Elimination System |
| NRCS | Natural Resource Conservation Service |
| NRI | Natural Resources Inventory |
| PCBs | Polychlorinated Biphenyls |
| PSU | Primary Sampling Unit |
| RESAC | Regional Earth Science Applications Center |
| TMDL | Total Maximum Daily Load |
| Ton/yr | Tons per Year |
| TSD | Technical Support Document |
| TSS | Total Suspended Solids |
| TM | Thematic Mapper |
| USGS | United States Geological Survey |
| WLA | Waste Load Allocation |
| WTP | Water Treatment Plant |
| WQA | Water Quality Analysis |
| WQIA | Water Quality Improvement Act |
| WQLS | Water Quality Limited Segment |
| WWTP | Wastewater Treatment Plant |

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EXECUTIVE SUMMARY

This document, upon approval by the U.S. Environmental Protection Agency (EPA), establishes a Total Maximum Daily Load (TMDL) for sediment in the Gwynns Falls watershed (basin number 02130905) (2008 *Integrated Report of Surface Water Quality in Maryland Assessment Unit ID: MD-02130905*). Section 303(d) of the federal Clean Water Act (CWA) and the EPA's implementing regulations direct each state to identify and list waters, known as water quality limited segments (WQLSs), in which current required controls of a specified substance are inadequate to achieve water quality standards. For each WQLS, the State is required to either establish a TMDL of the specified substance that the waterbody can receive without violating water quality standards, or demonstrate that water quality standards are being met (CFR 2008b).

The Maryland Department of the Environment (MDE) has identified the waters of the Gwynns Falls watershed on the State's 2008 Integrated Report as impaired by sediments (1996), nutrients – phosphorus (1996), bacteria (2002), and impacts to biological communities (2002) (MDE 2008). The designated uses of the Gwynns Falls mainstem and its tributaries is Use I (Water Contact Recreation, and Protection of Nontidal Warmwater Aquatic Life), except for the Gwynns Falls mainstem and its tributaries above Reisterstown Road and Red Run and its tributaries, which are designated as Use III (Nontidal Cold Water), and Dead Run and its tributaries, which are classified as Use IV (Recreational Trout Waters) (COMAR 2008a,b,c,d,e).

The TMDL established herein by MDE will address the 1996 sediments listing, for which a data solicitation was conducted, and all readily available data from the past five years have been considered. A TMDL for fecal bacteria was approved by the EPA in 2007, and a Water Quality Analysis (WQA) for nutrients to address the phosphorus listing is scheduled to be submitted to the EPA in 2009. The listing for impacts to biological communities will be refined in the 2010 Integrated Report's list of impaired waterbodies as a result of a stressor identification analysis.

The Gwynns Falls watershed aquatic health scores, consisting of the Benthic Index of Biotic Integrity (BIBI) and Fish Index of Biotic Integrity (FIBI), indicate that the biological metrics for the watershed exhibit a significant negative deviation from reference conditions based on Maryland's biocriteria listing methodology. The biocriteria listing methodology assesses the overall condition of Maryland's 8-digit (MD 8-digit) watersheds that have multiple sites with failing biological metrics by measuring the percentage of stream miles that are degraded, based on the BIBI and FIBI scores at these sites, and then calculating whether the percentage of degraded stream miles differs significantly from reference conditions (i.e., unimpaired watershed <10% stream miles degraded) (Roth et al. 2005; MDE 2008). The objective of the TMDL established herein is to ensure that there will be no sediment impacts affecting aquatic health, thereby establishing a sediment load that supports the Use I/III/IV designations for the Gwynns Falls watershed.

Currently in Maryland, there are no specific numeric criteria that quantify the impact of sediment on the aquatic health of nontidal stream systems. Therefore, to determine

FINAL

whether aquatic health is impacted by elevated sediment loads, MDE's recently developed *Biological Stressor Identification* (BSID) methodology was applied. The BSID identifies the most probable cause(s) for observed biological impairments throughout MD's 8-digit watersheds by ranking the likely stressors affecting a watershed using a suite of available physical, chemical, and land use data. The ranking of stressors was conducted via a risk-based, systematic, weight-of-evidence approach. The risk-based approach estimates the strength of association between various stressors and a degraded biological community. The BSID analysis then identifies individual stressors (pollutants) as probable or unlikely causes of the poor biological conditions within a given MD 8-digit watershed and subsequently concludes whether or not these individual stressors or groups of stressors are contributing to the impairment (MDE 2009a).

The BSID analysis for the Gwynns Falls watershed concludes that biological communities are likely impaired due to flow/sediment related stressors. Three individual stressors (channelization, channel alteration, and bar formation) that are associated with sediment related impacts and an altered hydrologic regime were identified as being probable causes of the biological impairment. Furthermore, the degradation of biological communities in the watershed is strongly associated with urban land use and its concomitant effects: altered hydrology, sediment related impacts, and elevated levels of sulfate, chlorides, and conductivity (a measure of the presence of dissolved substances) (MDE 2009b).

In order to quantify the impact of sediment on the aquatic health of non-tidal stream systems, a reference watershed TMDL approach was used and resulted in the establishment of a *sediment loading threshold* (Currey et al. 2006). This threshold is based on a detailed analysis of sediment loads from watersheds that are identified as supporting aquatic life (i.e., reference watersheds) based on Maryland's biocriteria (Roth et al. 1998, 2000; Stribling et al. 1998; MDE 2008). This threshold is then used to determine a watershed specific sediment TMDL.

The computational framework chosen for the Gwynns Falls watershed TMDL was the Chesapeake Bay Program Phase 5 (CBP P5) watershed model target *edge-of-field* (EOF) land use sediment loading rate calculations combined with a *sediment delivery ratio*. The *edge-of-stream* (EOS) sediment load is calculated per land use as a product of the land use area, land use target loading rate, and loss from the EOF to the main channel. The spatial domain of the CBP P5 watershed model segmentation aggregates to the MD 8-digit watersheds, which is consistent with the impairment listing.

EPA's regulations require TMDLs to take into account seasonality and critical conditions for stream flow, loading, and water quality parameters (CFR 2008b). The intent of this requirement is to ensure that the water quality of the waterbody is protected during times when it is most vulnerable. The biological monitoring data used to determine the reference watersheds integrates the stress effects over the course of time and thus inherently addresses critical conditions. Seasonality is captured in two components. First, it is implicitly included in biological sampling. Second, the Maryland Biological Stream

FINAL

Survey (MBSS) dataset included benthic sampling in the spring and fish sampling in the summer.

All TMDLs need to be presented as a sum of waste load allocations (WLAs) for point sources and load allocations (LAs) for nonpoint sources generated within the assessment unit, natural background, tributary, and adjacent segment loads. Furthermore, all TMDLs must include a margin of safety (MOS) to account for any lack of knowledge and uncertainty concerning the relationship between loads and water quality (CFR 2008a,b). It is proposed that the estimated variability around the reference watershed group used in this analysis already accounts for such uncertainty, and therefore the MOS is implicitly included.

The Gwynns Falls Total Baseline Sediment Load is 22,048.5 tons per year (ton/yr), which can be further subdivided into a nonpoint source baseline load (Nonpoint Source BL_{GF}) and two types of point source baseline loads: National Pollutant Discharge Elimination System (NPDES) regulated stormwater (NPDES Stormwater BL_{GF}) and regulated process water (Process Water BL_{GF}) (see Table ES-1).

Table ES-1: Gwynns Falls Baseline Sediment Loads (ton/yr)

| Total Baseline Load (ton/yr) | = | Nonpoint Source BL_{GF} | + | NPDES Stormwater BL_{GF} | + | Process Water BL_{GF} |
|---|---|---|---|--|---|---|
| 22,048.5 | = | 1,759.3 | + | 20,076.0 | + | 213.2 |

The Gwynns Falls Average Annual TMDL of Sediment/Total Suspended Solids (TSS) is 13,996.2 tons per year. The Load Allocation (LA_{GF}) is 1,759.3 tons per year, the NPDES Stormwater Waste Load Allocation (NPDES Stormwater WLA_{GF}) is 12,023.7 tons per year, and the Process Water Waste Load Allocation (Process Water WLA_{GF}) is 213.2 tons per year (see Table ES-2). This TMDL will ensure that the sediment loads and resulting effects are at a level to support the Use I/III/IV designations for the Gwynns Falls watershed, and more specifically, at a level the watershed can sustain without causing any sediment related impacts to aquatic health. The TMDL, however, will not completely resolve the impairment to biological communities within the watershed. Since the BSID watershed analysis identifies other possible stressors (i.e., chlorides, sulfate, conductivity) as impacting the biological conditions, this impairment remains to be fully addressed through the Integrated Report listing process and the TMDL development process, such that all impairing substances identified as impacting biological communities in the watershed are reduced to levels that will meet water quality standards, as established in future TMDLs for those substances (MDE 2009a).

Table ES-2 Gwynns Falls Average Annual TMDL of Sediment/Total Suspended Solids (ton/yr)

| TMDL (ton/yr) | = | LA_{GF} | + | NPDES Stormwater WLA_{GF} | + | Process Water WLA_{GF} | + | MOS |
|----------------------|---|-----------------------------|---|---|---|--|---|------------|
| 13,996.2 | = | 1,759.3 | + | 12,023.7 | + | 213.2 | + | Implicit |

Table ES-3: Gwynns Falls Baseline Load, TMDL, and Total Reduction Percentage

| Baseline Load (ton/yr) | TMDL (ton/yr) | Total Reduction (%) |
|-------------------------------|----------------------|----------------------------|
| 22,048.5 | 13,996.2 | 36.5 |

In addition to the TMDL value, a Maximum Daily Load (MDL) is also presented in this document. The calculation of the MDL, which is derived from the TMDL average annual loads, is explained in Appendix C and presented in Table C-1.

Once the EPA has approved this TMDL, and it is known what measures must be taken to reduce pollution levels, implementation of best management practices (BMPs) is expected to take place primarily via the municipal separate storm sewer system (MS4) permitting process for medium and large municipalities. MDE intends for the required reduction to be implemented in an iterative process that first addresses those sources with the largest impact to water quality, with consideration given to ease and cost of implementation.

Maryland has several well-established programs to draw upon, including the Water Quality Improvement Act of 1998 (WQIA) and the Federal Nonpoint Source Management Program (§ 319 of the Clean Water Act). Several potential funding sources available for local governments for implementation are available, such as the Buffer Incentive Program (BIP), the State Water Quality Revolving Loan Fund, and the Stormwater Pollution Cost Share Program.

FINAL

1.0 INTRODUCTION

This document, upon approval by the U.S. Environmental Protection Agency (EPA), establishes a Total Maximum Daily Load (TMDL) for sediment in the Gwynns Falls watershed (basin number 02130905) (2008 *Integrated Report of Surface Water Quality in Maryland* Assessment Unit ID: MD-02130905). Section 303(d)(1)(C) of the federal Clean Water Act (CWA) and the EPA's implementing regulations direct each state to develop a TMDL for each impaired water quality limited segment (WQLS) on the State's Integrated Report, taking into account seasonal variations, critical conditions, and a protective margin of safety (MOS) to account for uncertainty (CFR 2008b). A TMDL reflects the total pollutant loading of the impairing substance a waterbody can receive and still meet water quality standards.

TMDLs are established to determine the pollutant load reductions needed to achieve and maintain water quality standards. A water quality standard is the combination of a designated use for a particular body of water and the water quality criteria designed to protect that use. Designated uses include activities such as swimming, drinking water supply, protection of aquatic life, and shellfish propagation and harvest. Water quality criteria consist of narrative statements and numeric values designed to protect the designated uses. Criteria may differ among waters with different designated uses.

The Maryland Department of the Environment (MDE) has identified the waters of the Gwynns Falls watershed on the 2008 Integrated Report as impaired by sediments (1996), nutrients – phosphorus (1996), bacteria (2002), and impacts to biological communities (2002) (MDE 2008). The designated uses of the Gwynns Falls mainstem and its tributaries is Use I (Water Contact Recreation, and Protection of Nontidal Warmwater Aquatic Life), except for the Gwynns Falls mainstem and its tributaries above Reisterstown Road and Red Run and its tributaries, which are designated as Use III (Nontidal Cold Water), and Dead Run and its tributaries, which are classified as Use IV (Recreational Trout Waters) (COMAR 2008a,b,c,d,e).

The TMDL established herein by MDE will address the 1996 sediments listing, for which a data solicitation was conducted, and all readily available data from the past five years have been considered. A TMDL for fecal bacteria was approved by the EPA in 2007, and a Water Quality Analysis (WQA) for nutrients to address the phosphorus listing is scheduled to be submitted to the EPA in 2009. The listing for impacts to biological communities will be refined in the 2010 Integrated Report's list of impaired waterbodies as a result of a stressor identification analysis

The objective of the TMDL established herein is to ensure that there will be no sediment impacts affecting aquatic health, thereby establishing a sediment load that supports the Use I/III/IV designations for the Gwynns Falls watershed. Currently in Maryland, there are no specific numeric criteria that quantify the impact of sediment on the aquatic health of nontidal stream systems. Therefore, to determine whether aquatic health is impacted by elevated sediment loads, MDE's recently developed *Biological Stressor Identification* (BSID) methodology was applied.

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The BSID identifies the most probable cause(s) for observed biological impairments throughout Maryland's 8-digit (MD 8-digit) watersheds by ranking the likely stressors affecting a watershed using a suite of available physical, chemical, and land use data. The ranking of stressors was conducted via a risk-based, systematic, weight-of-evidence approach. The risk-based approach estimates the strength of association between various stressors and a degraded biological community. The BSID analysis then identifies individual stressors (pollutants) as probable or unlikely causes of the poor biological conditions within a given MD 8-digit watershed and subsequently concludes whether or not these individual stressors or groups of stressors are contributing to the impairment (MDE 2009a).

In order to quantify the impact of sediment on the aquatic health of non-tidal stream systems, a reference watershed TMDL approach was used and resulted in the establishment of a *sediment loading threshold* (Currey et al. 2006). This threshold is based on a detailed analysis of sediment loads from watersheds that are identified as supporting aquatic life (i.e., reference watersheds) based on Maryland's biocriteria (Roth et al. 1998, 2000; Stribling et al. 1998; MDE 2008). This threshold is then used to determine a watershed specific sediment TMDL.

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2.0 SETTING AND WATER QUALITY DESCRIPTION

2.1 General Setting

Location

The Gwynns Falls is a free flowing stream that originates in Baltimore County, Maryland and flows 25 miles in a southeasterly direction until it empties into the tidal Patapsco River. The watershed is located in the Patapsco River sub-basin of the Chesapeake Bay watershed within Baltimore County and Baltimore City, Maryland and covers approximately 65 square miles (see Figure 1). Five major tributaries of the Gwynns Falls, listed north to south, include: Red Run, Horsehead Branch, Scotts Level Branch, Dead Run, and Maidens Choice Creek. There is one “high quality”, or Tier II, stream segment (Benthic Index of Biotic Integrity (BIBI)/Fish Index of Biotic Integrity (FIBI) aquatic health scores > 4 (scale 1-5)), Red Run between the confluences of the stream’s 1st and 3rd unnamed tributaries, located within the watershed requiring the implementation of Maryland’s antidegradation policy. Also, approximately 0.4% of the watershed is covered by water (i.e., streams, ponds, etc.). The total population in the Gwynns Falls watershed is approximately 315,828 (MDE 2007b).

Geology/Soils

The Gwynns Falls watershed lies within the Piedmont and Atlantic Coastal Plain Geologic Provinces of Central Maryland. The Piedmont Province is characterized by a gentle to steep rolling topography, low hills, and ridges (DNR 2008; MGS 2008; MDE 2000). The surface geology is characterized by crystalline rocks, originally of sedimentary origin that were later transformed via heating into metamorphic rocks, consisting primarily of schist and gneiss. These formations are resistant to short term erosion and often determine the limits of the stream bank and streambed. The formations decrease in elevation from northwest to southeast and eventually extend beneath the younger sediments of the Coastal Plain. The fall line represents the transition between the Atlantic Coastal Plain Province and the Piedmont Province. The Atlantic Coastal Plain surface geology is characterized by thick, unconsolidated marine sediments deposited over the crystalline rock of the piedmont province. The deposits include clays, silts, sands, and gravels. In the areas around the head of tide, the topography is flat, with elevations below 100 feet. The elevations steadily increase going north to approximately 600 feet in the headwaters. Streambeds throughout the basin are comprised of rock and rubble with gradually sloped stream banks (CES 1995). The Gwynns Falls watershed lies predominantly in the Manor-Glenelg soil association in the upper Baltimore County portion of the watershed and the Legore-Aldino-Neshaminy soil association in the lower Baltimore County portion of the watershed (USDA 1977, 1998).

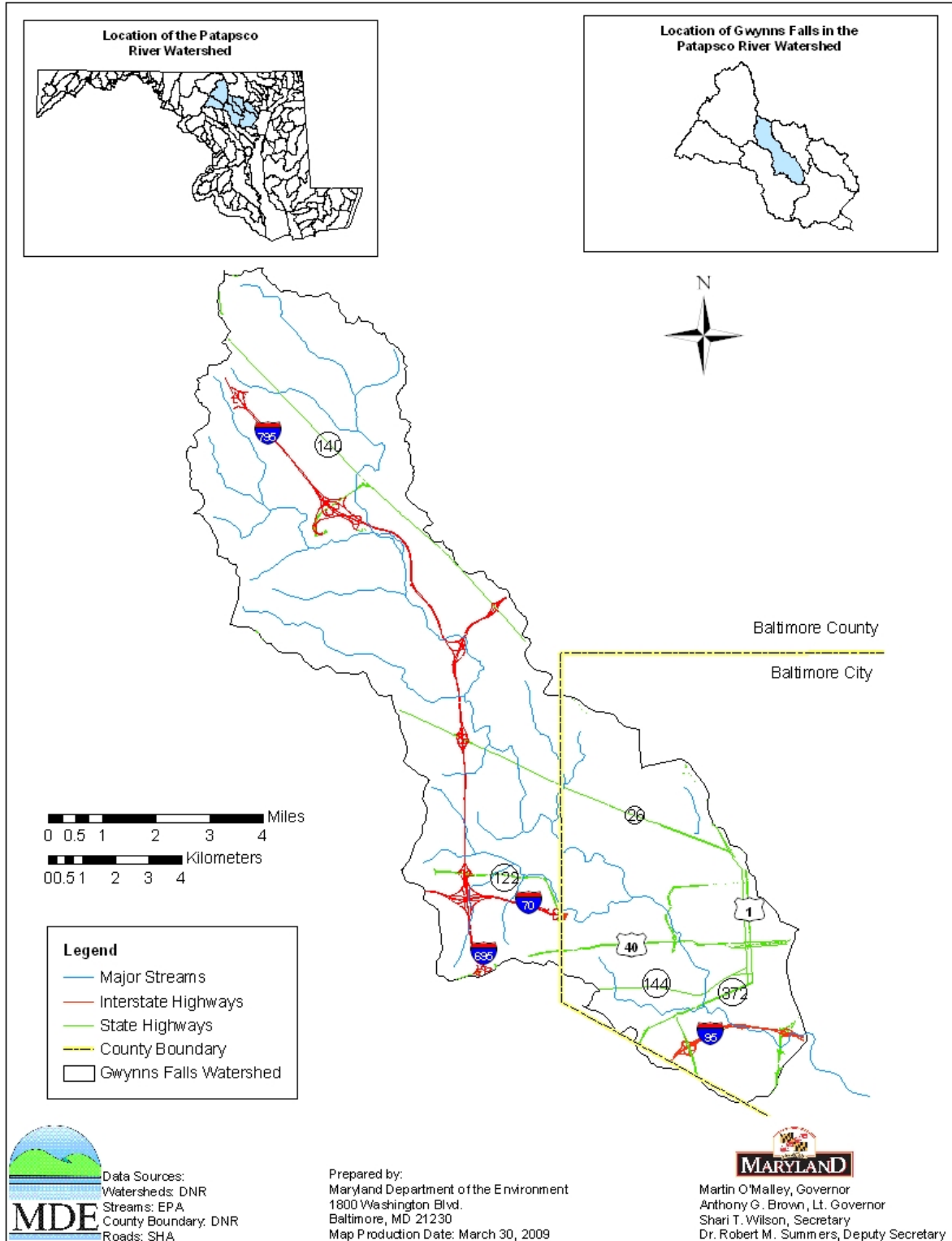


Figure 1: Location Map of the Gwynns Falls Watershed in Baltimore City and Baltimore County, Maryland

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2.1.1. Land Use

Land Use Methodology

The land use framework used to develop this TMDL was originally developed for the Chesapeake Bay Program Phase 5 (CBP P5) watershed model.¹ The CBP P5 land use Geographic Information System (GIS) framework was based on two distinct layers of development. The first GIS layer was developed by the Regional Earth Science Applications Center (RESAC) at the University of Maryland and was based on satellite imagery (Landsat 7-Enhanced Thematic Mapper (ETM) and 5-Thematic Mapper (TM)) (Goetz et al. 2004). This layer did not provide the required level of accuracy that is especially important when developing agricultural land uses. In order to develop accurate agricultural land use calculations, the CBP P5 used county level U.S. Agricultural Census data as a second layer (USDA 1982, 1987, 1992, 1997, 2002).

Given that land cover classifications based on satellite imagery are likely to be least accurate at edges (i.e., boundaries between covers), the RESAC land uses bordering agricultural areas were analyzed separately. If the agricultural census data accounted for more agricultural use than the RESAC's data, appropriate acres were added to agricultural land uses from non-agricultural land uses. Similarly, if census agricultural land estimates were smaller than RESAC's, appropriate acres were added to non-agricultural land uses.

Adjustments were also made to the RESAC land cover to determine developed land uses. RESAC land cover was originally based on the United States Geological Survey (USGS) protocols used to develop the 2000 National Land Cover Database. The only difference between the RESAC and USGS approaches was RESAC's use of town boundaries and road densities to determine urban land covered by trees or grasses. This approach greatly improved the accuracy of the identified urban land uses, but led to the misclassification of some land adjacent to roads and highways as developed land. This was corrected by subsequent analysis. To ensure that the model accurately represented development over the simulation period, post-processing techniques that reflected changes in urban land use have been applied.

The result of this approach is that CBP P5 land use does not exist in a single GIS coverage; instead it is only available in a tabular format. The CBP P5 watershed model is comprised of 25 land uses. Most of these land uses are differentiated only by their nitrogen and phosphorus loading rates. The land uses are divided into 13 classes with distinct sediment erosion rates. Table 1 lists the CBP P5 generalized land uses, detailed land uses, which are classified by their erosion rates, and the acres of each land use in the Gwynns Falls watershed. Details of the land use development methodology have been summarized in the report entitled *Chesapeake Bay Phase 5 Community Watershed Model* (US EPA 2008).

¹ The EPA Chesapeake Bay Program developed the first watershed model in 1982. There have been many upgrades since the first phase of this model. The CBP P5 was developed to estimate flow, nutrient, and sediment loads to the Bay.

Gwynns Falls Watershed Land Use Distribution

The Gwynns Falls watershed consists primarily of urban land use (87.5%), with a small amount of forest land use (10.5%). There are also small amounts of crop (1.7%) and pasture (0.2%). A detailed summary of the watershed land use areas is presented in Table 1, and a land use map is provided in Figure 2.

Table 1: Land Use Percentage Distribution for the Gwynns Falls Watershed

| General Land Use | Detailed Land Use | Area (Acres) | Percent | Grouped Percent of Total |
|-------------------------|------------------------------|---------------------|----------------|---------------------------------|
| Crop | Animal Feeding Operations | 13.1 | 0.0 | 1.7 |
| | Hay | 73.6 | 0.2 | |
| | High Till | 144.3 | 0.3 | |
| | Low Till | 470.9 | 1.1 | |
| | Nursery | 1.1 | 0.0 | |
| Extractive | Extractive | 15.9 | 0.0 | 0.0 |
| Forest | Forest | 4,328.9 | 10.4 | 10.5 |
| | Harvested Forest | 43.7 | 0.1 | |
| Pasture | Pasture | 86.6 | 0.2 | 0.2 |
| | Trampled Pasture | 0.2 | 0.0 | |
| Urban | Urban: Barren (Construction) | 357.7 | 0.9 | 87.5 |
| | Urban: Impervious | 13,582.9 | 32.7 | |
| | Urban: Pervious | 22,436.8 | 54.0 | |
| Total | | 41,555.8 | 100.0 | 100.0 |

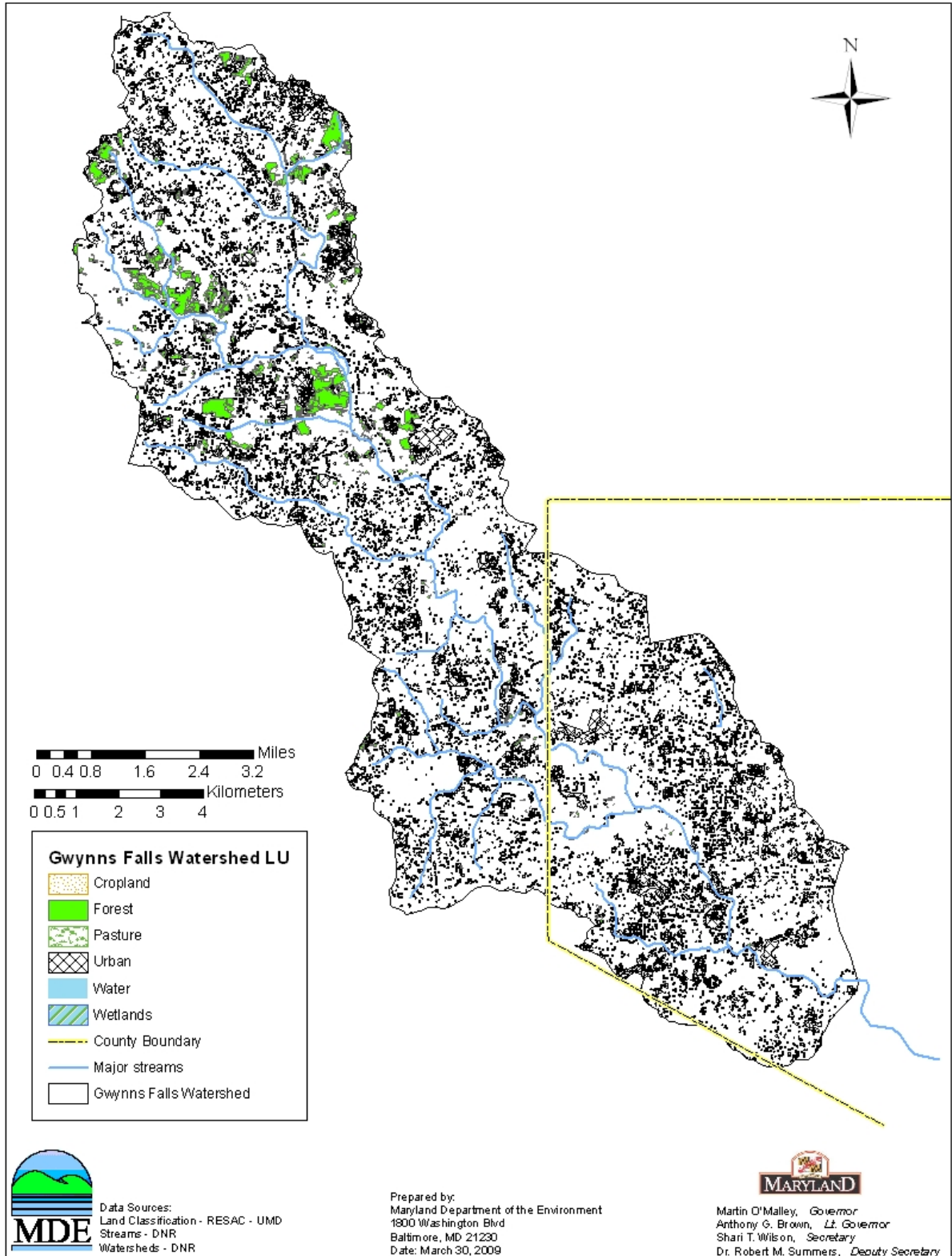


Figure 2: Land Use of the Gwynns Falls Watershed

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2.2 Source Assessment

The Gwynns Falls Watershed Total Baseline Sediment Load can be subdivided into nonpoint and point source loads. This section summarizes the methods used to derive each of these distinct source categories.

2.2.1 Nonpoint Source Assessment

In this document, the nonpoint source loads account for sediment loads from unregulated stormwater runoff within the Gwynns Falls watershed. This section provides the background and methods for determining the nonpoint source baseline loads generated within the Gwynns Falls watershed (Nonpoint Source BL_{GF}).

General load estimation methodology

Nonpoint source sediment loads generated within the Gwynns Falls watershed are estimated based on the *edge-of-stream (EOS) calibration target loading rates* from the CBP P5 model. This approach is based on the fact that not all of the *edge-of-field (EOF)* sediment load is delivered to the stream or river (some of it is stored on fields down slope, at the foot of hillsides, or in smaller rivers or streams that are not represented in the model). To calculate the actual EOS loads, a *sediment delivery ratio* (the ratio of sediment reaching a basin outlet compared to the total erosion within the basin) is used. Details of the methods used to calculate sediment load have been summarized in the report entitled *Chesapeake Bay Phase 5 Community Watershed Model* (US EPA 2008).

Edge-of-Field Target Erosion Rate Methodology

EOF target erosion rates for agricultural land uses and forested land use were based on erosion rates determined by the Natural Resource Inventory (NRI). NRI is a statistical survey of land use and natural resource conditions conducted by the Natural Resources Conservation Service (NRCS) (USDA 2006). Sampling methodology is explained by Nusser and Goebel (1997).

Estimates of average annual erosion rates for pasture and cropland are available on a county basis at five-year intervals, starting in 1982. Erosion rates for forested land uses are not available on a county basis from NRI; however, for the purpose of the CBP Phase 2 watershed model, NRI calculated average annual erosion rates for forested land use on a watershed basis. These rates are still being used as targets in the CBP P5 model.

The average value of the 1982 and 1987 surveys was used as the basis for EOF target loads. The erosion rates from this period do not reflect best management practices (BMPs) or other soil conservation policies introduced in the wake of the effort to restore the Chesapeake Bay. To compensate for this, a BMP factor was included in the loading estimates using best available “draft” information from the CBP P5. Rates for urban pervious, urban impervious, and barren land were based on a combination of best professional judgment, literature analysis, and regression analysis. Table 2 lists erosion rates specific to the Gwynns Falls watershed.

Table 2: Summary of EOF Erosion Rate Calculations

| Land Use | Data Source | Baltimore County (tons/acre/year) | Baltimore City (tons/acre/year) |
|--|-------------------------------------|--------------------------------------|------------------------------------|
| Forest | Phase 2 NRI | 0.46 | 0.47 |
| Harvested Forest ¹ | Average Phase 2 NRI (x 10) | 3 | 3 |
| Nursery | Pasture NRI (x 9.5) | 12.26 | 2.57 |
| Pasture | Pasture NRI (1982-1987) | 1.29 | 0.27 |
| Trampled pasture ² | Pasture NRI (x 9.5) | 12.26 | 2.57 |
| Animal Feeding Operations ² | Pasture NRI (x 9.5) | 12.26 | 2.57 |
| Hay ² | Crop NRI (1982-1987) (x 0.32) | 3.18 | 0.8 |
| High Till | Crop NRI (1982-1987) (x 1.25) | 12.42 | 3.14 |
| Low till With Manure ² | Crop NRI (1982-1987) (x 0.75) | 7.45 | 1.89 |
| Pervious Urban | Intercept Regression Analysis | 0.74 | 0.74 |
| Extractive | Best professional judgment | 10 | 10 |
| Barren | Literature survey | 20 | 20 |
| Impervious | 100% Impervious Regression Analysis | 5.18 | 5.18 |

Notes: ¹Based on an average of NRI values for the Chesapeake Bay Phase 5 segments.

²NRI score data adjusted based on land use.

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Sediment Delivery Ratio: The base formula for calculating *sediment delivery ratios* in the CBP P5 model is the same as the formula used by the NRCS (USDA 1983).

$$DF = 0.417762 * A^{-0.134958} - 0.127097 \quad (\text{Equation 2.1})$$

where

DF (delivery factor) = the sediment delivery ratio

A = drainage area in square miles

In order to account for the changes in sediment loads due to distance traveled to the stream, the CBP P5 model uses the *sediment delivery ratio*. Land use specific *sediment delivery ratios* were calculated for each river segment using the following procedure:

- (1) mean distance of each land use from the river reach was calculated;
- (2) *sediment delivery ratios* for each land use were calculated (drainage area in Equation 2.1 was assumed to be equal to the area of a circle with radius equal to the mean distance between the land use and the river reach).

Edge-of-Stream Loads

Edge-of-stream loads are the loads that actually enter the river reaches (i.e., the mainstem of a watershed). Such loads represent not only the erosion from the land but all of the intervening processes of deposition on hillsides and sediment transport through smaller rivers and streams.

Streambank Erosion

Many studies have documented the relationship between high amounts of connected impervious surfaces, increases in storm flows, and stream degradation in the form of streambank erosion (Schueler 1994; Arnold and Gibbons 1996). In many urbanized watersheds, small stream channels have been replaced by sewer pipes. As a result, impervious surfaces such as rooftops, parking lots, and road surfaces are now directly connected to the main stream channel via the storm sewer system. During a storm event, this causes a greater amount of precipitation to flow more rapidly into a given stream channel once it reaches the surface. Furthermore, less water infiltrates into the ground both during and after a storm event, thereby limiting the amount of groundwater recharge to a stream. This altered urban hydrology typically causes abnormally high flows in streams during storms and abnormally low flows during dry periods. The high flows occurring during storm events increase shear stress and cause excessive erosion of streambanks and streambeds, which leads to degraded stream channel conditions for biological communities (MDE 2007a).

Two methods of estimating streambank erosion were presented in the *Total Maximum Daily Loads of Sediment/Total Suspended Solids for the Anacostia River Basin, Montgomery and Prince George's Counties, Maryland and The District of Columbia*. The first estimate uses the Anacostia Hydrological Simulation Program – FORTRAN (HSPF) watershed model in conjunction with the Penn State University streambank

FINAL

erosion equation (Evans et al. 2003). The analysis estimated that approximately 73% of the total annual sediment load within the Anacostia River watershed could be attributed to streambank erosion (MDE 2007a).

The second method analyzes the long term relationship between flow and total suspended solids (TSS) concentrations to quantify the effects of an altered urban hydrology on watershed sediment loads. Changes in hydrology in the Anacostia River watershed were characterized using daily flow data from the USGS gage stations. The long-term changes over time in the flow duration curves (FDCs) for each of these stations was quantified using a type of statistical analysis known as “quantile regression.” The portion of the FDC representing the highest flows was determined to have increased significantly over time, consistent with hydrologic alteration from increased impervious surfaces. Also, a “sediment rating curve” (i.e., the relationship between suspended sediment concentration and flow) was computed and combined with the FDCs to estimate annual sediment loads before and after increased development (i.e., altered hydrology). The results of the analysis indicate that approximately 75% of the total annual sediment load in the Anacostia River watershed is due to alterations in hydrology (MDE 2007a).

Using CBP P5 urban sediment EOF target values, MDE developed a formula for estimating the percent of erosional sediment resultant from streambank erosion (i.e., that portion of the total urban sediment load attributed to stream bank erosion) based on the amount of impervious land within a watershed. The equation uses the urban sediment loading factors to estimate the proportion of the urban sediment load from stream bank erosion. The assumption is that as impervious surfaces increase, the upland sources decrease, flow increases, and the change in sediment load results from increased streambank erosion. While this formula only represents an empirical approximation, it is consistent with results from the Anacostia River Sediment TMDL and recognizes that stream bank erosion can be a significant portion of the total sediment load. The formula is as follows:

$$\%E = \frac{I * L_I}{I * L_I + (1 - I)L_P} \quad (\text{Equation 2.2})$$

where:

% E = percent erosional sediment resultant from streambank erosion

I = percent impervious

L_I = Impervious urban land use EOF load

L_P = Pervious urban land use EOF load

The relationship demonstrated in equation 2.2 is expressed graphically in Figure 3. Using the equation, the Anacostia River watershed (23% impervious) would equate to approximately a 68% erosional sediment load resultant from streambank erosion. Per Table 1, approximately 33% of the Gwynns Falls watershed is covered by impervious surfaces. This would equate to approximately a 77% erosional sediment load resultant from streambank erosion.

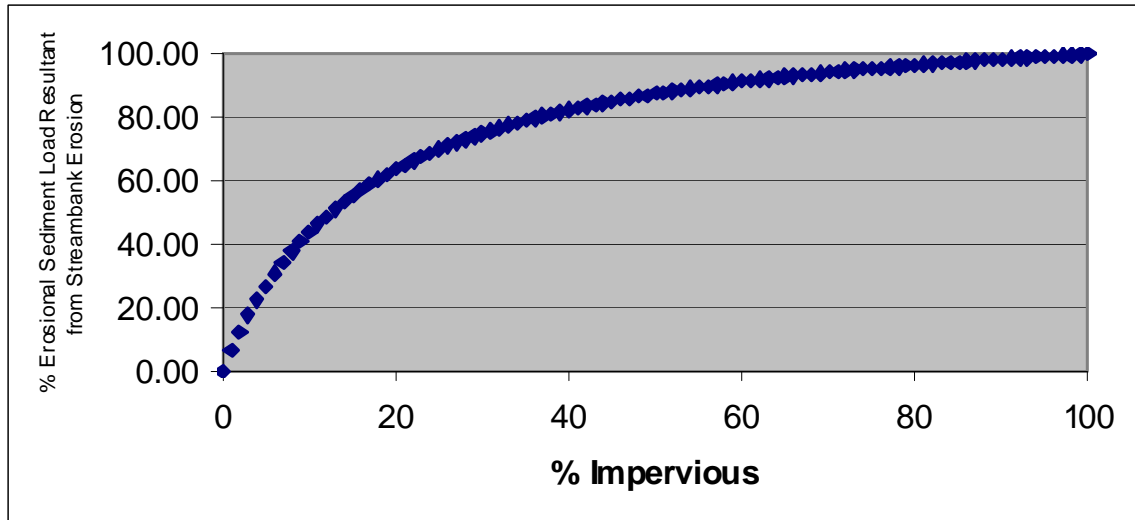


Figure 3: Percent Impervious vs. Percent Erosional Sediment Load Resultant from Streambank Erosion

For this TMDL, erosional sediment resultant from streambank erosion represents an aggregate load within the total urban impervious EOF loads as described in the report *Chesapeake Bay Phase V Community Watershed Model* (US EPA 2008) and is not explicitly reported.

2.2.2 Point Source Assessment

A list of 57 active permitted point sources that contribute to the sediment load in the Gwynns Falls watershed was compiled using MDE's Environmental Permit Service Center (EPSC) database. The types of permits identified include individual municipal, individual municipal separate storm sewer systems (MS4s), general mineral mining, general industrial stormwater, and general MS4s. The permits can be grouped into two categories, process water and stormwater. The process water category includes those loads generated by continuous discharge sources whose permits have TSS limits. The stormwater category includes all National Pollutant Discharge Elimination System (NPDES) regulated stormwater discharges. Other permits that do not meet these conditions are considered *de minimis* in terms of the total sediment load.

The sediment loads for the 5 process water permits (Process Water BL_{GF}) are calculated based on their TSS limits and corresponding flow information. The 52 NPDES Phase I or Phase II stormwater permits identified throughout the Gwynns Falls watershed are regulated based on BMPs and do not include TSS limits. In the absence of TSS limits, the NPDES regulated stormwater baseline load (NPDES Stormwater BL_{GF}) is calculated using methods described in Section 2.2.1 and watershed specific urban land use sediment delivery factors. A detailed list of the permits appears in Appendix B.

2.2.3 Summary of Baseline Loads

Table 3 summarizes the Gwynns Falls Baseline Sediment Load, reported in tons per year (ton/yr) and presented in terms of nonpoint and point source loadings.

Table 3: Gwynns Falls Baseline Sediment Loads (ton/yr)

| Total Baseline Load (ton/yr) | = | Nonpoint Source BL_{GF} | + | NPDES Stormwater BL_{GF} | + | Process Water BL_{GF} |
|--|---|--|---|---|---|--|
| 22,048.5 | = | 1,759.3 | + | 20,076.0 | + | 213.2 |

Table 4 presents a breakdown of the Gwynns Falls Total Baseline Sediment Load, detailing loads per land use. The largest portion of the sediment load is from urban land (92%). The remainder of the sediment load is from crop land (5%) and forest (2%), with small amounts from other land uses.

Table 4: Detailed Baseline Sediment Budget Loads Within the Gwynns Falls Watershed

| General Land Use | Detailed Land Use | Load (Ton/Yr) | Percent | Grouped Percent of Total |
|-------------------------|------------------------------|----------------------|----------------|---------------------------------|
| Crop | Animal Feeding Operations | 34.9 | 0.2 | 5.4 |
| | Hay | 49.9 | 0.2 | |
| | High Till | 361.3 | 1.6 | |
| | Low Till | 740.1 | 3.4 | |
| | Nursery | 2.9 | 0.0 | |
| Extractive | Extractive | 34.3 | 0.2 | 0.2 |
| Forest | Forest | 482.0 | 2.2 | 2.3 |
| | Harvested Forest | 31.7 | 0.1 | |
| Pasture | Pasture | 21.6 | 0.1 | 0.1 |
| | Trampled Pasture | 0.7 | 0.0 | |
| Urban ¹ | Urban: Barren (Construction) | 1069.8 | 4.9 | 91.1 |
| | Urban: Impervious | 15,507.8 | 70.3 | |
| | Urban: Pervious | 3,498.4 | 15.9 | |
| | Process Water | 213.2 | 1.0 | 1.0 |
| Total | | 22,048.5 | 100.0 | 100.0 |

Note: ¹ The urban land use load represents the permitted stormwater load.

2.3 Water Quality Characterization

The Gwynns Falls watershed was originally listed on Maryland's 1996 303(d) List as impaired by elevated sediments from nonpoint sources, with supporting evidence cited in Maryland's 1996 305(b) report. The 1996 305(b) report did not directly state that elevated sediments were a concern, and it has been determined that the sediment listing was based on best professional judgment (MDE 2004; DNR 1996).

Currently in Maryland, there are no specific numeric criteria for suspended sediments. Therefore, to determine whether aquatic health is impacted by elevated sediment loads, MDE's recently developed biological stressor identification methodology was applied. The primary goal of the BSID analysis is to identify the most probable cause(s) for observed biological impairments throughout MD's 8-digit watersheds (MDE 2009a).

The BSID analysis applies a case-control, risk-based, weight-of-evidence approach to identify potential causes of biological impairment. The risk-based approach estimates the strength of association between various stressors and a degraded biological community. The BSID analysis then identifies individual stressors (pollutants) as probable or unlikely causes of the poor biological conditions within a given MD 8-digit watershed and subsequently reviews ecological plausibility/concludes whether or not these individual stressors or groups of stressors are contributing to the impairment (MDE 2009a).

The primary dataset for BSID analysis is round two Maryland Department of Natural Resources (DNR) Maryland Biological Stream Survey (MBSS) data (collected between 2000-2004) because it provides a broad spectrum of paired data variables, which allow for a more comprehensive stressor analysis. The MBSS is a robust statewide probability-based sampling survey for assessing the biological conditions of wadeable, non-tidal streams (Klauda et al. 1998; Roth et al. 2005). It uses a fixed length (75 m) randomly selected stream segment for collecting site level information within a primary sampling unit (PSU), also defined as a watershed. The randomly selected stream segments, from which field data are collected, are selected using either stratified random sampling with proportional allocation, or simple random sampling (Cochran 1977). The random sample design allows for unbiased estimates of overall watershed conditions. Thus, the dataset facilitated case-control analyses because 1) in-stream biological data are paired with chemical, physical, and land use data variables that could be identified as possible stressors and 2) it uses a probabilistic statewide monitoring design.

The BSID analysis groups the individual stressors (physical and chemical variables) into three generalized parameters in order to assess how the resulting impacts of these stressors can alter the biological community and structure. The three generalized parameters include: sediment, habitat, and water chemistry. Identification of a sediment/flow stressor as contributing to the biological impairment is based on the results of the individual stressor associations within both the sediment and habitat parameters that reveal the effects of sediment related impacts or an altered hydrologic regime (MDE 2009a).

FINAL

In addition to the MBSS round two data applied within the BSID analysis, data from the Maryland DNR Core/Trend Program was also used for water quality characterization in the TMDL. The program collected benthic macroinvertebrate data between 1976 and 2006. This data was used to calculate four benthic community measures: total number of taxa, the Shannon Weiner diversity index, the modified Hilsenhoff biotic integrity index, and percent Ephemeroptera, Plecoptera, and Trichoptera (EPT). DNR has extensive monitoring data for two stations on the mainstem of the Gwynns Falls through the Core/Trend program. One station is located at Liberty Road and the other at Route 1. (See Figure 4 and table 5) (DNR 2007).

Gwynns Falls Watershed Monitoring Stations

A total of 30 water quality monitoring stations were used to characterize the Gwynns Falls Watershed. Twenty-eight biological/physical habitat monitoring stations from the MBSS program round one and two data collection were used to characterize the Gwynns Falls Watershed in Maryland's 2008 Integrated Report. The BSID analysis used the 12 biological/physical habitat monitoring stations from the MBSS program round two data collection. Additionally, two biological monitoring stations from the Maryland Core/Trend monitoring network were applied within the TMDL analysis. All stations are presented in Figure 4 and listed in Table 5.

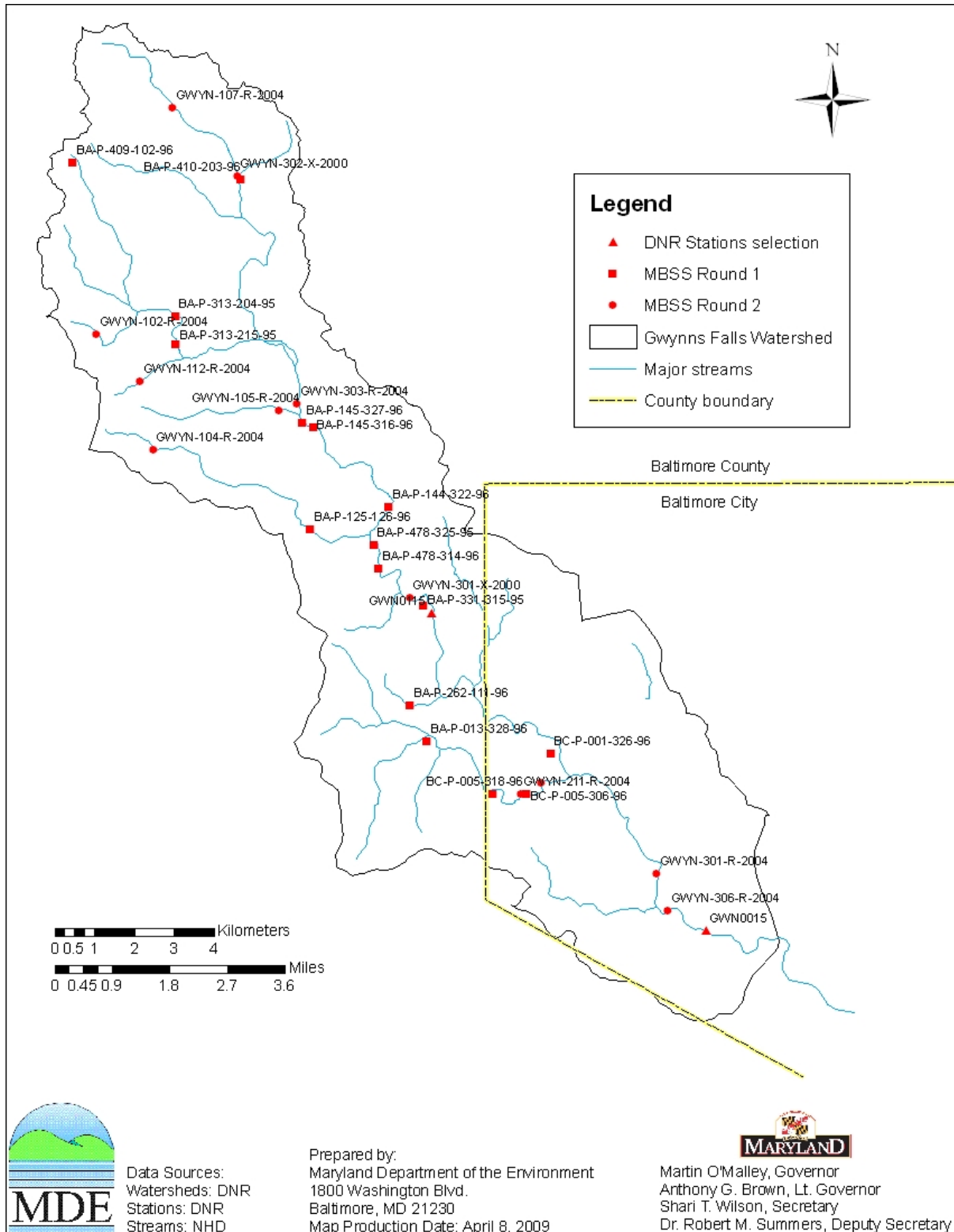


Figure 4: Monitoring Stations in the Gwynns Falls Watershed

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Table 5: Monitoring Stations in the Gwynns Falls Watershed

| Site Number | Sponsor | Site Type | Site Name | Latitude (dec degrees) | Longitude (dec degrees) |
|--------------------|----------------|------------------|------------------|-----------------------------------|------------------------------------|
| BA-P-013-328-96 | MD DNR | MBSS, Round 1 | DEAD RUN | 39.3140 | -76.7280 |
| BA-P-125-126-96 | MD DNR | MBSS, Round 1 | SCOTTS LEVEL BR | 39.3620 | -76.7620 |
| BA-P-144-322-96 | MD DNR | MBSS, Round 1 | GWYNNS FALLS | 39.3670 | -76.7390 |
| BA-P-145-316-96 | MD DNR | MBSS, Round 1 | GWYNNS FALLS | 39.3850 | -76.7610 |
| BA-P-145-327-96 | MD DNR | MBSS, Round 1 | GWYNNS FALLS | 39.3860 | -76.7640 |
| BA-P-262-111-96 | MD DNR | MBSS, Round 1 | GWYNNS FALLS UT1 | 39.3220 | -76.7330 |
| BA-P-313-204-95 | MD DNR | MBSS, Round 1 | RED RUN | 39.4102 | -76.8012 |
| BA-P-313-215-95 | MD DNR | MBSS, Round 1 | RED RUN | 39.4040 | -76.8009 |
| BA-P-331-315-95 | MD DNR | MBSS, Round 1 | GWYNNS FALLS | 39.3446 | -76.7289 |
| BA-P-409-102-96 | MD DNR | MBSS, Round 1 | RED RUN | 39.4450 | -76.8310 |
| BA-P-410-203-96 | MD DNR | MBSS, Round 1 | GWYNNS FALLS | 39.4410 | -76.7820 |
| BA-P-478-314-96 | MD DNR | MBSS, Round 1 | GWYNNS FALLS | 39.3530 | -76.7420 |
| BA-P-478-325-95 | MD DNR | MBSS, Round 1 | GWYNNS FALLS | 39.3583 | -76.7434 |
| BC-P-001-326-96 | MD DNR | MBSS, Round 1 | GWYNNS FALLS | 39.3110 | -76.6920 |
| BC-P-005-306-96 | MD DNR | MBSS, Round 1 | DEAD RUN | 39.3020 | -76.6990 |
| BC-P-005-318-96 | MD DNR | MBSS, Round 1 | DEAD RUN | 39.3020 | -76.7090 |
| GWYN-102-R-2004 | MD DNR | MBSS, Round 2 | RED RUN UT 2 | 39.4062 | -76.8241 |
| GWYN-104-R-2004 | MD DNR | MBSS, Round 2 | SCOTTS LEVEL BR | 39.3801 | -76.8078 |
| GWYN-105-R-2004 | MD DNR | MBSS, Round 2 | HORSEHEAD BR | 39.3888 | -76.7709 |
| GWYN-107-R-2004 | MD DNR | MBSS, Round 2 | GWYNNS FALLS | 39.4572 | -76.8018 |
| GWYN-112-R-2004 | MD DNR | MBSS, Round 2 | RED RUN UT 1 | 39.3955 | -76.8114 |
| GWYN-210-R-2004 | MD DNR | MBSS, Round 2 | DEAD RUN | 39.3044 | -76.6949 |
| GWYN-211-R-2004 | MD DNR | MBSS, Round 2 | DEAD RUN | 39.3019 | -76.7008 |
| GWYN-301-R-2004 | MD DNR | MBSS, Round 2 | GWYNNS FALLS | 39.2838 | -76.6614 |
| GWYN-301-X-2000 | MD DNR | MBSS, Round 2 | GWYNNS FALLS | 39.3464 | -76.7331 |
| GWYN-302-X-2000 | MD DNR | MBSS, Round 2 | GWYNNS FALLS | 39.4419 | -76.7831 |
| GWYN-303-R-2004 | MD DNR | MBSS, Round 2 | GWYNNS FALLS | 39.3904 | -76.7656 |
| GWYN-306-R-2004 | MD DNR | MBSS, Round 2 | GWYNNS FALLS | 39.2755 | -76.6582 |
| GWN0015 | MD DNR | Trend | Route 1 | 39.3140 | -76.7280 |
| GWN0115 | MD DNR | Core | Liberty road | 39.3620 | -76.7620 |

2.4 Water Quality Impairment

The Maryland water quality standards surface water use designations for the Gwynns Falls mainstem and its tributaries is Use I (Water Contact Recreation, and Protection of Nontidal Warmwater Aquatic Life), except for the Gwynns Falls mainstem and its tributaries above Reisterstown Road and Red Run and its tributaries, which are designated as Use III (Nontidal Cold Water), and Dead Run and its tributaries, which are classified as Use IV (Recreational Trout Waters) (COMAR 2008a,b,c,d,e). The water quality impairment of the Gwynns Falls watershed addressed by this TMDL is caused by an elevated sediment load beyond a level that the watershed can sustain without causing any sediment related impacts to aquatic health, where aquatic health is based on benthic and fish Index of Biotic Integrity (IBI) scores, as demonstrated via the BSID analysis for the watershed.

The Gwynns Falls watershed is listed on Maryland's 2008 Integrated Report as impaired for impacts to biological communities. Greater than 79% of the stream miles in the Gwynns Falls watershed are assessed as having degraded biological conditions (when compared to regional reference indices). The biological impairment listing is based on the combined results of MBSS round one (1995-1997) and round two (2000-2004) data, which includes twenty-eight stations. Twenty-two of the twenty-eight stations have degraded BIBI/FIBI scores significantly lower than 3.0 (MDE 2008). As mentioned in Section 2.3, however, only MBSS round 2 data were used in the BSID analysis. See Figure 4 and Table 5 for station locations and information.

The results of the BSID analysis for the Gwynns Falls watershed are presented in a report entitled *Watershed Report for Biological Impairment of the Gwynns Falls Watershed in Baltimore City and Baltimore County, Maryland Biological Stressor Identification Analysis Results and Interpretation* (MDE 2009b). The report states that the degradation of biological communities in the Gwynns Falls watershed is strongly associated with urban land use and its concomitant effects: altered hydrology, sediment related impacts, and elevated levels of sulfate, chlorides, and conductivity (a measure of the presence of dissolved substances).

The BSID analysis has determined that the biological impairment in the Gwynns Falls watershed is due in part to flow/sediment related stressors. Specifically, the analysis confirmed that individual stressors within the sediment and habitat parameter groupings were contributing to the biological impairment in the watershed. Also, the analysis identified the following stressors within the sediment and habitat parameter groupings as having a statistically significant association with impaired biological communities at the respective percentage of degraded sites: channelization (34%), channel alteration (poor: 24%), and bar formation (extensive: 23%). Overall, sediment and flow stressors within the sediment and habitat parameter groupings were identified at approximately 24% and 40%, respectively, of the degraded sites throughout the watershed (MDE 2009b). Therefore, since sediment is identified as a stressor to the biological communities in the Gwynns Falls watershed, a TMDL is required.

FINAL

As a supplement to the MBSS round two data used in the BSID analysis, the biological monitoring results from the two Maryland DNR Core/trend stations along the mainstem of the Gwynns Falls indicate that mainstem water quality can be classified as poor to fair/good based on percent EPT, taxa number, biotic index, and diversity index (see Table 6). Statistical analysis of the long term Core/Trend data indicates since 1977, that one station has shown improvement and one station has shown no change (DNR 2007). The poor water quality status for Station GWN0015 is consistent with the results of the MBSS data at the nearby upstream station, GWYN-306-R-2004.

Table 6: Gwynns Falls Core/Trend Data

| Site Number | Current Water Quality Status | Trend Since 1970's |
|--------------------|-------------------------------------|---------------------------|
| GWN0015 | POOR | NO CHANGE |
| GWN0115 | FAIR/GOOD | SLIGHT IMPROVEMENT |

FINAL

3.0 TARGETED WATER QUALITY GOAL

The objective of the sediment TMDL established herein is to reduce sediment loads, and subsequent effects on aquatic health, in the Gwynns Falls watershed to levels that support the Use I/III/IV designations (Water contact recreation, and protection of Nontidal Warmwater Aquatic Life) (Nontidal Coldwater) (Recreational Trout Waters) (COMAR 2008a,b,c,d,e). Assessment of aquatic health is based on Maryland's biocriteria protocol, which evaluates both the amount and diversity of the benthic and fish community through the use of the IBI (Roth et al. 1998, 2000; Stribling et al. 1998; MDE 2008).

Reductions in sediment loads are expected to result from decreased watershed and streambed erosion, which will then lead to improved benthic and fish habitat conditions. Specifically, sediment load reductions are expected to result in an increase in the number of benthic sensitive species present, an increase in the available and suitable habitat for a benthic community, a possible decrease in fine sediment (fines), and improved stream habitat diversity, all of which will result in improved water quality.

The TMDL, however, will not completely resolve the impairment to biological communities within the watershed. Since the BSID watershed analysis identifies other possible stressors (i.e., chlorides, sulfate, conductivity) as impacting the biological conditions, this impairment remains to be fully addressed through the Integrated Report listing process and the TMDL development process, such that all impairing substances identified as impacting biological communities in the watershed are reduced to levels that will meet water quality standards, as established in future TMDLs for those substances (MDE 2009a).

4.0 TOTAL MAXIMUM DAILY LOADS AND SOURCE ALLOCATION

4.1 Overview

This section describes how the sediment TMDL and the corresponding allocations were developed for the Gwynns Falls watershed. Section 4.2 describes the analysis framework for estimating sediment loading rates and the assimilative capacity of the watershed stream system. Section 4.3 summarizes the scenarios that were used in the analysis and presents results. Section 4.4 discusses critical conditions and seasonality. Section 4.5 explains the calculations of TMDL loading caps. Section 4.6 details the load allocations, and Section 4.7 explains the rationale for the margin of safety. Finally, Section 4.8 summarizes the TMDL.

4.2 Analysis Framework

Since there are no specific numeric criteria that quantify the impact of sediment on the aquatic health of nontidal stream systems, a reference watershed approach will be used to establish the TMDL. Furthermore, as the BSID analysis established a link between biological impairment and sediment related stressors, the reference watershed approach will utilize a biological endpoint.

Watershed Model

The watershed model framework chosen for the Gwynns Falls watershed TMDL was the CBP P5 long-term average annual watershed model EOS loading rates. The spatial domain of the CBP P5 watershed model segmentation aggregates to the MD 8-digit watersheds, which is consistent with the impairment listing. The EOS loading rates were used because actual time variable CBP P5 calibration and scenario runs are currently being developed and are not yet available. These target-loading rates are used to calibrate the land use EOS loads within the CBP P5 model and thus should be consistent with future CBP modeling efforts.

The nonpoint source and NPDES stormwater baseline sediment loads generated within the Gwynns Falls watershed are calculated as the sum of corresponding land use EOS loads within the watershed and represent a long-term average loading rate. Individual land use EOS loads are calculated as a product of the land use area, land use target loading rate, and loss from the EOF to the main channel. The loss from the EOF to the main channel is the *sediment delivery ratio* and is defined as the ratio of the sediment load reaching a basin outlet to the total erosion within the basin. A *sediment delivery ratio* is estimated for each land use type based on the proximity of the land use to the main channel. Thus, as the distance to the main channel increases, more sediment is stored within the channels (i.e., *sediment delivery ratio* decreases). Details of the data sources for the unit loading rates can be found in Section 2.2 of this report.

The Gwynns Falls watershed was evaluated using two watershed TMDL segments (see Figure 5). TMDL Segment 1 represents the sediment loads generated in the northwestern portion of the watershed. TMDL Segment 2 represents the sediment loads generated in the southeastern portion of the watershed.

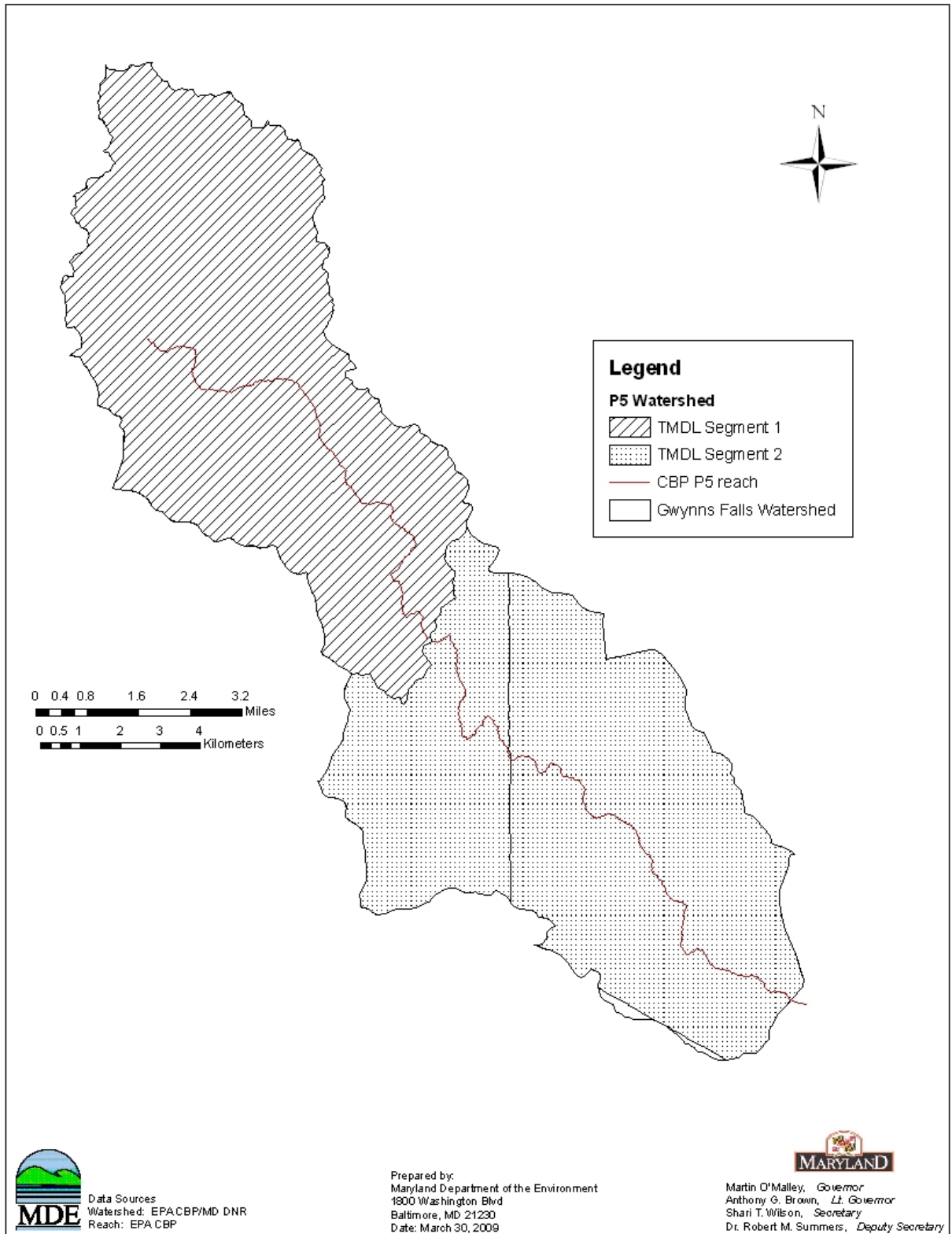


Figure 5: Gwynns Falls Watershed TMDL Segmentation

Reference Watershed Approach

Currently in Maryland, there are no specific numeric criteria that quantify the impact of sediment on the aquatic health of non-tidal stream systems. Therefore, in order to quantify the impact of sediment on the aquatic health of non-tidal stream systems, a reference watershed TMDL approach was used and resulted in the establishment of a *sediment loading threshold* for watersheds within the Highland and Piedmont physiographic regions (Currey et al. 2006). Reference watersheds were determined based on Maryland's biocriteria methodology. The biocriteria methodology assesses biological impairment at the 8-digit watershed scale based on the percentage of MBSS monitoring stations, translated into watershed stream miles, that are degraded. Individual monitoring station impairment is determined based on BIBI/FIBI scores lower than the Minimum Allowable IBI Limit (MAL), which is calculated based on the average annual allowable IBI value of 3.0 (on a scale of 1 to 5). Applying the MAL threshold helps avoid classification errors when assessing biological impairment (Roth et al. 1998, 2000; Stribling et al. 1998; MDE 2008).

Comparison of watershed sediment loads to loads from reference watersheds requires that the watersheds be similar in physical and hydrological characteristics. To satisfy this requirement, Currey et al. (2006) selected reference watersheds only from the Highland and Piedmont physiographic regions (see appendix A for the list of reference watersheds). This region is consistent with the non-coastal region that was identified in the 1998 development of FIBI and subsequently used in the development of BIBI (Roth et al. 1998; Stribling et al. 1998).

To reduce the effect of the variability within the Highland and Piedmont physiographic regions, the watershed sediment loads were then normalized by a constant background condition, the all forested watershed condition. This new normalized term, defined as the *forest normalized sediment load* (Y_n), represents how many times greater the current watershed sediment load is than the *all forested sediment load*. A similar approach was used by EPA Region 9 for sediment TMDLs in California (e.g., Navarro River or Trinity River TMDLs), where the loading capacity was based on an analysis of the amount of human-caused sediment delivery that can occur in addition to natural sediment delivery, without causing adverse impacts to aquatic life. The *forest normalized sediment load* for this TMDL is calculated as the current watershed sediment load divided by the *all forested sediment load*. The equation for the *forest normalized sediment load* is as follows:

$$Y_n = \frac{y_{ws}}{y_{for}} \quad \text{(Equation 4.1)}$$

where:

- Y_n = forest normalized sediment load
- y_{ws} = current watershed sediment load (ton/yr)
- y_{for} = all forested sediment load (ton/yr)

FINAL

Nine reference watersheds were selected from the Highland/Piedmont region. Reference watershed *forest normalized sediment loads* were calculated using CBP P5 2000 land use in order to maintain consistency with MBSS sampling years. The median and 75th percentile of the reference watershed *forest normalized sediment loads* were calculated and found to be 3.3 and 4.2 respectively. These values are in close agreement with more complex methods used to determine the *sediment loading threshold* in previous nontidal sediment TMDLs. Therefore, the median value of 3.3 was established as the *sediment loading threshold* as an environmentally conservative approach to develop this TMDL (see Appendix A for more details).

The *forest normalized sediment loads* for the Gwynns Falls watershed (estimated as 4.3 and 5.9 for TMDL Segments 1 and 2 respectively) were calculated using CBP P5 2005 landuse, to best represent current conditions. A comparison of the Gwynns Falls watershed *forest normalized sediment loads* to the *forest normalized reference sediment load* (also referred to as the *sediment loading threshold*) demonstrates that both TMDL segments exceed the *sediment loading threshold*, indicating that they are receiving loads that are above the maximum allowable load that the watershed can sustain and still meet water quality standards.

4.3 Scenario Descriptions and Results

The following analyses allow a comparison of baseline conditions (under which water quality problems exist) with future conditions, which project the water quality response to various simulated sediment load reductions. The analyses are grouped according to baseline conditions and future conditions associated with TMDLs.

Baseline Conditions

The baseline conditions are intended to provide a point of reference by which to compare the future scenario that simulates conditions of a TMDL. The baseline conditions typically reflect an approximation of nonpoint source loads during the monitoring time frame, as well as estimated point source loads based on discharge data for the same period.

The Gwynns Falls watershed baseline sediment loads are estimated using the CBP P5 target EOS land use sediment loading rates with 2005 land use. Watershed loading calculations, based on the CBP P5 segmentation scheme, are represented by multiple CBP P5 model segments within each TMDL segment. The sediment loads from these segments are combined to represent the baseline condition. The point source sediment loads are estimated based on the existing permit information. Details of these loading source estimates can be found in Section 2.2 and Appendix B of this report.

Future (TMDL) Conditions

This scenario represents the future conditions of maximum allowable sediment loads whereby there will be no sediment related impacts to aquatic health. In the TMDL calculation, the allowable load for the impaired watershed is calculated as the product of the *sediment loading threshold* (determined from watersheds with a healthy biological community) and the Gwynns Falls *all forested sediment load* (see Section 4.2). The resulting load is considered the maximum allowable load the watershed can sustain without causing any sediment related impacts to aquatic health.

The TMDL loading and associated reductions are averaged at the MD 8-digit watershed scale, which is consistent with the original listing scale. It is important to recognize that some subwatersheds may require higher reductions than others, depending on the distribution of the land use.

FINAL

The formula for estimating the TMDL is as follows:

$$TMDL = \sum_{i=1}^n Yn_{ref} \cdot y_{forest_i} \quad (\text{Equation 4.2})$$

where

TMDL = allowable load for impaired watershed (ton/yr)

Yn_{ref} = sediment loading threshold = forest normalized reference sediment load (3.3)

y_{forest_i} = all forested sediment load for segment i (ton /yr)

i = CBP P5 model segment

n = number of CBP P5 model segments in watershed

The Gwynns Falls watershed allowable sediment load is estimated using equation 4.2.

4.4 Critical Condition and Seasonality

EPA's regulations require TMDLs to take into account seasonality and critical conditions for stream flow, loading, and water quality parameters (CFR 2008b). The intent of this requirement is to ensure that the water quality of the waterbody is protected during times when it is most vulnerable. The biological monitoring data used to determine the reference watersheds integrates the stress effects over the course of time and thus inherently addresses critical conditions. Seasonality is captured in two components. First, it is implicitly included through the use of the biological monitoring data. Second, the MBSS dataset included benthic sampling in the spring and fish sampling in the summer.

4.5 TMDL Loading Caps

This section presents the Gwynns Falls watershed average annual sediment TMDL. This load is considered the maximum allowable long-term average annual load the watershed can sustain without causing any sediment related impacts to aquatic health.

The long-term average annual TMDL was calculated for both TMDL Segment 1 and Segment 2 (see Figure 5) independently, based on Equation 4.2 and set at a load 3.3 times the all forested condition. In order to attain the TMDL loading cap calculated for the segments, reductions will be applied to the predominant controllable sources. If only these predominant (generally the largest) sources are controlled, water quality standards can be achieved in the most effective, efficient, and equitable manner. Urban land was identified as the most extensive predominant controllable source in both of the TMDL segments.

Currently, MDE requires that large and medium MS4s retrofit 10% of existing urban land area where there is failing or no stormwater management every permit cycle (5 years). This level of restoration has been determined to be the current maximum feasible, regulated stormwater reduction scenario. Therefore, the reductions applied within this TMDL analysis are consistent with this 10% retrofit goal to existing urban land every 5

FINAL

years with an estimated 65% TSS reduction efficiency from future stormwater BMPs (Claytor and Schueler 1997; Baldwin et al. 2007; Baish and Caliri 2009).

If the TMDL still is not achieved after applying the current maximum feasible urban stormwater reductions, then constant reductions will be applied to the remaining predominant controllable sources (i.e., significant contributors of sediment to the stream system), independent of jurisdiction. In addition to urban land, predominant sources typically include high till crops, low till crops, hay, pasture, and harvested forest, but additional sources might need to be controlled in order to ensure that the TMDL is attained.

The Gwynns Falls Baseline Load and TMDL are presented in Table 7.

Table 7: Gwynns Falls Baseline Load and TMDL

| | Baseline Load (ton/yr) | TMDL (ton/yr) | Reduction (%) |
|-----------------------|----------------------------------|-------------------------|-------------------------|
| TMDL Segment 1 | 8,474.7 | 6,481.3 | 23.5 |
| TMDL Segment 2 | 13,573.6 | 7,514.9 | 44.6 |
| Total | 22,048.5 | 13,996.2 | 36.5 |

4.6 Load Allocations Between Point and Nonpoint Sources

Per EPA regulation, all TMDLs need to be presented as a sum of waste load allocations (WLAs) for point sources and load allocations (LAs) for nonpoint source loads generated within the assessment unit, as well as natural background, tributary, and adjacent segment loads (CFR 2008a). Consequently, the Gwynns Falls watershed TMDL allocations are presented in terms of WLAs (i.e., point source loads identified within the watershed) and LAs (i.e., the nonpoint source loads within the watershed). The State reserves the right to allocate the TMDL among different sources in any manner that is reasonably calculated to protect aquatic life from sediment related impacts.

As described in Section 4.5, reductions were only applied to the regulated urban stormwater sources. Furthermore, reductions were only applied to urban areas developed prior to 1985 (i.e., approximate areas with no stormwater management). This is consistent with MS4 permit requirements for retrofitting existing urban areas at a rate of 10% every 5 years. The reduction in sediment loads associated with retrofitting 10% of existing urban areas every 5 years, with an estimated 65% TSS reduction efficiency, represents the current maximum feasible reduction scenario from the urban land use within the watershed.

FINAL

In this watershed, in addition to urban land, crop and pasture were identified as the predominant controllable sources; however, no reductions were applied to these sources, since the TMDL is achieved when the current maximum feasible reductions are applied to the regulated urban stormwater sources in the watershed. Forest is the only non-controllable source, as it represents the most natural condition in the watershed, and no reductions were applied to permitted process water sources because at 1.0% of the total load, such controls would produce no discernable water quality benefit.

Table 8 summarizes the TMDL results for the Gwynns Falls watershed, derived by applying the current maximum feasible reductions to the applicable urban sediment sources. Tables 9 and 10 summarize the TMDL scenarios for TMDL Segments 1 and 2 individually. The reductions associated with the current maximum feasible scenario result in sediment loading reductions greater than those needed to achieve the TMDL. Thus, the TMDL results in Tables 8, 9, and 10 represent a feasible reduction scenario from the applicable urban sediment sources, determined using the current maximum feasible reduction scenario as a basis. The TMDL results in an overall reduction of 36% for the Gwynns Falls watershed. For more detailed information regarding the Gwynns Falls Watershed TMDL nonpoint source LA, please see the technical memorandum to this document entitled “*Significant Sediment Nonpoint Sources in the Gwynns Falls Watershed*”.

Table 8: Gwynns Falls TMDL Reductions by Source Category

| Baseline Load Source Categories | | Baseline Load (ton/yr) | TMDL Components | TMDL (ton/yr) | Reduction (%) |
|---------------------------------|---------|------------------------|-----------------|-----------------|---------------|
| Nonpoint Source | | 1,759.3 | LA | 1,759.3 | 0.0% |
| Point Source | Urban | 20,076.0 | WLA | 12,023.7 | 40.1% |
| | Permits | 213.2 | | 213.2 | 0.0% |
| TOTAL | | 22,048.5 | | 13,996.2 | 36.5% |

Table 9: Gwynns Falls TMDL Segment 1 Reductions by Source Category

| Baseline Load Source Categories | | Baseline Load (ton/yr) | TMDL Components | TMDL (ton/yr) | Reduction (%) |
|---------------------------------|---------|------------------------|-----------------|----------------|---------------|
| Nonpoint Source | | 1,507.0 | LA | 1,507.0 | 0.0 |
| Point Source | Urban | 6,967.7 | WLA | 4,974.2 | 28.6 |
| | Permits | 0.1 | | 0.1 | 0.0 |
| TOTAL | | 8,474.7 | | 6,481.3 | 23.5 |

Table 10: Gwynns Falls TMDL Segment 2 Reductions by Source Category

| Baseline Load Source Categories | | Baseline Load (ton/yr) | TMDL Components | TMDL (ton/yr) | Reduction (%) |
|---------------------------------|---------|------------------------|-----------------|----------------|---------------|
| Nonpoint Source | | 252.3 | LA | 252.3 | 0.0 |
| Point Source | Urban | 13,108.2 | WLA | 7,049.5 | 46.2 |
| | Permits | 213.1 | | 213.1 | 0.0 |
| TOTAL | | 13,573.6 | | 7,514.9 | 44.6 |

The WLA of the Gwynns Falls watershed is allocated to two permitted source categories, Process Water WLA and Stormwater WLA. The categories are described below.

Process Water WLA

Process Water permits with specific TSS limits and corresponding flow information are assigned to the WLA. In this case, detailed information is available to accurately estimate the WLA. If specific TSS limits are not explicitly stated in the process water permit, then TSS loads are expected to be *de minimis*. If loads are *de minimis*, then they pose little or no risk to the aquatic environment and are not a significant source.

Process Water permits with specific TSS limits include:

- Individual industrial facilities
- Individual municipal facilities
- General mineral mining facilities

There are 5 process water sources with explicit TSS limits, which include 1 municipal sources, and 4 mineral mines. The total estimated TSS load from all of the process water sources is based on current permit limits and is equal to 213.2 ton/yr. As mentioned above, no reductions were applied to this source because at 1.0% of the total load, such controls would produce no discernable water quality benefit. For a detailed list of the 5 process water sources including information on their permit limits, please see Appendix B. For information regarding the allocations to individual process water point sources, please see the technical memoranda to this document entitled “*Significant Sediment Point Sources in the Gwynns Falls Watershed*”.

Stormwater WLA

Per EPA requirements, “stormwater discharges that are regulated under Phase I or Phase II of the NPDES stormwater program are point sources that must be included in the WLA portion of a TMDL” (US EPA 2002). Phase I and II permits can include the following types of discharges:

- Small, medium, and large MS4s – these can be owned by local jurisdictions, municipalities, and state and federal entities (e.g., departments of transportation, hospitals, military bases),

FINAL

- Industrial facilities permitted for stormwater discharges, and
- Small and large construction sites.

EPA recognizes that available data and information are usually not detailed enough to determine WLAs for NPDES regulated stormwater discharges on an outfall-specific basis (US EPA 2002). Therefore, NPDES regulated stormwater loads within the Gwynns Falls watershed will be expressed as a single NPDES stormwater WLA. Upon approval of the TMDL, “NPDES-regulated municipal stormwater and small construction storm water discharges effluent limits should be expressed as BMPs or other similar requirements, rather than as numeric effluent limits” (US EPA 2002).

The Gwynns Falls NPDES stormwater WLA is based on reductions applied to the sediment load from the urban land use of the watershed derived from the current maximum feasible stormwater reduction scenario and may include legacy or other sediment sources. Some of these sources may also be subject to controls from other management programs. The Gwynns Falls NPDES stormwater WLA requires an overall reduction of 40.1% (see Table 8).

As stormwater assessment and/or other program monitoring efforts result in a more refined source assessment, MDE reserves the right to revise the current NPDES stormwater WLA provided the revisions are reasonably calculated to protect aquatic life from sediment related impacts.

For more information on the methods used to calculate the baseline urban sediment load, see Section 2.2.2. For a detailed list of all of the NPDES regulated stormwater discharges within the watershed, please see Appendix B, and for information regarding the NPDES stormwater WLA distribution amongst these discharges, please see the technical memorandum to this document entitled “*Significant Sediment Point Sources in the Gwynns Falls Watershed*”.

4.7 Margin of Safety

All TMDLs must include a margin of safety to account for any lack of knowledge and uncertainty concerning the relationship between loads and water quality (CFR 2008b). It is proposed that the estimated variability around the reference watershed group used in this analysis already accounts for such uncertainty. Analysis of the reference group *forest normalized sediment loads* indicates that approximately 75% of the reference watersheds have a value of less than 4.2. Also, 50% of the reference watersheds have a value less than 3.3. Based on this analysis the *forest normalized reference sediment load* (also referred to as the *sediment loading threshold*) was set at the median value of 3.3 (Currey et al. 2006). This is considered an environmentally conservative estimate, since 50% of the reference watersheds have a load above this value, which when compared to the 75% value, results in an implicit margin of safety of approximately 18%.

4.8 Summary of Total Maximum Daily Loads

The average annual Gwynns Falls watershed TMDL is summarized in Table 11. The TMDL is the sum of the LA, NPDES Stormwater WLA, Process Water WLA, and MOS. The Maximum Daily Load (MDL) is summarized in Table 12 (See Appendix C for more details).

Table 11: Gwynns Falls Watershed Average Annual TMDL of Sediment/TSS (ton/yr)

| | | | | | | | | |
|----------------------|---|------------------------|---|--|---|---|---|------------|
| TMDL (ton/yr) | = | LA_{GF} | + | NPDES Stormwater WLA_{GF} | + | Process Water WLA_{GF} | + | MOS |
| 13,996.2 | = | 1,759.3 | + | 12,023.7 | + | 213.2 | + | Implicit |

Table 12: Gwynns Falls Maximum Daily Loads of Sediment/TSS (ton/day)

| | | | | | | | | |
|----------------------|---|------------------------|---|--|---|---|---|------------|
| MDL (ton/day) | = | LA_{GF} | + | NPDES Stormwater WLA_{GF} | + | Process Water WLA_{GF} | + | MOS |
| 558.7 | = | 70.4 | + | 486.5 | + | 1.82 | + | Implicit |

FINAL

5.0 ASSURANCE OF IMPLEMENTATION

This section provides the basis for reasonable assurances that the sediment TMDL will be achieved and maintained. Section 303(d) of the Clean Water Act and current EPA regulations require reasonable assurance that the TMDL load and wasteload allocations can and will be implemented (CFR 2008b). Maryland has several well-established programs to draw upon, including the Water Quality Improvement Act of 1998 (WQIA) and the Federal Nonpoint Source Management Program (§ 319 of the Clean Water Act).

Potential funding sources available for local governments for implementation include the Buffer Incentive Program (BIP), the State Water Quality Revolving Loan Fund, and the Stormwater Pollution Cost Share Program. Details of these programs and additional funding sources can be found at <http://www.dnr.state.md.us/bay/services/summaries.html>.

Potential BMPs for reducing sediment loads and resulting impacts can be grouped into three general categories. The first is directed toward agricultural lands, the second towards urban (developed) land, and the third applies to all land uses. Since urban land was identified as the most extensive primary, predominant controllable source of sediment within the watershed (i.e., 92% of the total Gwynns Falls Baseline Sediment Load), and based on current maximum feasible reductions to regulated urban stormwater, the entirety of the required sediment reductions within the Gwynns Falls watershed are attributed to urban (developed) land use. The various BMPs applicable to reducing urban sediment loads are discussed below.

Sediment from urban areas can be reduced by stormwater retrofits, impervious surface reduction, street sweeping, inlet cleaning, increases in urban tree canopy cover, and stream restoration. Stormwater retrofits include modification of existing stormwater structural practices to address both water quality and flow control. The majority of the sediment reductions required from the urban areas within the Gwynns Falls watershed are attributed to streambank erosion (see section 2.2.1). Therefore, flow controls must be installed to reduce sheer stress and limit bank erosion in order to address this portion of the urban sediment load. Additionally, impervious surface reduction results in a change in hydrology that could also reduce streambank erosion. In terms of upland urban sediment loads, stormwater retrofit reductions range from as low as 10% for dry detention to approximately 80% for wet ponds, wetlands, infiltration practices, and filtering practices (US EPA 2003). It is anticipated that the implementation of the TMDL will include the array of urban BMPs and practices outlined above. Implementation is expected to occur primarily via the MS4 permitting process for medium and large municipalities, which requires that these jurisdictions retrofit 10% of the existing urban land area every permit cycle, or 5 years.

It has been estimated that the average TSS removal efficiencies for BMPs installed between the years of 1985-2002 and post 2002, which are reflective of the stormwater management regulations in place during these time periods, is 50% and 80%, respectively (Claytor and Schueler 1997; Baldwin et al. 2007; Baish and Caliri 2009). Based on these average TSS reduction efficiencies, BMP specific reduction efficiencies as estimated by

FINAL

CBP, and best professional judgment, MDE estimates that future stormwater retrofits, which are expected to be implemented as part of the 10% retrofit goal to existing urban land every 5 years, will have approximately a 65% reduction efficiency for TSS, which is subject to change over time. Additionally, any new development in the watershed will be subject to the Stormwater Management Act of 2007 and will be required to use environmental site design (ESD) to the maximum extent practicable.

All non-forested land uses can benefit from improved riparian buffer systems. A riparian buffer reduces the effects of upland sediment sources through trapping and filtering. Riparian buffer efficiencies vary depending on type (grass or forested), land use (urban or agriculture), and physiographic region. The CBP estimates riparian buffer sediment reduction efficiencies in the Gwynns Falls region to be approximately 50% (US EPA 2006). Additionally, reforestation, whether adjacent to part of the watershed stream system or in a watershed's interior, can decrease upland sediment sources as well.

In summary, through the use of the aforementioned funding mechanisms and best management practices, there is reasonable assurance that this TMDL can be implemented.

FINAL

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APPENDIX A – Watershed Characterization Data

Table A-1: Reference Watersheds

| MD 8-digit Name | MD 8-digit | Percent stream mile degraded (%)^{1,2} | Forest Normalized Sediment Load³ |
|------------------------|-------------------|---|--|
| Deer Creek | 02120202 | 11 | 3.9 |
| Broad Creek | 02120205 | 12 | 4.5 |
| Little Gunpowder Falls | 02130804 | 15 | 3.3 |
| Prettyboy Reservoir | 02130806 | 16 | 3.7 |
| Middle Patuxent River | 02131106 | 20 | 3.2 |
| Brighton Dam | 02131108 | 11 | 4.2 |
| Sideling Creek | 02140510 | 20 | 1.9 |
| Fifteen Mile Creek | 02140511 | 4 | 1.6 |
| Savage River | 02141006 | 7 | 2.5 |
| Median | | | 3.3 |
| 75th | | | 4.2 |

- Notes:**
- ¹Percent stream miles degraded within an 8-digit watershed is based on the percentage of impaired MBSS stations within the watershed (MDE 2008).
 - ²The percent stream miles degraded threshold to determine if an 8-digit watershed is impaired for impacts to biological communities is based on a comparison to reference conditions (MDE 2008).
 - ³Forest normalized sediment loads based on Maryland watershed area only (consistent with MBSS random monitoring data).

APPENDIX B – MDE Permit Information

Table B-1: Permit Summary

| Permit # | NPDES | Facility | County | City | Type | TMDL |
|----------|-----------|--|------------------|--------------|--------|-------------------|
| 04DP0681 | MD0003034 | ASHBURTON WATER FILTRATION PLANT | BALTIMORE CITY | BALTIMORE | WMA2M | Process Water WLA |
| 00MM0975 | MDG490975 | ARUNDEL CORPORATION - DELIGHT QUARRY | BALTIMORE COUNTY | REISTERSTOWN | WMA5 | Process Water WLA |
| 00MM9722 | MDG499722 | LARRY E. KNIGHT, INC. | BALTIMORE COUNTY | GLYNDON | WMA5 | Process Water WLA |
| 00MM9831 | MDG499831 | S & G CONCRETE - GRANTLEY | BALTIMORE CITY | BALTIMORE | WMA5 | Process Water WLA |
| 00MM9866 | MDG499866 | AJO CONCRETE CONTRACTING, INC | BALTIMORE CITY | BALTIMORE | WMA5 | Process Water WLA |
| 02SW0025 | | SOLO CUP OPERATING CORPORATION (SCOC) | BALTIMORE COUNTY | OWINGS MILLS | WMA5SW | Stormwater WLA |
| 02SW0034 | | FOUNDRY SERVICE & SUPPLY CO., INC. | BALTIMORE COUNTY | PIKESVILLE | WMA5SW | Stormwater WLA |
| 02SW0155 | | NURAD TECHNOLOGIES, INC. | BALTIMORE CITY | BALTIMORE | WMA5SW | Stormwater WLA |
| 02SW0306 | | QUEST INTERNATIONAL FLAVORS & FOOD INGREDIENTS | BALTIMORE COUNTY | OWINGS MILLS | WMA5SW | Stormwater WLA |
| 02SW0659 | | PITT OHIO EXPRESS, INC. - BALTIMORE | BALTIMORE CITY | BALTIMORE | WMA5SW | Stormwater WLA |
| 02SW0703 | | BALTIMORE CITY DPW - WESTERN SUBSTATION | BALTIMORE CITY | BALTIMORE | WMA5SW | Stormwater WLA |
| 02SW0705 | | BALTIMORE CITY DPW - NORTHWESTERN SUBSTATION | BALTIMORE CITY | BALTIMORE | WMA5SW | Stormwater WLA |
| 02SW0712 | | NEW ENGLAND MOTOR FREIGHT | BALTIMORE CITY | BALTIMORE | WMA5SW | Stormwater WLA |
| 02SW0739 | | RUBBER MILLERS, INC. | BALTIMORE CITY | BALTIMORE | WMA5SW | Stormwater WLA |
| 02SW0777 | | EMANUEL TIRE COMPANY-MORELAND | BALTIMORE CITY | BALTIMORE | WMA5SW | Stormwater WLA |
| 02SW0779 | | SAFETY-KLEEN SYSTEMS, INC. - BALTIMORE | BALTIMORE CITY | BALTIMORE | WMA5SW | Stormwater WLA |
| 02SW0805 | | GEORGE G. RUPPERSBERGER & SONS, INC. | BALTIMORE CITY | BALTIMORE | WMA5SW | Stormwater WLA |

FINAL

| Permit # | NPDES | Facility | County | City | Type | TMDL |
|----------|-------|---|------------------|--------------|--------|----------------|
| 02SW0848 | | UNITED PARCEL SERVICE - VERO ROAD | BALTIMORE COUNTY | BALTIMORE | WMA5SW | Stormwater WLA |
| 02SW0864 | | P. FLANIGAN & SONS INC. - WESTPORT | BALTIMORE CITY | BALTIMORE | WMA5SW | Stormwater WLA |
| 02SW0868 | | BALTIMORE CONCRETE PRODUCTS, INC. | BALTIMORE CITY | BALTIMORE | WMA5SW | Stormwater WLA |
| 02SW0930 | | ESTES EXPRESS LINES | BALTIMORE CITY | BALTIMORE | WMA5SW | Stormwater WLA |
| 02SW1014 | | P. FLANIGAN & SONS, INC. | BALTIMORE CITY | BALTIMORE | WMA5SW | Stormwater WLA |
| 02SW1016 | | CAPITOL CAKE COMPANY | BALTIMORE CITY | BALTIMORE | WMA5SW | Stormwater WLA |
| 02SW1027 | | NATIONAL INSTRUMENT COMPANY, INC. | BALTIMORE CITY | BALTIMORE | WMA5SW | Stormwater WLA |
| 02SW1053 | | LIGON AND LIGON, INC. | BALTIMORE CITY | BALTIMORE | WMA5SW | Stormwater WLA |
| 02SW1137 | | WOODLAWN MOTOR COACH, INC. | BALTIMORE COUNTY | BALTIMORE | WMA5SW | Stormwater WLA |
| 02SW1138 | | ALL SUPPLIES & PARTS, INC. - ASAP COMPRESSORS | BALTIMORE CITY | BALTIMORE | WMA5SW | Stormwater WLA |
| 02SW1206 | | TRIFINITY MANUFACTURING BALTIMORE, LLC | BALTIMORE CITY | BALTIMORE | WMA5SW | Stormwater WLA |
| 02SW1216 | | UNITED IRON AND METAL, LLC | BALTIMORE CITY | BALTIMORE | WMA5SW | Stormwater WLA |
| 02SW1248 | | POTTS & CALLAHAN, INC. - GWYNN'S FALLS | BALTIMORE CITY | BALTIMORE | WMA5SW | Stormwater WLA |
| 02SW1272 | | UNILEVER BESTFOODS NORTH AMERICA | BALTIMORE CITY | BALTIMORE | WMA5SW | Stormwater WLA |
| 02SW1297 | | WINCHESTER HOMES, INC. | BALTIMORE CITY | BALTIMORE | WMA5SW | Stormwater WLA |
| 02SW1307 | | NORTHWEST TRANSFER STATION | BALTIMORE CITY | BALTIMORE | WMA5SW | Stormwater WLA |
| 02SW1375 | | MR. MARTIN L. REESE | BALTIMORE CITY | BALTIMORE | WMA5SW | Stormwater WLA |
| 02SW1398 | | DANIEL G. SCHUSTER, LLC. - OWINGS MILLS | BALTIMORE COUNTY | OWINGS MILLS | WMA5SW | Stormwater WLA |
| 02SW1492 | | CRUSADER CHEMICAL COMPANY, INC. | BALTIMORE CITY | BALTIMORE | WMA5SW | Stormwater WLA |

FINAL

| Permit # | NPDES | Facility | County | City | Type | TMDL |
|----------|-----------|--|------------------|--------------|--------|----------------|
| 02SW1495 | | CARROLL AWNING COMPANY, INC. | BALTIMORE CITY | BALTIMORE | WMA5SW | Stormwater WLA |
| 02SW1563 | | CHEMLIME N.J., INC. | BALTIMORE COUNTY | BALTIMORE | WMA5SW | Stormwater WLA |
| 02SW1656 | | JOE CORBI'S WHOLESALE PIZZA | BALTIMORE CITY | BALTIMORE | WMA5SW | Stormwater WLA |
| 02SW1657 | | ALPHARMA USHP - BALTIMORE | BALTIMORE COUNTY | BALTIMORE | WMA5SW | Stormwater WLA |
| 02SW1673 | | MTA - NORTHEAST MAINTENANCE SHOP | BALTIMORE CITY | BALTIMORE | WMA5SW | Stormwater WLA |
| 02SW1677 | | MTA - NORTHWEST BUS DIVISION | BALTIMORE CITY | BALTIMORE | WMA5SW | Stormwater WLA |
| 02SW1716 | | SHIRE U.S. MANUFACTURING, INC. | BALTIMORE COUNTY | OWINGS MILLS | WMA5SW | Stormwater WLA |
| 02SW1778 | | TRIAD INCORPORATED | BALTIMORE CITY | BALTIMORE | WMA5SW | Stormwater WLA |
| 02SW1836 | | PATUXENT MATERIALS, INC. - BALTIMORE | BALTIMORE CITY | BALTIMORE | WMA5SW | Stormwater WLA |
| 02SW1884 | | CRISPY BAGEL COMPANY | BALTIMORE CITY | BALTIMORE | WMA5SW | Stormwater WLA |
| 02SW1912 | | DECKER'S SALVAGE COMPANY, INC | BALTIMORE CITY | BALTIMORE | WMA5SW | Stormwater WLA |
| 02SW1964 | | BALTIMORE COUNTY BUREAU OF HIGHWAYS - SHOP 2 | BALTIMORE COUNTY | BALTIMORE | WMA5SW | Stormwater WLA |
| 02SW1978 | | P & J CONTRACTING COMPANY, INC. | BALTIMORE CITY | BALTIMORE | WMA5SW | Stormwater WLA |
| 02SW1992 | | BEVERAGE CAPITAL CORPORATION | BALTIMORE COUNTY | BALTIMORE | WMA5SW | Stormwater WLA |
| 02SW1996 | | MTA - OLD COURT METRO MAINTENANCE FACILITY | BALTIMORE COUNTY | PIKESVILLE | WMA5SW | Stormwater WLA |
| 02SW2009 | | SHA - OWINGS MILLS SHOP | BALTIMORE COUNTY | OWINGS MILLS | WMA5SW | Stormwater WLA |
| 02SW3031 | | RALOID CORPORATION | BALTIMORE COUNTY | REISTERSTOWN | WMA5SW | Stormwater WLA |
| 05DP3317 | MD0068314 | BALTIMORE COUNTY MS4 | BALTIMORE | COUNTY-WIDE | WMA6 | Stormwater WLA |
| 99DP3315 | MD0068292 | BALTIMORE CITY MS4 | BALTIMORE CITY | CITY-WIDE | WMA6 | Stormwater WLA |
| 99DP3313 | MD0068276 | STATE HIGHWAY ADMINSTRATION MS4 | ALL PHASE I | STATE-WIDE | WMA6 | Stormwater WLA |

FINAL

| Permit # | NPDES | Facility | County | City | Type | TMDL |
|-----------------|--------------|---------------------------------|---------------|-------------|-------------|----------------|
| | | MDE GENERAL PERMIT TO CONSTRUCT | ALL | ALL | | Stormwater WLA |

Notes: ¹TMDL column identifies how the permit was considered in the TMDL allocation.

²WTP = Water Treatment Plant

³WWTP = Wastewater Treatment Plant

FINAL

Table B-2: Municipal Permit Data

| Facility name | NPDES # | MDE Permit # | Flow (MGD¹) | Permit Avg Monthly Conc. (mg/l²) | Permit Avg. Weekly Conc. (mg/l) |
|----------------------------------|----------------|---------------------|-------------------------------|--|--|
| ASHBURTON WATER FILTRATION PLANT | MD0003034 | 04DP0681 | 7.0 | 20 | 30 |

Table B-3: General Mine Permit Data

| Facility name | NPDES # | MDE Permit # | Flow (MGD) | Permit Avg Quarterly Conc. (mg/l) | Permit Daily Max Conc. (mg/l) |
|--------------------------------------|----------------|---------------------|-------------------|--|--------------------------------------|
| ARUNDEL CORPORATION - DELIGHT QUARRY | MDG490975 | 00MM0975 | 0.001 | 30 | 66 |
| LARRY E. KNIGHT, INC. | MDG499722 | 00MM9722 | 0.001 | 30 | 60 |
| S & G CONCRETE - GRANTLEY | MDG499831 | 00MM9831 | 0.005 | 30 | 60 |
| AJO CONCRETE CONTRACTING, INC | MDG499866 | 00MM9866 | 0.001 | 30 | 60 |

Table B-4: Stormwater Permits¹

| Permit # | Facility | NPDES Group |
|-----------------|--|--------------------|
| 02SW0025 | SOLO CUP OPERATING CORPORATION (SCOC) | Phase I |
| 02SW0034 | FOUNDRY SERVICE & SUPPLY CO., INC. | Phase I |
| 02SW0155 | NURAD TECHNOLOGIES, INC. | Phase I |
| 02SW0306 | QUEST INTERNATIONAL FLAVORS & FOOD INGREDIENTS | Phase I |
| 02SW0659 | PITT OHIO EXPRESS, INC. - BALTIMORE | Phase I |
| 02SW0703 | BALTIMORE CITY DPW - WESTERN SUBSTATION | Phase I |
| 02SW0705 | BALTIMORE CITY DPW - NORTHWESTERN SUBSTATION | Phase I |
| 02SW0712 | NEW ENGLAND MOTOR FREIGHT | Phase I |
| 02SW0739 | RUBBER MILLERS, INC. | Phase I |
| 02SW0777 | EMANUEL TIRE COMPANY-MORELAND | Phase I |
| 02SW0779 | SAFETY-KLEEN SYSTEMS, INC. - BALTIMORE | Phase I |
| 02SW0805 | GEORGE G. RUPPERSBERGER & SONS, INC. | Phase I |
| 02SW0848 | UNITED PARCEL SERVICE - VERO ROAD | Phase I |
| 02SW0864 | P. FLANIGAN & SONS INC. - WESTPORT | Phase I |
| 02SW0868 | BALTIMORE CONCRETE PRODUCTS, INC. | Phase I |
| 02SW0930 | ESTES EXPRESS LINES | Phase I |
| 02SW1014 | P. FLANIGAN & SONS, INC. | Phase I |
| 02SW1016 | CAPITOL CAKE COMPANY | Phase I |
| 02SW1027 | NATIONAL INSTRUMENT COMPANY, INC. | Phase I |
| 02SW1053 | LIGON AND LIGON, INC. | Phase I |
| 02SW1137 | WOODLAWN MOTOR COACH, INC. | Phase I |
| 02SW1138 | ALL SUPPLIES & PARTS, INC. - ASAP COMPRESSORS | Phase I |
| 02SW1206 | TRIFINITY MANUFACTURING BALTIMORE, LLC | Phase I |
| 02SW1216 | UNITED IRON AND METAL, LLC | Phase I |
| 02SW1248 | POTTS & CALLAHAN, INC. - GWYNN'S FALLS | Phase I |
| 02SW1272 | UNILEVER BESTFOODS NORTH AMERICA | Phase I |
| 02SW1297 | WINCHESTER HOMES, INC. | Phase I |
| 02SW1307 | NORTHWEST TRANSFER STATION | Phase I |
| 02SW1375 | MR. MARTIN L. REESE | Phase I |

FINAL

| Permit # | Facility | NPDES Group |
|-----------------|---|--------------------|
| 02SW1398 | DANIEL G. SCHUSTER, LLC. - OWINGS MILLS | Phase I |
| 02SW1492 | CRUSADER CHEMICAL COMPANY, INC. | Phase I |
| 02SW1495 | CARROLL AWNING COMPANY, INC. | Phase I |
| 02SW1563 | CHEMLIME N.J., INC. | Phase I |
| 02SW1656 | JOE CORBI'S WHOLESALE PIZZA | Phase I |
| 02SW1657 | ALPHARMA USHP - BALTIMORE | Phase I |
| 02SW1673 | MTA - NORTHEAST MAINTENANCE SHOP | Phase I |
| 02SW1677 | MTA - NORTHWEST BUS DIVISION | Phase I |
| 02SW1716 | SHIRE U.S. MANUFACTURING, INC. | Phase I |
| 02SW1778 | TRIAD INCORPORATED | Phase I |
| 02SW1836 | PATUXENT MATERIALS, INC. - BALTIMORE | Phase I |
| 02SW1884 | CRISPY BAGEL COMPANY | Phase I |
| 02SW1912 | DECKER'S SALVAGE COMPANY, INC | Phase I |
| 02SW1964 | BALTIMORE COUNTY BUREAU OF HIGHWAYS - SHOP 2 | Phase I |
| 02SW1978 | P & J CONTRACTING COMPANY, INC. | Phase I |
| 02SW1992 | BEVERAGE CAPITAL CORPORATION | Phase I |
| 02SW1996 | MTA - OLD COURT METRO MAINTENANCE FACILITY | Phase I |
| 02SW2009 | SHA - OWINGS MILLS SHOP | Phase I |
| 02SW3031 | RALOID CORPORATION | Phase I |
| 05DP3317 | BALTIMORE COUNTY MUNICIPAL SEPARATE STORM SEWER | Phase I |
| 99DP3315 | BALTIMORE CITY MS4 | Phase I |
| 99DP3313 | STATE HIGHWAY ADMINISTRATION MS4 | Phase I |
| | MDE GENERAL PERMIT TO CONSTRUCT | Phase I/II |

Notes: ¹ Although not listed in this table, some individual permits from Tables B-2 and B-3 incorporate stormwater requirements and are accounted for within the NPDES stormwater WLA (specifically the “Other” Regulated Stormwater Allocation in the Technical Memorandum *Significant Sediment Point Sources in the Gwynns Falls Watershed* accompanying this TMDL report) as well additional Phase II permitted MS4s, such as military bases, hospitals, etc.

APPENDIX C – Technical Approach Used to Generate Maximum Daily Loads

Summary

This appendix documents the technical approach used to define maximum daily loads of sediment consistent with the average annual TMDL in the Gwynns Falls watershed, which is considered the maximum allowable load the watershed can sustain without causing any sediment related impacts to aquatic health. The approach builds upon the modeling analysis that was conducted to determine the sediment loadings and can be summarized as follows.

- The approach defines maximum daily loads for each of the source categories.
- The approach builds upon the TMDL modeling analysis that was conducted to ensure that average annual loading targets do not cause any sediment related impacts to aquatic health.
- The approach converts daily time-series loadings into TMDL values in a manner that is consistent with available EPA guidance on generating daily loads for TMDLs (US EPA 2007).
- The approach considers a daily load level of a resolution based on the specific data that exists for each source category.

Introduction

This appendix documents the development and application of the approach used to define maximum daily load values. It is divided into sections discussing:

- Basis for approach
- Options considered
- Selected approach
- Results of approach

Basis for approach

The overall approach for the development of daily loads was based upon the following factors:

- **Average Annual TMDL:** The basis of the average annual sediment TMDL is that cumulative high sediment loading rates have negative impacts on the biological community. Thus, the average annual sediment load was calculated so as to not cause any sediment related impacts to aquatic health.
- **CBP P5 Watershed Model Sediment Loads:** There are two spatial calibration points for sediment within the CBP P5 watershed model framework. First, EOS loads are calibrated to long term EOS target loads. These target loads are the loads used to determine an average annual TMDL. Furthermore, the target loads were used in the TMDL because, as calibration targets, they are expected to

FINAL

remain relatively unchanged during the final calibration stages of the CBP P5 model, and therefore will be the most consistent with the final CBP P5 watershed model sediment loading estimates. Currently, the CBP P5 model river segments are being calibrated to daily monitoring information for watersheds with a flow greater than 100 cfs, or an approximate area of 100 square miles.

- **Draft EPA guidance document entitled “Developing Daily Loads for Load-based TMDLs”:** This guidance document provides options for defining maximum daily loads when using TMDL approaches that generate daily output (US EPA 2007).

The rationale for developing TMDLs expressed as *daily* loads was to accept the existing average annual TMDL, but then develop a method for converting this number to a maximum *daily* load – in a manner consistent with EPA guidance and available information.

Options considered

The draft EPA guidance document for developing daily loads does not specify a single approach that must be adhered to, but rather it contains a range of acceptable options (US EPA 2007). The selection of a specific method for translating a time-series of allowable loads into the expression of a TMDL requires decisions regarding both the level of resolution (e.g., single daily load for all conditions vs. loads that vary with environmental conditions) and level of probability associated with the TMDL.

This section describes the range of options that were considered when developing methods to calculate Gwynns Falls Maximum Daily Loads.

Level of Resolution

The level of resolution pertains to the amount of detail used in specifying the maximum daily load. The draft EPA guidance document on daily loads provides three categories of options for level of resolution, all of which are potentially applicable for the Gwynns Falls watershed:

1. **Representative daily load:** In this option, a single daily load (or multiple representative daily loads) is specified that covers all time periods and environmental conditions.
2. **Flow-variable daily load:** This option allows the maximum daily load to vary based upon the observed flow condition.
3. **Temporally-variable daily load:** This option allows the maximum daily load to vary based upon seasons or times of varying source or water body behavior (US EPA 2007).

FINAL

Probability Level

All TMDLs have some probability of being exceeded, with the specific probability being either explicitly specified or implicitly assumed. This level of probability directly or indirectly reflects two separate phenomena:

1. Water quality criteria consist of components describing acceptable magnitude, duration, and frequency. The frequency component addresses how often conditions can allowably surpass the combined magnitude and duration components.
2. Pollutant loads, especially from wet weather sources, typically exhibit a large degree of variability over time. It is rarely practical to specify a “never to be exceeded value” for a daily load, as essentially any loading value has some finite probability of being exceeded.

The draft daily load guidance document states that the probability component of the maximum daily load should be “based on a representative statistical measure” that is dependent upon the specific TMDL and the best professional judgment of the developers (US EPA 2007). This statistical measure represents how often the maximum daily load is expected/allowed to be exceeded. The primary options for selecting this level of protection would be:

1. **The maximum daily load reflects some central tendency:** In this option, the maximum daily load is based upon the mean or median value of the range of loads expected to occur. The variability in the actual loads is not addressed.
2. **The maximum daily load reflects a level of protection implicitly provided by the selection of some “critical” period:** In this option, the maximum daily load is based upon the allowable load that is predicted to occur during some critical period examined during the analysis. The developer does not explicitly specify the probability of occurrence.
3. **The maximum daily load is a value that will be exceeded with a pre-defined probability:** In this option, a “reasonable” upper bound percentile is selected for the maximum daily load based upon a characterization of the variability of daily loads. For example, selection of the 95th percentile value would result in a maximum daily load that would be exceeded 5% of the time.

Selected Approach

The approach selected for defining a Gwynns Falls Maximum Daily Load was based upon the specific data that exists for each source category. The approach consists of unique methods for each of the following categories of sources:

- Approach for Nonpoint Sources and Stormwater Point Sources within the Gwynns Falls watershed
- Approach for Process Water Point Sources within the Gwynns Falls watershed

FINAL

Approach for Nonpoint Sources and Stormwater Point Sources within the Gwynns Falls watershed

The level of resolution selected for the Gwynns Falls Maximum Daily Load was a representative daily load, expressed as a single daily load for each loading source. This approach was chosen based upon the specific data that exists for nonpoint sources and stormwater point sources within the Gwynns Falls watershed. Currently, the best available data is the CBP P5 model daily time series calibrated to long-term average annual loads (per landuse). The CBP reach simulation results are calibrated to daily monitoring information for watershed segments with a flow typically greater than 100 cfs, but they have not been through appropriate peer review. Therefore, it was concluded that it would not be appropriate to apply the absolute values of the reach simulation model results to the TMDL, and the annual loads were used instead. However, it was assumed that the distribution of the daily values was correct, in order to calculate a normalized statistical parameter to estimate the maximum daily loads.

The maximum daily load was estimated based on three factors: a specified probability level, the average annual sediment TMDL, and the coefficient of variation (CV) of the CBP P5 Gwynns Falls reach simulation daily loads. The probability level (or exceedance frequency) is based upon guidance from EPA (US EPA 1991) where examples suggest that when converting from a long-term average to a daily value, the z-score corresponding to the 99th percentile of the log-normal probability distribution should be used. The average annual sediment TMDL is estimated from the CBP P5 EOS target loads. The calculation of the CV is described below.

The CBP P5 Gwynns Falls reach simulation consisted of a daily time series beginning in 1985 and extending to the year 2005. The CV was estimated by first converting the daily sediment load values to a log distribution and then verifying that the results approximated the normal distribution (see Figure C-1). Next, the CV was calculated using the arithmetic mean and standard deviation results from the log transformation. The log-transformed values were used to reduce the possible influence of outliers. The resulting CV of 15.4 was calculated using the following equation:

$$CV = \frac{\beta}{\alpha} \quad \text{(Equation C.1)}$$

where:

CV = coefficient of variation

$$\beta = \alpha \sqrt{e^{\sigma^2} - 1}$$

$$\alpha = e^{(\mu + 0.5 \cdot \sigma^2)}$$

α = mean (arithmetic)

β = standard deviation (arithmetic)

μ = mean of logarithms

σ = standard deviation of logarithms

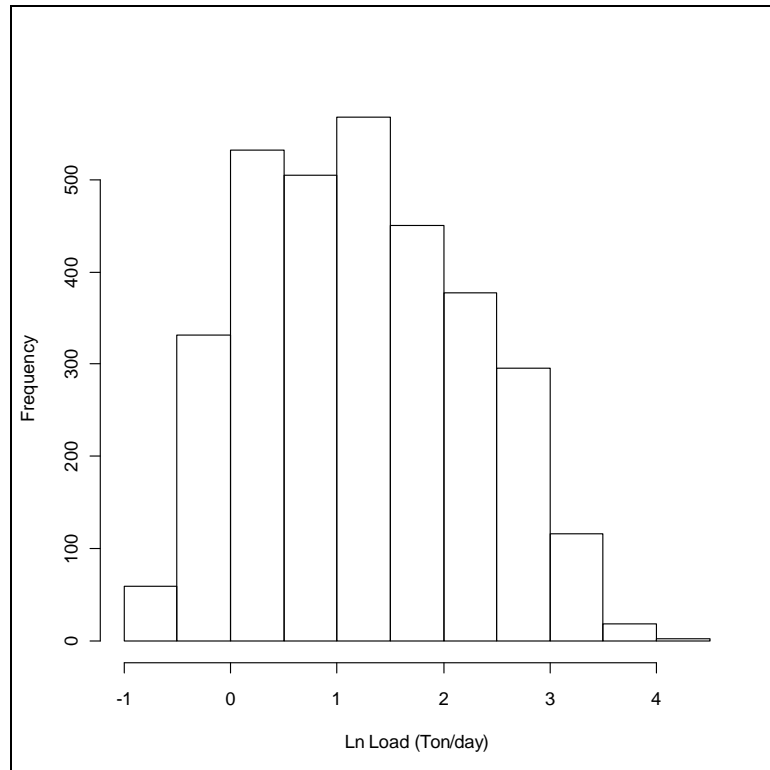


Figure C-1: Histogram of CBP River Segment Daily Simulation Results for the Gwynns Falls Watershed

The maximum “daily” load for each contributing source is estimated as the long-term average annual load multiplied by a factor that accounts for expected variability of daily loading values. The equation is as follows:

$$MDL = LTA * e^{(z\sigma - 0.5\sigma^2)} \quad \text{(Equation C.2)}$$

where:

MDL = Maximum daily load

LTA = Long term average (average annual load)

Z = z-score associated with target probability level

$\sigma = \ln(CV^2 + 1)$

CV = Coefficient of variation based on arithmetic mean and standard deviation

Using a z-score associated with the 99th percent probability, a CV of 15.4, and consistent units, the resulting dimensionless conversion factor from long term average annual loads to a maximum daily load is 14.96. The average annual Gwynns Falls TMDL of sediment/TSS is reported in ton/year, and the conversion from ton/year to a maximum daily load in ton/day is 0.04 (e.g. 14.96/365)

Approach for Process Water Point Sources within the Gwynns Falls watershed

The TMDL also considers contributions from other point sources (i.e., sources other than stormwater point sources) in the watershed that have NPDES permits with sediment

FINAL

limits. As these sources are generally minor contributors to the overall sediment load, the TMDL analysis that defined the average annual TMDL did not propose any reductions for these sources and held each of them constant at their existing technology-based NPDES permit monthly (or daily if monthly was not specified) limit for the entire year.

The approach used to determine maximum daily loads for these sources was dependent upon whether a maximum daily load was specified within the permit. If a maximum daily limit was specified, then the reported average flow was multiplied by the daily maximum limit to obtain a maximum daily load. If a maximum daily limit was not specified, the maximum daily loads were calculated based on the guidance provided in the Technical Support Document (TSD) for Water Quality-based Toxics Control (US EPA 1991). The long-term average annual TMDL was converted to maximum daily limits using Table 5-2 of the TSD assuming a coefficient of variation of 0.6 and a 99th percentile probability. This results in a dimensionless multiplication factor of 3.11. The average annual Gwynns Falls TMDL of sediment/TSS is reported in ton/yr, and the conversion from ton/yr to a maximum daily load in ton/day is 0.0085 (e.g. 3.11/365)

Results of approach

This section lists the results of the selected approach to define the Gwynns Falls Maximum Daily Loads.

- Calculation Approach for Nonpoint Sources and Stormwater Point Sources within the Gwynns Falls watershed

$$LA_{GF} \text{ (Ton/day)} = \text{Average Annual TMDL } LA_{GF} \text{ (ton/yr)} * .04$$

$$\text{Stormwater } WLA_{GF} \text{ (Ton/day)} = \text{Average Annual TMDL Stormwater } WLA_{GF} \text{ (ton/yr)} * .04$$

- Calculation Approach for Process Water Point Sources within the Gwynns Falls watershed

- For permits with a daily maximum limit:

$$\text{Process Water } WLA_{GF} \text{ (ton/day)} = \text{Permit flow (mgd)} * \text{Daily maximum permit limit(mg/l)} * 0.0042$$

- For permits without a daily maximum limit:

$$\text{Process Water } WLA_{GF} \text{ (Ton/day)} = \text{Average Annual TMDL } WLA_{GF} \text{ Other (ton/yr)} * 0.0085$$

Table C-1: Gwynns Falls Maximum Daily Loads of Sediment/TSS (ton/day)

| MDL (ton/day) | = | LA_{GF} | + | NPDES Stormwater WLA_{GF} | + | Process Water WLA_{GF} | + | MOS |
|----------------------|----------|------------------------|----------|--|----------|---|----------|------------|
| 558.7 | = | 70.4 | + | 486.5 | + | 1.82 | + | Implicit |