VARYLAND DAM SARETY

Dam Break Analysis



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Embankment Dam Schematic





Dam Overtopping Photo 1



Dam Overtopping Photo 2



Overtopping Breach of Earth Dam

Initial Breach













Piping Failure for Earth Dam



Piping Failure at Loveton Dam (1989)



Loveton Dam Failure (1989)



Loveton Failure Viewed from Downstream



Medford Quarry Wash Pond Piping Failure



Piping Failure

Anti-seep collars do not prevent seepage failures!

Annap. Mall Piping Failure



Sinkhole in Dam Crest



TYPICAL PROBLEMS



Pipe Installation in Dam

Dam Embankment Flowable Fill Filter Diaphragm



FILTER DIAPHRAGM



Foundation Failure



Slope Failure



Structural Failure





Overtopping Piping Foundation Other

Dam Hazard Classifications



Significant Hazard = Class "b"

• High Hazard = Class "c"

MDE Dam Hazard Classifications

- Low Hazard Potential loss of life is very unlikely due to low danger flood depths.
- Significant Hazard Potential loss of life is possible with no more than 6 lives in jeopardy and flooding to no more than two isolated houses and downstream roads.
- High Hazard Potential loss of life is very likely with more than 6 lives in jeopardy, and serious damage to residential, commercial, or industrial buildings, and downstream roads.





Probable Maximum Flood (PMF)

PMF - the largest flood considered possible based on the most severe combination of meteorological and hydrologic conditions that are reasonably possible.



WORLD RECORD RAINFALL AMOUNTS

SOURCE: JENNINGS, A. H. WORLD'S GREATEST OBSERVED POINT RAINFALL. MONTHLY WEATHER REV., VOL 78, 1950

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Rainfall Greater than 50% PMP


Increased Flood Risks



- HEC-1 Computer Model
 - Develop & Route Hydrographs
 - Fail Dam with NWS Dam Break Method
 - Route Breach Hydrograph
 Downstream
 - Route Through & Over Downstream Roads or Dams

Breach Parameters for HEC-1 Model

- Breach Bottom Elevation
- Breach Top Elevation (Trigger Elevation)
- Bottom Breach Width
- Breach Side Slope
- Time of Failure
- HEC-HMS New Windows Model

Breach Parameters

Trigger Elevation for Failure



Bottom Width, b

Breach Photo

Breach Shape



Suggested Breach Parameters for Earth Dams

Source	Average Breach Width (ft)	Breach Side Slope (1V:ZH)	Breach Failure Time (hrs)
NWS (1988)	1H to 5H	Z = 0 to 1	0.1 to 2.0
COE (1980)	0.5H to 4H	Z = 0 to 1	0.5 to 4
FERC (1991)	1H to 5H	Z = 0 to 1	0.1 to 1.0
USBR (1982)	3H	N/A	0.00333b
Boss Dambrk (1988)	0.5 to 4H	Z= 0 to 1	0.5 to 4
Harrington (1999)	1H to 8H	Z= 0 to 1	H/120 to H/180

Froelich Breach Predictor Equations $b = 9.5 K_0 (V_s H)^{0.25}$ $\tau = 0.59 (V_s^{0.47}) H^{-0.91}$

- **b** = Average Breach Width (ft),
 - = Time of Failure (hrs)
- **K**₀ = 0.7 for Piping & 1.0 for Overtopping Failure
- Vs = Storage Volume (ac-ft)
- H = Selected Failure Depth (ft) above Breach Bottom
- T = Time of Failure (hrs, ~H/120 or Minimum of 10 Min)

NWS Simple Dam Break Equation

 $Q_b = Q_0 + 3.1B_r (C/(T_f + C/\sqrt{H}))^3$

- **Q**_b = Breach + Non-Breach Flow (cfs)
- **Q**_o = Non-Breach Flow (cfs)
- **B**_r = Final Average Breach Width (ft, ~ 1H to 5H)
- C = 23.4 As/Br
- **A**_s = Reservoir Surface Area (ac) at Failure Elevation
- **H** = Selected Failure Depth (ft) above Final Breach Elevation
- **T_f = Time of Failure (hrs, ~H/120 or Minimum of 10 Min)**

NWS Simple DAMBRK Equation 100-Year Failure for Your Dam BREACH FLOW EQUATION: $Q_b = Q_0 + 3.1 Br(C/Tf + C/H^{1/2})^3$,

WHERE,

Q_b = BREACH FLOW + NON-BREACH FLOW (cfs)

Qo = NON-BREACH FLOW (cfs)

Br = FINAL AVERAGE BREACH WIDTH (ft, APPROX. 1H TO 5H)

C = 23.4*As/Br

As = RESERVOIR SURFACE AREA (ac) AT MAXIMUM POOL LEVEL

H = SELECTED FAILURE DEPTH (ft) ABOVE FINAL BREACH ELEVATION

Tf = TIME TO FAILURE (hrs, USE H/120 OR A MINIMUM OF 10 MIN)

INPUT VARIABLES:						
Qo =	0	cfs				
As =	5.00	ac				
H =	20.0	ft				

OUTP	UT VARIA	BLES:			
SELE	CTED	TIME		MAXIMUM	
BREA	СН	OF		BREACH	
WIDT	THS	FAILURE	COMPUTED	FLOW	
Br, [ft	1	T _f , [hrs]	C VALUE	Q _b ,[cfs]	
20.0	[H]	0.17	5.85	3844	
30.0	[1.5H]	0.17	3.90	4875	
40.0	[2H]	0.17	2.93	5545	
50.0	[2.5H]	0.17	2.34	5961	
60.0	[3H]	0.17	1.95	6196	
70.0	[3.5H]	0.17	1.67	6303	
80.0	[4.0H]	0.17	1.46	6318	
100.0	[5.0H]	0.17	1.17	6175	
35.4	Froelich	0.22	3.31	4508	<selected flow<="" th=""></selected>
35.4	Froelich	0.17		2847	= Vs/T _f

DEVELOPED BY BRUCE HARRINGTON, 9/92

BREACH PREDICTOR EQUATIONS

Recently some statistically derived predictors for average breach width (b) and time of failure (Tf) have been developed by MacDonald and Langridge-Monopolis (1984) and Froelich (1987,1995). From Froelich's work in which he used the properties of 63 breaches of dams ranging in height from 12 to 285 feet, with 6 dams greater than 100 feet, the following predictor equations were obtained:

b = 9.5Ko(VsH)^0.25

$T_f = 0.59(Vs^{47})/(H^{91})$

where,

b = average breach width (ft),
T_f = time of failure (hrs),
Ko = 0.7 for piping and 1.0 for overtopping failure
Vs = storage volume (ac-ft), and
H = height (ft) of water over breach bottom

BREACH WIDTH & TIME OF FAILURE FOR

NWS Simple DAMBRK Equation 100-Year Failure for Your Dam

INPUT VARIABLES:

OUTPUT PARAMETERS:

н =	20.0 ft
Vs =	40.0 ac-ft
Ko =	0.7

35.4	ft
0.22	hrs
	35.4 0.22

DEVELOPED BY BRUCE HARRINGTON, 9/92, REVISED 10/96

SCS (NRCS) Breach Formula

 $Q_{b} = 3.2 H^{5/2}$

- Usually Conservative Estimate of Breach
 Flow but not Always
- Storage Volume not included in Formula
- Similar to a V-Notch Weir Formula

COMPARISON OF DAM BREACH EQUATIONS NWS SIMPLE DAMBRK vs NRCS BREACH EQUATIONS

NWS SIMPLE DAMBRK EQUATION:

NRCS MD-378 EQUATION:

 $Q_{NRCS} = 3.2 H^{2.5}$

$$Q_{NWS} = 3.1B_r (C/T_f + C/\sqrt{H})^3$$

 $\begin{array}{l} Br = 3H \ (Breach Width, ft) \\ H = Height of Water at failure, ft \\ C = 23.4As/Br = 7.8As/H \\ As = Surface Area at Failure (acres) \\ T_f = H/120 \ (Failure Time, hrs) \\ = Minimum Time of 10 min = 0.17 hrs \end{array}$

H [ft]	As [ac]	T _f [hrs]	с	Q _{NWS} [cfs]	Q _{NRCS} [cfs]
5.0	0.3	0.17	0.47	88	179
5.0	1.0	0.17	1.56	270	179
5.0	5.0	0.17	7.80	451	179
10.0	0.3	0.17	0.23	79	1012
10.0	1.0	0.17	0.78	610	1012
10.0	5.0	0.17	3.90	1996	1012
15.0	0.5	0.17	0.26	184	2789
15.0	1.0	0.17	0.52	696	2789
15.0	5.0	0.17	2.60	4117	2789
20.0	1.0	0.17	0.39	648	5724
20.0	3.0	0.17	1.17	3705	5724
20.0	10.0	0 17	3 90	9750	5724
40.0	10.0	0.33	1.95	10605	32382
40-0	20-0	0.33	3.90	26012	32382
40-0-	40-0	0.33	7.80	46207	32382

NWS Simple Dam Break Equation

- Developed from NWS Full Dam Break Model
- Based on Falling Head Weir Flow
- Input Non-Breach Flow, Surface Area,
 Selected Failure Depth, & Time of Failure

NWS Simple Dam Break Model

- Easy to Use
- Uses NWS Simple Dam Break Equation for Breach Flow
- Uses Dynamic Routing of Flood Wave
- Input Downstream Cross Sections
- Will Not Route through Downstream Structures

NWS Full Dam Break Model (DAMBRK)

- Very Difficult to Learn & Temperamental
- Uses Unsteady State Dynamic Routing by a Finite Difference Technique
- Includes Pressure & Acceleration Effects
- A Hydrograph must be Inputted
- Has Been Replaced by NWS Flood Wave Model (FLDWAV), Free Download at: http://hsp.nws.noaa.gov/oh/hrl/rvrmech/rvrmain.htm

PRETTYBOY DAM DANGER REACH

A COMPARISON OF NWS DAMBRK & HEC-1 MODELS

Template Cross Sections

Miles	**** Discharge ****		**** Elevati	**** Elevation ****		
Below	NWS	HEC-1	NWS	HEC-1	Change	
Dam	[cfs]	[cfs]	[NGVD]	[NGVD]	[feet]	
Dam	509947	508554	538.1	538.1		
1.49	474643	477837	426.3	416.4	9.9	
5.37	414066	405271	390.3	388.2	2.1	
9.70	385871	364986	353.4	352.0	1.4	
14.20	349989	334765	326.0	310.5	15.5	
18.18	335059	299656	310.7	311.1	-0.4	

Recommended Dam Failure Methods for Small Dams < 15 feet High

- Use NWS SMPDBK and SCS Breach Equation to determine Breach Flows
- Use HECRAS Model to determine
 Downstream Flood Depths
- Stop Danger Reach when roads flood < 1.5 feet, and Flooding to Houses & Buildings < 6 inches

Recommended Dam Failure Methods for Dams > 15 & < 75 feet high

- Use Hec-1 Model for Breach Flows
- Use HECRAS Model to determine Downstream Flood Depths & USBR Hazard Charts to determine Flood Dangers
- Stop Danger Reach when Increased Flooding < 1 foot or no structures flooded

Recommended Dam Failure Methods for Dams > or = 75 feet high

- Use HMR-52 & HEC-1 Model for Hydrology
- Use DAMBRK or FLDWAV Model for Breach Flow
- Suggest Checking DAMBRK and FLDWAV Results with HECRAS Model

Flood Danger for Cars



■ Low Danger ■ Judgement Zone ■ High Danger

Flood Danger for Houses



Source: USBR Hazard Charts, 1988

Low Danger Judgement Zone High Danger

Flood Danger for Adults



Hurricane Floyd September 15-16, 1999

NANT GROWTH NANTE BLUE

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Rainfall from Hurricane Floyd, Sept 99



Hurricane Floyd Rainfall on Eastern Shore



Nagel Mill Dam before Floyd



Nagel Mill Dam after Floyd



Nagel Mill Dam after Floyd



Nagel Mill Dam after Repair



Nagels Breach Statistics

Piping Failure Breach Width = 60 ft = 4H Side Slope Z = 0.4 Time of Failure <20 min

Foreman Branch Dam before Floyd



Foreman Branch Dam after Floyd



Foreman Branch Dam after Floyd



Foreman Branch Dam after Repair



Foreman Dam Breach Statistics

Overtopping Failure Breach Width = 85 ft = 8H Side Slope Z = 0.5 Time of Failure <30 min

Frazer Mill Dam before Floyd


Frazer Mill Dam after Floyd



Frazer Mill Dam after Floyd



Frazer Dam Breach Statistics

Overtopping Failure Breach Width = 120 ft = 6H Side Slope Z = 0.6 Time of Failure Unknown

Jones Lake Dam before Floyd



Jones Lake Dam before Floyd



Jones Lake Dam after Floyd



Jones Lake Dam Breach Statistics

Piping Failure Breach Width = 103 ft = 6H Side Slope Z = 0.6 Failure Time Unknown

Sassafras Dam before Floyd



Sassafras Dam after Floyd



Sassafras Dam During Floyd



Sassafras Dam after Repair



Sassafras Dam During Repair



Sassafras Dam Breach Statistics

Overtopping Failure Breach Width = 47 ft = 4H Side Slope Z = 0.2 Failure Time = 15 Min

Stubbs Dam after Floyd



Stubbs Dam after Floyd



Stubbs Dam after Repair



Stubbs Dam Breach Statistics

Piping Failure Breach Width = 30 ft = 2.5H Side Slope Z = 0.2 Failure Time Unknown

Tuckahoe Dam after Floyd



Tuckahoe Breach below Spillway



St Pauls Emergency Spillway during Floyd



Boundary Dam Near Seattle Washington



Hoover Dam One of the "Seven Modern Civil Engineering Wonders"

Location: Black Canyon Arizona & Nevada

Owner: U.S. Bureau of Reclamation

Built: 1931-1935

<u>Height</u>: 726.4 ft. <u>Length</u>: 1244 ft. <u>Max. Depth</u>: 500 ft. <u>Storage</u>: 28,537,000 ac.-ft.

Introduction

- Purpose. The purpose of the Emergency Action Plan (EAP) is to safeguard lives and secondarily to reduce property damage in the event that (*your dam*) would fail. To carry out this mission, the EAP contains:
 procedures to monitor (*your dam*) periodically and during flood warnings issued by the National Weather Service; 2) notify (*County*) Emergency Operation Center of a potential dam failure; and 3) warn and evacuate the isolated residences at risk. These procedures are to supplement and be used in conjunction with (*your County's Emergency Operation Plan*).
- Flood Description. Failure of the dam could cause significant damage to (all roads and isolated residences downstream of your dam within the danger reach) located ____ miles downstream of (your dam).

OPERATING PROCEDURE

- I. The dam will be inspected periodically each year for maintenance and distress signals.
- II. The dam observer will inspect the dam when the National Weather Service issues a Flood Warning for the area and complete the following tasks.
 - 1. The dam observer will note & record water levels in reservoir and the rate at which the pool is rising.
 - 2. If the dam shows signs of internal piping (muddy seepage exiting the downstream embankment), erosion, slope failures, blocked spillways, or other ominous distress signs, the dam observer wil call the County Emergency Operation Center to send out police to roadblock downstream roads and warn any isolated residences in the danger reach. The dam observer may contact the Md Dam Safety Division or his designated engineer to provide assistance.
 - 3. If the pool level rises too within one foot (or other levels accepted by MDE) of the dam crest, the dam observer will contact the County Emergency Operations Center to dispatch police to roadblock downstream roads and warn any isolated residences in the danger reach.

DAM NAME

Signatures of Perso	Signatures of Persons Involved in Emergency Action Plan				
)am Owner 	By		Date		
	Typed Name:				
	Phone: (c)	lay) ight)			
ounty Department of	Ву	D	ate		
mergency Operations	True d Norres				
	Typed Name:				
	Phone: (d	av)			
	(1	ight)			
cal or State Police	Ву	D	ate		
arracks "?"					
	Typed Name: Title				
	Phone: (d	lay)			
	1)	ight)			
D Department of the Enviro	onment By		Date		
am Safety Division					
	Typed Name:	Brad Ia	rossi		
	Title:	Chief			
	Phone:	410-631-3538			
wner's Engineer	Bv		Date		

PREVENTATIVE ACTIONS

If time allows, contact your engineer (______) and the Maryland Dam Safety Division for advice on preventative actions. Listed below are potential emergency actions which may prevent or delay the failure of the dam. They should be considered based on site-specific conditions, as well as the risk of failure and risk to employees.

Possible Actions To Be Taken In The Event Of:

Imminent Overtopping by Flood Waters:

- 1) Open drain or flood gates to maximum capacity.
- 2) Place sand bags along the dam crest to increase freeboard.
- 3) Place riprap or sandbags in damaged areas of dam.
- Provide erosion protection on downstream slope by placing riprap or other appropriate materials.
- Divert flood waters around dam if possible (such as emergency spillway)

Erosion of Dam by Seepage Through the Embankment, Foundation, or Abutments:

- Plug the seepage with appropriate material such as (riprap, hay bales, bentonite, sandbags, soil, or plastic sheeting if the leak is on upstream face of dam).
- Lower the reservoir level until the flow decreases to a nonerosive velocity or stops leaking.
- Place a sand and gravel filter over the seepage exit area to minimize loss of embankment soils.
- Continue lowering the reservoir level until the seepage stops or is controlled. Refill reservoir to normal levels only after seepage is repaired.

Slide or Slope Failure on Upstream or Downstream Slope of Embankment:

 Lower the reservoir water level at a rate, and to an elevation that is considered safe. Contact your engineer or the Dam Safety

SUPPLIES AND RESOURCES

In an emergency situation, equipment and supplies may be needed on short notice. The following supplies and resources may be needed during an emergency: earthmoving equipment, sand and gravel, sandbags, riprap, pumps, pipe, laborers.

List of Contractors

It will be the responsibility of the owner to maintain the list of contractors that may be contacted during an emergency condition f equipments, materials, and repairs.

For each contractor on the list, the following information is needed:

- Contractor name
- Contact person.
- Address.
- Phone number.
- Equipment & repair supplies available.
- Arrival time to dam

1.	Contractor:				
	Contact person:	Phone No:			
	Address:				
	Services contracted for:				

2. Contractor:

Address:		

DANGER REACH MAP

EVACUATION ROUTES



MDE Dam Break Web Site ftp://ftp.mde.state.md.us/outgoing/Dam_Safety/

Microsoft Word - Model Emergency Action Plans **Hazard Guidelines**

Microsoft Excel Spreadsheets

> **Executable Programs**

- **NWS Dam Break Equation**
- USBR Hazard Graphs
- Hydrology Spreadsheets
- Hydraulic Spreadsheets
- HEC-1 Program
- NWS Simple Dam Break Program
- Sample Data for HEC-1 & NWS **Simple Dam Break**

Any Questions?



Bruce Harrington, MD Dam Safety, 410-334-3411