PRE-DESIGN INVESTIGATION ROD AND WIRE MILL AREA CHARACTERIZATION REPORT

AREA A: PARCEL A3 TRADEPOINT ATLANTIC SPARROWS POINT, MARYLAND

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Revision 0 – June 10, 2016

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1.0 INTRODUCTION

ARM Group Inc. (ARM), on behalf of EnviroAnalytics Group (EAG), has completed a Pre-Design Investigation (PDI) within a portion of Parcel A3 of the Tradepoint Atlantic property (formerly Sparrows Point Terminal, LLC). Parcel A3 is comprised of 64 acres of the approximately 3,100-acre former steel making facility (**Figure 1**). The portion that is the focus of this PDI includes the northernmost 15 acres that is currently undergoing groundwater interim remedial measures (Site). The Site is bounded to the west by Riverside Drive and Bear Creek, to the north by Bethlehem Boulevard and Interstate 695, and to the east by a BGE substation and the former Pipe Mill Area (which is currently designated as Parcel A1).

The PDI was performed in accordance with procedures outlined in the Phase II and Pre-Design Investigation Work Plan – Parcel A3. This Work Plan (dated September 17, 2015) was approved by the Maryland Department of the Environment and the United States Environmental Protection Agency in compliance with requirements pursuant to the following:

- Administrative Consent Order (ACO) between Tradepoint Atlantic (formerly Sparrows Point Terminal, LLC) and the Maryland Department of the Environment (effective September 12, 2014); and
- Settlement Agreement and Covenant Not to Sue (SA) between Tradepoint Atlantic (formerly Sparrows Point Terminal, LLC) and the United States Environmental Protection Agency (effective November 25, 2014).

An application to enter the Tradepoint Atlantic property into the Maryland Department of the Environment Voluntary Cleanup Program (MDE-VCP) was submitted to MDE on September 10, 2014. The property's current and anticipated future use is Tier 3 (Industrial), and plans for the property include demolition and redevelopment over the next several years. Parcel A3 is also part of the acreage that remains subject to the requirements of the Multimedia Consent Decree between Bethlehem Steel Corporation, the United States Environmental Protection Agency (EPA), and the Maryland Department of the Environment (MDE) (effective October 8, 1997) as documented in correspondence received from EPA on September 12, 2014.

1.1. SITE HISTORY

From the late 1800s until 2012, the production and manufacturing of steel was conducted at Sparrows Point. Iron and steel production operations and processes at Sparrows Point included raw material handling, coke production, sinter production, iron production, steel production, and semi-finished and finished product preparation. In 1970, Sparrows Point was the largest steel facility in the United States, producing hot and cold rolled sheets, coated materials, pipes, plates, and rod and wire. The steel making operations at Sparrows Point ceased in fall 2012.



The Rod and Wire Mill area is located in the northwestern portion of the Site, and is the location of the former mills that produced rods and wire products from the 1940's to the early 1980's. All manufacturing activities at the Rod and Wire Mill area ceased operation in the early 1980's with subsequent demolition of all structures between 1994 and 2000, based on historical aerial photos. Current ground cover includes slag aggregate that was placed in conjunction with the demolition program.

Manufacturing activities at the Rod and Wire Mill included leaching of zinc ore and a subsequent treatment process to remove cadmium impurities. The leaching process was implemented in large tanks located inside the north end of the former Rod and Wire Mill building. In the 1950's through the early 1970's, the acidic leach residue was stored in the Northwest Pond until about 1959 when filters were installed to dewater the residues. Dewatered sludge generated from this process was temporarily stored on the ground outside the north end of the mill in the former Sludge Bin Storage Area. Filtrate from the dewatering process was recycled to the wire plating process. Excess filtrate was discharged to the East Pond until 1971, after which it was sent to the Humphrey Creek Wastewater Treatment Plant (HCWWTP) for treatment. These operations ended in the early 1980's when the Rod and Wire Mill was shut down. The referenced historical potentially impacted areas are shown in **Figure 2**.

1.2. ROD AND WIRE MILL GROUNDWATER INTERIM MEASURE

Historical operations in the Rod and Wire Mill Area resulted in releases of cadmium and zinc to soil and groundwater. In 1986, a soil and groundwater remediation program was initiated to address groundwater exhibiting elevated levels of cadmium and zinc, and residual soil contamination in the Sludge Bin Storage Area. Remediation initially consisted of a soil flushing program and associated pumping and treatment of groundwater from shallow and intermediate wells. The groundwater pumping was discontinued and the treatment plant dismantled in 1999 to support a demolition project at the Rod and Wire Mill allowing for reassessment of the interim measure. A Work Plan to re-establish Interim Measures was submitted in July 2000; the Work Plan was approved by the Agencies in November 2000. Re-establishment of the Interim Measure included an institutional control for soil, upgrades to the monitoring well network, construction of two recovery wells, installation of a transmission pipeline to the HCWWTP, and evaluation of pump test data, groundwater flow characteristics, and review of the system's effectiveness.

The pumping and treatment of groundwater resumed in September 2001 and currently continues. At present, known dissolved cadmium and zinc plumes exist in the sandy subsurface from approximately 20 to 30 feet below ground surface (bgs). The average depth to water is approximately 3 to 5 feet bgs, and the sandy substrate exists down to approximately 50 to 60 feet bgs. There is currently no indication that significant dissolved phase concentrations are deeper than 30 ft. bgs.



Interim Measures (IMs) are currently underway at the former Rod and Wire Mill Area as described below:

- Institutional controls for soils have been established to provide a "Restricted Work Area" to control the exposure of onsite workers to soils in the Former Sludge Bin Storage Area.
- A groundwater monitoring network has been installed including the use of 31 wells for monitoring the performance of the groundwater pump and treat system. This monitoring network is used to collect water level and groundwater quality data.
- A groundwater pump and treat system is operated and maintained consisting of two intermediate depth zone recovery wells (RW10-PZM020 and RW15-PZM020) that operate at a rate of between 5.0 and 12.0 gallons per minute (gpm). The expected normal operating rate for the treatment plant was set at a combined rate of 8.0 to 12.0 gpm with a maximum design flow of 25 gpm. Recovered groundwater is transported via a pipeline to the HCWWTP for subsequent treatment and discharge in accordance with the NPDES permit requirements for the Facility.

A total of 4,487,659 gallons of water were extracted from the Former Rod and Wire Mill Area pumping wells and treated at the HCWWTP during 2015. The average pumping rate for the pump and treat system was 12,295 gpd, or 8.5 gpm. Average annual pumping rates of approximately 3.84 gpm were achieved in recovery well RW15-PZM020 and 4.69 gpm in RW10-PZM020. These pumping rates appear to effectively capture the most impacted groundwater beneath the Former Sludge Bin Storage Area. A total of 210 pounds (lbs) of cadmium and 10,630 pounds (lbs) of zinc were removed and treated during 2015.

- Average Cadmium and Zinc Concentrations:
 - RW10-PZM020:

	2015	2014	2013	2012
Cadmium (ppm)	9.55	9.83	11.75	12
Zinc (ppm)	487	526	373	470

• RW15-PZM020:

	2015	2014	2013	2012
Cadmium (ppm)	0.78	1.08	1.0	3.3
Zinc (ppm)	35.8	34.9	44	51



• <u>Treated mass (lbs)</u>:

• RW10-PZM020:

	2015	2014	2013	2012
Cadmium	197	193	99	142
Zinc	10,027	10,334	3,073	5,805

• RW15-PZM020:

	2015	2014	2013	2012
Cadmium	13	23	12	41
Zinc	603	756	573	637

1.3. OBJECTIVES

The objective of this investigation was to characterize the impacted subsurface area currently undergoing interim remedial action for the future implementation of a remedial strategy. This scope included characterization of the nature and extent of current soil and groundwater contamination in this area. A summary of the soil boring and groundwater well identification numbers and the analyses performed has been provided as **Appendix A**. The PDI work scope also included characterization of the hydrologic properties of the aquifer in the Rod and Wire Mill area. The purpose of the aquifer analysis was to develop a groundwater model which could be used to screen and evaluate potential options for the final remedial approach, assist in developing the remedial design, and identify any additional data requirements.



2.0 SITE GEOLOGY/HYDROGEOLOGY

The encountered subsurface geology included slag fill materials overlying natural soils, which included fine-grained sediments (clays and silts) and coarse grained sediments (sands). Groundwater was observed within the soil cores at depths ranging from 4 to 18 feet below the ground surface (bgs) across the Site. Soil boring logs are provided in **Appendix B**.

Groundwater occurrence at the Site has been segregated into three horizons identified as shallow, intermediate and deep zones. The shallow water bearing zone (water table) includes piezometers screened to depths of approximately 15-feet below ground surface. The intermediate water bearing zone includes piezometers screened from approximately 20- to 30-foot depths. The intermediate water bearing zone is the focus of the interim pump and treat measure and is therefore also referred to as the intermediate pumping zone. The deep water bearing zone is defined as those piezometers screened from approximately 50- to 75-feet below ground surface.

Temporary groundwater sample collection points were installed in the intermediate zone at four locations during the Pre-Design Investigation to investigate groundwater conditions beneath the former Rod and Wire Mill area. In addition to the temporary groundwater sample collection points, several existing intermediate wells were sampled during the PDI. These existing wells included RW02-PZM020, RW07-PZM017, RW10-PZM020, RW19-PZM020, and RW20-PZM020. The locations of the groundwater sampling points are indicated on **Figure 3**. The temporary groundwater sample collection points and existing wells were surveyed by a Maryland-licensed surveyor, and supporting documentation from the surveys is included as **Appendix C**.

A synoptic round of groundwater level measurements was collected on January 28, 2016 from each of the groundwater points included in the PDI sampling plan. Several site-wide wells which were not included in the sampling plan were included in the potentiometric survey to provide better resolution of the groundwater potentiometric surface. Surveyed top of casing (TOC) and ground surface elevations for all applicable locations can be found in **Table 1**, along with the depth to water (DTW) measurements from this date.

Based on the field measurements, a groundwater potentiometric map was constructed for the intermediate hydrogeologic zone. The intermediate contour map is included on **Figure 4**. In this zone, groundwater flow appears to flow from the north and east toward the recovery system pumping wells. The western half of the Site is affected by the recovery system as well as elevations below 0 feet amsl were reported in several wells



3.0 SITE INVESTIGATION

A total of 192 soil samples (112 with Geoprobe, 80 with hollow stem augers) and nine intermediate groundwater samples were collected for analysis between October 1 and November 17, 2015 during the PDI. The PDI also included slug tests and an aquifer pumping test, which aided in the development of the preliminary groundwater model. Methods and protocols were utilized that followed the procedures included in the Quality Assurance Project Plan (QAPP) dated October 2, 2015 approved by the agencies to support the investigation and remediation of the Tradepoint Atlantic property. Information regarding the project organization, field activities and sampling methods, sampling equipment, sample handling and management procedures, the selected laboratory and analytical methods, quality control and quality assurance procedures, investigation-derived waste (IDW) management methods, and reporting requirements are described in detail in the approved Parcel A3 Work Plan dated September 17, 2015, and the QAPP.

All site characterization activities were conducted under the site-specific health and safety plan (HASP) provided as Appendix A of the approved Work Plan.

3.1. SOIL INVESTIGATION

A total of 18 borings were completed during the Pre-Design Investigation (**Figure 5**). Of these 18 boring locations, 14 were completed to a total depth of 35 feet for the purpose of investigating the current extents of metals contamination. The former East Pond and former Sludge Bin Storage Area were the primary focus of the Pre-Design Investigation based upon historical groundwater data and investigations. The remaining four locations were geotechnical borings completed to a minimum of 50 feet for the purpose of characterizing soils for the possible alignment of a permeable-reactive barrier (PRB) wall for the treatment of groundwater.

A summary of the areas that were investigated for the PDI, along with the boring identification number and the analyses performed, has been provided as **Appendix A**. During the completion of fieldwork, it was necessary to shift three borings from the proposed locations given in the Work Plan, two in the Former East Pond due to standing water and one of the geotechnical borings due to refusal. **Table 2** provides the identification numbers of the field adjusted borings, the rationale for field adjustment, the coordinates of the proposed and final locations, and the distance/direction of the field shifts.

3.1.1. Geoprobe Borings

Continuous core soil borings were advanced at 14 locations across the Site to assess the presence or absence of soil contamination, and to assess the vertical distribution of any encountered contamination (**Figure 5**). Using the Geoprobe[®] MC-7 Macrocore soil sampler, the continuous core soil borings were advanced to 35 feet deep. At each location, each soil core was visually



inspected and screened with a hand-held X-ray fluorescence spectrometer (XRF) for cadmium and zinc prior to logging soil types. Soil boring logs have been included in **Appendix B**, and the XRF calibration logs as **Appendix D**. Please note that unless otherwise indicated, all Unified Soil Classification System (USCS) group symbols provided on the attached boring logs are from visual observations, and not from laboratory testing.

One shallow sample was collected from the 0- to 1-foot depth interval, and deeper samples were collected at approximate 5-foot intervals down to the total boring depth of 35 feet. If the XRF or other field observations indicated zinc/cadmium contamination to exist at a specific depth within the 5-foot interval, the sampling location was shifted to the alternate depth interval indicated by the XRF response. Soil sampling activities were conducted in accordance with the procedures and methods referenced in **Field SOPs Number 009**, **Number 012**, **and Number 013** provided in Appendix A of the QAPP.

Down-hole soil sampling equipment was decontaminated after soil sampling had been concluded at a location, according to the procedures and methods referenced in **Field SOP Number 016** provided in Appendix A of the QAPP.

Soil samples collected for contaminant delineation were submitted to Pace Analytical Services, Inc. (PACE), and analyzed for COPI List (RCRA) metals. Following the receipt of initial data, PACE provided additional (estimated) data for the remaining Target Analyte List (TAL) metals not specified in the RCRA list. A grain size analysis and soil typing procedure were also performed by the subcontracted laboratory Geotechnics, Inc. Based on the specific sampling targets, select locations associated with the East Pond were also analyzed for fraction organic carbon (FOC). Analytical methods, sample containers, preservatives, and holding times for the sample analyses are listed in the QAPP Worksheet 19 & 30 – Sample Containers, Preservation, and Holding Times.

3.1.2. Hollow Stem Auger Borings

A total of four hollow stem auger borings were completed to the west of the remedial investigation area in order to characterize the stratigraphy and geotechnical characteristics of the subsurface (**Figure 5**). These geotechnical borings were installed to provide data for the possible design of a PRB wall for groundwater treatment. Using 8-inch diameter hollow-stem augers and a Dietrich B-120 drill rig, the continuous soil borings were advanced to 50 feet deep. Soil samples were recovered at various intervals as further described below. Blow counts were recorded and recovered soil samples were visually inspected and screened with a hand-held Photo Ionization Detector (PID) prior to logging soil types. Soil boring logs have been included in **Appendix B**, and the PID calibration log as **Appendix E**. Please note that unless otherwise indicated, all USCS group symbols provided on the attached boring logs are from visual observations, and not from laboratory testing.



From each soil boring, one shallow sample (shelby tube or split-spoon) was collected from the 0 to 1-foot depth interval, and deeper samples were collected periodically down to the total boring depth of at least 50 feet. Thicknesses ranged from 1 to 2.5 feet for each individual sample. Shelby tube and split-spoon samples were alternated by field personnel, based on observations in the field. Intermittent periods of augering were completed between sample intervals. Soil sampling activities were conducted in accordance with the procedures and methods referenced in **Field SOPs Number 009, Number 012, and Number 013** provided in Appendix A of the QAPP.

Bulk soil samples were also collected from each of the geotechnical boreholes. Samples weighing approximately 12.5 lbs, 14.8 lbs, 15.8 lbs, and 13.0 lbs were collected from RW-001-GB, RW-002-GB, RW-003-GB, and RW-004-GB, respectively. These bulk samples were pooled to create one composite soil sample weighing approximately 56 lbs. The large composite sample was delivered to PeroxyChem for bench-scale testing related to the possible future design of a groundwater treatment PRB wall.

After soil sampling had been concluded at a location, down-hole soil sampling equipment was decontaminated according to the procedures and methods referenced in **Field SOP Number 016** provided in Appendix A of the QAPP.

Soil samples collected for the geotechnical investigation were submitted to PACE, and analyzed by Geotechnics, Inc. Not all parameters were analyzed for every sample. Generally, the samples collected using split-spoons were analyzed for FOC, while those collected with shelby tubes were analyzed for bulk density, total porosity, grain size analysis (and soil typing), and permeability.

3.2. GROUNDWATER INVESTIGATION

A total of five existing site-wide wells in the intermediate hydrogeologic zone were sampled for inclusion in the PDI. Four temporary groundwater sample collection points were also installed in the intermediate hydrogeologic zone to facilitate the gathering of groundwater samples and to support the definition of the potentiometric surface. The soil boring locations where the intermediate temporary groundwater sample collection points were installed during the PDI included RW-057-SB, RW-063-SB, RW-067-SB, and RW-070-SB (**Figure 3**). The temporary groundwater sample collection point construction logs have been included as **Appendix F**.

At each location the Geoprobe[®] DT22 Dual Tube sampling system was advanced to a target depth of approximately 30 to 35 feet bgs, the 1.25-inch inner rod string was removed, and the temporary, 1-inch PVC groundwater sample collection point was installed through the outer casing. Following its installation, the 0-hour depth to water was documented and the collection point was checked for the presence of Non-Aqueous Phase Liquid (NAPL) using an oil-water interface probe in accordance with the methods referenced in **Field SOP Number 019** provided



in Appendix A of the QAPP. The existing groundwater wells were also checked for the presence of NAPL prior to sampling.

After the installation of each temporary groundwater sample collection point, down-hole equipment was decontaminated according to the procedures and methods referenced in **Field SOP Number 016** provided in Appendix A of the QAPP.

Groundwater samples were collected in accordance with methods referenced in Field SOP **Number 006** provided in Appendix A of the QAPP, which employed the use of laboratorysupplied sample containers and preservatives, a peristaltic pump, dedicated polyethylene tubing, and a YSI water quality meter with a flow-through cell. Groundwater samples submitted for TAL metals were filtered in the field with an in-line 0.45 micron filter. The sampling and purge logs have been included in **Appendix G**. YSI meter calibrations were performed before the start of the day of each sampling event, and a calibration post-check was completed at the end of the day. Appropriate documentation of the YSI calibration has also been included in **Appendix G**.

Groundwater samples were submitted to PACE, and analyzed for total organic carbon (TOC), total dissolved solids (TDS), biological oxygen demand (BOD), chemical oxygen demand (COD), total metals, sulfide, sulfate, ferrous iron, nitrate-N, and alkalinity. The additional parameters listed in the Parcel A3 Work Plan of dissolved oxygen (DO), oxidation-reduction potential (ORP), and pH were collected in the field during groundwater purging. Analytical methods, sample containers, preservatives, and holding times for the sample analyses are listed in the QAPP Worksheet 19 & 30 – Sample Containers, Preservation, and Holding Times.

3.3. AQUIFER INVESTIGATION

The aquifer investigation involved three phases including slug testing, an aquifer pumping test, and numerical groundwater model as described below.

3.3.1. Slug Testing

Hydraulic conductivity was measured at thirty-eight (38) wells within Parcel A3 via slug testing. The slug test method entails instantaneously adding (for a falling-head test) or removing (for a rising-head test) a known volume of water to or from each well and recording the resulting water level response as the hydraulic head recovers to static equilibrium. Hydraulic conductivity is then calculated from the head response using an appropriate analytical method based on several site-specific factors including the type of well construction, degree of aquifer penetration, and confined or unconfined nature of the aquifer.

Of the thirty-eight wells that were slug tested, four (4) were screened in the deep hydrogeologic zone, twelve (12) were screened in the intermediate hydrogeologic zone, and twenty-two (22) were screened in the shallow hydrogeologic zone. Both falling-head and rising-head slug tests



were performed in each of these wells, except for RW17-PZM019, in which only a falling-head test was performed due to excessively rapid and turbulent recovery during the rising-head test.

During the falling-head tests fresh potable water obtained from the onsite wastewater treatment plant (HCWWTP) was quickly poured into each well until the water level reached the top of the casing. During the rising-head tests a bailer was used to remove between 1.5 and 3 gallons from each well. The water removed from each well was containerized in 55-gallon drums and disposed of according to **Field SOP Number 005** provided in Appendix A of the QAPP. An electronic pressure transducer recorded the water levels during all slug tests in 5-second intervals.

3.3.2. Aquifer Pumping Test

A long-term operational aquifer pumping test was performed on wells RW10-PZM020 and RW15-PZM020 from November 4 – December 8, 2015. Water levels in the pumping wells and fourteen (14) existing observation wells in the intermediate hydrogeologic zone were recorded using electronic pressure transducers/dataloggers (1-minute intervals) and/or manual water level measurements. In addition, water levels in twenty one (21) existing observation wells in the shallow hydrogeologic zone were also recorded via manual water level measurements. The shallow well RW22-PZM was also measured with an electronic datalogger to measure tidal effects. Precipitation measurements from the Fort Howard weather station located 3 miles southwest of the Rod and Wire Mill area (Weather Station ID: KMDEDGEM3, Edgemere, MD) were utilized in this report. Pumping rates in RW10-PZM020 and RW15-PZM020 were recorded hourly using a totalizing flow meter. The pumping schedule listed in the aquifer testing operations summary is given below:

Date	Event
11/04/15	Pumping test plan initiated. Both wells are pumping.
11/12/15	Both wells off. Recovery and static monitoring.
11/17/15	RW15-PZM020 begins pumping.
11/20/15	RW10-PZM020 begins pumping.
11/30/15	Both wells off. Recovery monitoring.
12/01/15	RW10-PZM020 begins pumping.
12/02/15	RW15-PZM020 begins pumping.
12/04/15	RW15-PZM020 off. RW10-PZM020 off temporarily and restarted.
12/06/15	Both wells off. Recovery monitoring.
12/08/15	Pumping test operations ceased.

Aquifer Testing Operations Summary



Following completion of the pumping tests, all dataloggers were removed from the wells and RW10-PZM020 and RW15-PZM020 resumed normal pumping operations.

3.3.3. Numerical Groundwater Modeling

A numerical groundwater model was developed for the Rod and Wire Mill area intermediate aquifer zone. This model may be used along with the results from the aquifer pumping test to screen and evaluate potential options for the final remedial approach, assist in developing the remedial design, and identify any additional data requirements during the design process. The groundwater model was developed using results from the slug testing and aquifer pumping tests, as well as additional hydrogeologic and geologic information, including historic groundwater levels, local tidal influences, and field data (well logs) from the shallow, intermediate, and lower hydrogeologic zones. To improve the resolution of the model in the Rod and Wire Mill area, three additional permanent groundwater wells were installed in the intermediate aquifer zone at final depths of approximately 30 to 40 feet bgs. The well construction logs for these additional wells (RW22, RW23, and RW24) have been included in **Appendix F**.

3.4. MANAGEMENT OF INVESTIGATION-DERIVED WASTE (IDW)

In accordance with **Field SOP Number 005** provided in Appendix A of the QAPP, potentially impacted materials, or IDW, generated during this Phase II Investigation was containerized in 55-gallon (DOT-UN1A2) drums. The types of IDW that was generated during this Phase II Investigation included the following:

- soil cuttings generated from soil borings or the installation of the temporary groundwater sampling points;
- purged groundwater;
- decontamination fluids; and
- used personal protective equipment

Following the completion of field activities, a composite sample was gathered from the designated Parcel A3 PDI IDW soil drums for TCLP analysis. Following this analysis, the waste soil was characterized as non-hazardous. A list of all detections from the TCLP analysis of the soil cuttings can be found in **Table 3**, which indicates no exceedances of TCLP criteria.

IDW drums containing aqueous materials were characterized by preparing composite samples from randomly selected drums. Each composite sample included aliquots from three individual drums that were chosen from a set of 30 drums being stored on-site at the date of collection. A total of eight aqueous composite samples were collected for TCLP analysis. A list of all detections from the TCLP analysis of the aqueous waste can be found in **Table 4**, which indicates no exceedances of TCLP criteria. Although there were no TCLP exceedances, one aqueous drum was designated as hazardous waste because it contained purge water from one



piezometer which had an elevated detection of cadmium (44.5 mg/L) in its analytical sample. This drum was segregated based on this preliminary analytical result and was not included in the composite samples.

The parcel-specific IDW drum log from the Site investigation is included as **Appendix H**. All IDW procedures were carried out in accordance with methods referenced in the QAPP Worksheet 21 – Field SOPs and Appendix A of the QAPP.



4.0 RESULTS AND DISCUSSION

4.1. SOIL ANALYTICAL RECORDS

The laboratory soil Certificates of Analysis (including Chains of Custody) are included as **Appendix I**, and the supplemental reports from Geotechnics, Inc. have been included at the close of each certificate. Data Validation Reports (completed only for the initial list of RCRA metals) have been included as **Appendix J**. The laboratory and data validation reports contain a qualifiers key for the final flags assigned to individual results in the attached summary tables.

4.2. SOIL METALS

Table 5 provides the analytical metals data for the soil samples collected during the Pre-Design Investigation. The main contaminants of concern in the former Rod and Wire Mill area are zinc and cadmium based on the previous historical uses in the target area.

Contour maps were developed that show the zinc and cadmium concentrations at specific depth intervals from 0 to 35 feet bgs. Contour data was pooled based on the target depth intervals indicated in the approved Work Plan. Where applicable, individual borings from the separate Phase II Investigation were included for the development of the isoconcentration contours. Specifically, RW-008-SB, RW-036-S, RW-037-SB, and RW-039-SB provided relevant zinc and cadmium concentration data for soils between 0 and 10 feet bgs, which improved the resolution of the isoconcentration contours within this interval.

Figures S-1 through S-8 display soil cadmium contours for the depth ranges of 0 to 1, 2 to 5, 6 to 10, 11 to 15, 16 to 20, 21 to 25, 26 to 30, and 31 to 35 feet, respectively. The lowest contour interval ranges from 0 mg/kg (non-detect) to 0.38 mg/kg, the maximum contaminant level (MCL) based screening level for the protection of groundwater specified in the EPA Regional Screening Level (RSL) Summary Table published November 2015. The highest contour interval extends up to 3,600 mg/kg, with a maximum detection (RW-069-SB-3) of 3,530 mg/kg. While not directly applicable to the Pre-Design Investigation, exceedances of the project action limit (PAL) for cadmium (980 mg/kg) are indicated on all relevant figures.

Figures S-9 through S-16 display soil zinc contours for the depth ranges of 0 to 1, 2 to 5, 6 to 10, 11 to 15, 16 to 20, 21 to 25, 26 to 30, and 31 to 35 feet, respectively. The lowest contour interval ranges from 0 mg/kg (non-detect) to 370 mg/kg, the risk based screening level (with a target hazard quotient of 1.0) for the protection of groundwater specified in the EPA Regional Screening Level (RSL) Summary Table published November 2015. The highest contour interval extends up to 118,000 mg/kg, with a maximum detection (RW-064-SB-12) of 117,000 mg/kg. There were no exceedances of the PAL for zinc (350,000 mg/kg) in any of the soil samples.



Following the development of the zinc and cadmium contours, three dimensional (3D) representations were developed for these two contaminants. The 3D visuals for the cadmium and zinc contours have been included as **Figure 6** and **Figure 7**, respectively.

4.3. SOIL GEOTECHNICAL TESTING

All geotechnical parameters and FOC were reported by the subcontracted laboratory Geotechnics, Inc. The certificates of analysis from these supplemental analyses have been included at the close of each of the PACE laboratory reports for the same sample group (**Appendix I**). The details of the geotechnical analysis are summarized in **Table 6**, and supporting data may be viewed in the laboratory reports. The summary table includes a sample key indicating the sample IDs used by EAG, PACE, and Geotechnics, Inc. Relevant soils data included FOC, percent moisture/solids, Unified Soil Classification System (USCS) symbol and classification, grain size distribution (% greater than #4 sieve, % between #4 and #200 sieve, and % finer than #200 sieve), specific gravity, permeability, bulk density (unit wet/dry weight), and porosity. Not all geotechnical parameters were applicable for every sample.

Cross sections have been developed to describe the lithology of the subsurface in the area of the Pre-Design Investigation. These cross sections were constructed using field-identified soil types. **Figure 8** indicates the locations of the PDI and geotechnical borings, and highlights the three cross sections prepared for the study area. The cross sections include information from the geotechnical borings as well as the shallower borings (35 feet bgs) completed for the purpose of contaminant delineation. **Cross Section A-A'** extends from the center of RW-003-GB to the northeast across the former Sludge Bin Storage Area and the former East Pond. **Cross Section B-B'** extends from the north end of the RW-001-GB to the southeast across the former Sludge Bin Storage Area and the former East Pond. **Cross Section C-C'** extends along the line investigated by borings RW-001-GB to RW-004-GB from the north to the south. The cross sections generally show overlying slag/gravel fill in select locations, followed by intermittent striation of sand and clay layers down to the full boring depth.

4.4. GROUNDWATER ANALYTICAL RECORDS

The laboratory groundwater Certificates of Analysis (including Chains of Custody) are included as **Appendix K**. Data Validation Reports have been included as **Appendix L**. The laboratory and data validation reports contain a qualifiers key for the final flags assigned to individual results in the attached summary tables.

4.5. GROUNDWATER PARAMETERS

Table 7 provides the analytical total metals data for the groundwater samples collected during the Pre-Design Investigation. The main contaminants of concern in the former Rod and Wire Mill area are zinc and cadmium based on the previous historical uses in the target area. Contour



maps have been developed showing the zinc and cadmium concentrations in the intermediate hydrogeologic zone. The contour maps for cadmium and zinc have been included as **Figure 9** and **Figure 10**, respectively. Additional water quality parameters (TOC, TDS, BOD, COD, sulfide, sulfate, ferrous iron, nitrate-N, and alkalinity) are also included in **Table 7**. Other parameters included in the table (DO, ORP, and pH) were used to indicate stabilization of groundwater prior to sampling. These parameters were extracted from the field groundwater purge logs (**Appendix G**), and the last recorded field value was used in each case. Hydraulic Conductivity Results

The Bouwer-Rice Method (Bouwer and Rice, 1976) was used to calculate the hydraulic conductivities following each slug test because of its wide range of applicability. This method is valid for wells in confined or unconfined aquifers, wells that fully or partially penetrate an aquifer, and wells that are screened or open to the surrounding formation.

The average hydraulic conductivities for the shallow, intermediate, and deep hydrogeologic zones were calculated to be 8.33, 15.81, and 3.51 ft/day, respectively. **Table M1** in **Appendix M** summarizes the calculated hydraulic conductivities for each test. The falling-head and rising-head conductivities were pooled for each well, yielding an average hydraulic conductivity for the location. The conductivity value only applies to the aquifer in the immediate vicinity of each well at the screened depth intervals. The hydrographs and calculated results for each individual test are included in **Appendix M**.

4.6. AQUIFER PUMPING TEST RESULTS

Measurements from the pumping test are included in **Appendix N** (hydrographs for the pumping wells and all monitoring wells including graphs of precipitation and pump ON and OFF events). The instantaneous pumping rates for RW10-PZM020 and RW15-PZM020 in gallons per minute (GPM) varied between 2 GPM to 7 GPM and 3 GPM to 5 GPM, respectively, throughout the test. Water level measurements were taken from 22 monitoring wells in the shallow hydrogeologic zone and 15 monitoring wells in the intermediate hydrogeologic zone. Measurements from RW22-PZM were impacted by the presence of floating hydrocarbon product (NAPL) in the well and were not included in the water level maps or the groundwater modeling.

Hydraulic conductivity and storage were calculated using the Cooper-Jacob Straight Line Approximation (Cooper and Jacob, 1946) for both pumping wells based on water level data from periods when only the well of interest was pumping. Storage was calculated for RW15-PZM020 only. The storage value for RW10-PZM020 could not be determined due to a precipitation event on November 19, 2015 that obscured the drawdown response in the existing observation wells. The hydraulic conductivity values for the pumping wells are included in **Appendix M**. The conductivity and storage calculations are also included (following the slug testing hydrographs).



Average stabilized water levels for the pumping wells and each monitoring well were determined during the times when (1) both wells were pumping, (2) only one well was pumping, and (3) no wells were pumping. These water levels were incorporated into the numerical groundwater model for calibration purposes.

4.7. INITIAL GROUNDWATER MODEL

4.7.1. Model Construction and Calibration

The numerical groundwater model for the intermediate aquifer zone was created using the United States Geological Survey (USGS) MODFLOW computer software. The model used in this project is steady-state and three-dimensional with 11,772 rectangular cells and six layers representing the shallow, intermediate, and deep aquifers (hydrogeologic zones) and three aquitard units. Ambient (non-pumping) conditions were established using the static water level measurements in the monitoring and pumping wells prior to the aquifer tests. General head boundaries around portions of the outer edge of the model domain were adjusted to approximate ambient conditions. Preliminary hydraulic conductivity zones in the model were estimated using computed hydraulic conductivities from the slug test and aquifer pumping test results. The model was calibrated to steady-state pumping conditions (i.e., RW10-PZM020 and RW15-PZM020 pumping) as measured during the aquifer pumping test by modifying the hydraulic conductivity zones and general head boundary conditions until the model-computed heads were within 0.25 feet of the measured heads in the monitoring wells. A detailed report documenting the development of the numerical groundwater model has been included as **Appendix O**. The final calibrated model hydraulic conductivity values are shown in **Figure 11**.

4.7.2. Model Results

4.7.2.1. RW10 and RW15 Pumping

The modeled groundwater contours for the condition when both pumping wells are operating (pump on) in the intermediate aquifer zone are shown in **Figure 12**. All abbreviated well designations refer to the existing observation wells in the intermediate hydrogeologic zone. Modeled groundwater elevation contours matched measured water level measurements in all intermediate aquifer monitoring wells within 0.25 feet. Measureable drawdowns of 1.49 feet or more associated with the pumping of RW10 and RW15 were observed in all monitoring wells including RW19, RW20, and RW21 located on the west and southwest sides of the Rod and Wire Mill area. Modeled groundwater elevation contours indicate that RW10 and RW15 pumping wells provide sufficient drawdown to capture flows from the northern and eastern portions of the Rod and Wire Mill area. Areas located south and west of the RWM do not have sufficient control points beyond the existing monitoring wells to verify complete capture.



4.7.2.2. RW10 and RW15 Not Pumping

The measured groundwater contours for the condition when both pumping wells are not operating (pump off) in the intermediate aquifer zone are shown in **Figure 13** and **Figure 14**. Two figures are shown for the pump off condition due to the different recovery responses measured in RW10 and RW15. Groundwater mounding in the vicinity of RW10 and RW15 was noted for the period November 12 to 17, 2015 (both pumps OFF; **Figure 13**), and a depression in the groundwater surface was noted in the vicinity of RW15 for the period December 6 to 9, 2015 (both pumps OFF, **Figure 14**).

The groundwater mounding shown in **Figure 13** indicates that groundwater is moving from shallow aquifer zones vertically downward in close proximity to the RW10 and RW15 well bores and into the intermediate aquifer when both pumps are off. The groundwater depression in the vicinity of RW15 (**Figure 14**) indicates that recovery was incomplete in this well bore area possibly due to localized blockage to return flow after the pump was turned off. The variability in the recovery response of the two pumping wells indicates one or more of the following:

- a) Vertical communication between shallow and intermediate aquifer zones in the vicinity of RW10 and RW15.
- b) Temporary blockage of the well screen/sand pack in RW15 during the pump off condition.
- c) Changes in the vertical hydraulic gradient between shallow aquifers and the intermediate aquifer associated with the regular pumping of RW10 and RW15, precipitation events, or other factors associated with heterogeneous aquifer parameters at the Site. The vertical hydraulic gradient at the Rod and Wire Mill area may be positive or negative depending on the conditions mentioned above coupled with the similarity in hydraulic heads between aquifers at this site.
- d) The other monitoring wells in the intermediate aquifer consistently recovered to within 0.5 feet during the two pump off conditions supporting a) and b) above.

4.7.2.3. Scenarios from Modeled Results

Modeled pumping scenarios with RW15 pumping and RW10 off, RW15 off and RW10 pumping, and both RW15 and RW10 off are illustrated in **Figures 15, 16, and 17** respectively. Pump on scenarios for both RW10 and RW15 indicate capture from the north and east portions of the site; however, areas located south and west have very small hydraulic gradients and limited control points to assure 100% capture of fluids migrating from the west. The scenario with both RW10 and RW15 pumps off indicates southerly and westward migration of fluids away from the Rod and Wire Mill area.



5.0 FINDINGS AND RECOMMENDATIONS

The objectives of this Pre-Design Investigation were to identify the presence/extent of any existing soil and groundwater contamination, and to describe the stratigraphy and lithology of the subsurface in the potential location of a PRB wall. During the investigation, nine groundwater samples and 192 soil samples (112 with Geoprobe, 80 with hollow stem augers) were collected and analyzed. A large composite soil sample was also submitted to PeroxyChem for batch testing related to the PRB wall. Slug tests and aquifer pumping tests were completed to support the development of a groundwater flow model. This flow model may assist in the selection and design of the final remedial approach.

Groundwater samples were analyzed for total metals, TOC, TDS, BOD, COD, sulfide, sulfate, ferrous iron, nitrate-N, and alkalinity. Additional parameters collected in the field during groundwater purging (pH, ORP, DO) were also reported. The resulting groundwater data indicates that zinc contamination may be more widespread than cadmium in the intermediate hydrogeologic zone. RW-057-PZ (Sludge Bin Storage Area) and RW-067-PZ (East Pond) both exhibited elevated levels of zinc in groundwater, while levels of cadmium were negligible in RW-067-PZ. Furthermore, the cadmium mass appears to be concentrated in the vicinity of the former Sludge Bin Storage Area, with greater than 90% of the mass detected within three sample locations (RW07-PZM017, RW10-PZM020, and RW-057-PZ). Zinc contamination appears to be more widespread, with detections exceeding 10 mg/L in all locations except for one (RW19-PZM020). Based on the established potentiometric surface, natural groundwater flow is towards the west along a slight gradient before intersecting with Bear Creek.

The existing recovery well system utilizing RW10-PZM020 and RW15-PZM020 appears to capture groundwater from the eastern and northern portions of the site when both pumps are operating. Groundwater capture in the western and southern portions of the site is less certain due to low hydraulic gradients and lack of control points in those areas. Measured groundwater levels and modeled scenarios with only one pump operating also indicate uncertain capture of groundwater west and south of the site. The measured groundwater levels and modeled scenario with both pumps off indicates that groundwater will generally flow from east to west and off-site.

Soil samples collected with the Geoprobe were analyzed for metals, and a grain size analysis was performed along with a USCS soil classification. Soil samples associated with the former East Pond were also analyzed for FOC. The geotechnical borings completed with hollow stem augers were analyzed for their grain size distribution and soil classification, along with FOC, bulk density, permeability and total porosity. These parameters are relevant for determining the anticipated effectiveness of treatment in the remedial zone, as well as the necessary vertical extent of a PRB wall. The bulk soil sample collected from the geotechnical borings was delivered to PeroxyChem for bench-scale modeling. Following the completion of batch tests,



PeroxyChem prepared a completion report documenting their work. This soil testing report is included as **Appendix P**.

Based on the 14 PDI borings completed within the boundaries of the former East Pond and former Sludge Bin Storage Area, the zinc and cadmium contamination appears to be highly co-located. The most elevated detections for both metals were observed in the location of borings RW-064-SB (11 to 15 feet bgs) and RW-069-SB (2 to 5 feet bgs), both of which targeted the former East Pond area. Notably, the elevated levels at location RW-069-SB appear to extend vertically downward into the next sampling interval (6 to 10 feet bgs), but appear to be more significant at the adjacent boring RW-068-SB, located roughly 90 feet to the southeast. This may be indicative of a continuous zone of contamination within the specified depth range. The severe impacts observed at RW-064-SB do not appear extensive, as the zinc and cadmium detections above and below the contaminated sample (11 to 15 feet bgs) were negligible. Slight elevations of zinc and cadmium were observed in the surficial soil samples from RW-067-SB (East Pond) and RW-057-SB (Sludge Storage Bins). At RW-067-SB, the concentrations of the target metals appeared to dissipate rapidly with depth, while remaining more persistent in the former Sludge Bin Storage Area from 2 to 5 feet bgs.

Field logged soil types were used in the construction of cross sections below the Former East Pond and Sludge Bin Storage Area. Slag fill was observed overlying several boring locations, with striated clay and sandy layers extending through the remainder of the borehole depths. **Cross Section C-C'** is particularly beneficial for describing potential confining layers in the vicinity of the potential PRB wall. This cross section demonstrates the extent of a 5 to 15 foot thick clay layer overlying the intermediate hydrogeologic zone where the highest levels of groundwater contamination have been consistently documented. A second main clay layer is located 5 to 35 feet beneath the first layer, indicating the presence of a sandy water bearing unit with this approximate thickness. The full thickness of the deeper clay layer is undefined, but RW-001-GB extended approximately 25 feet into the clay without breakthrough. In the event that a PRB wall is installed, the lowest extent of the reactive zone must extend to within this deeper clay unit to prevent circumvention below the wall.

The PDI provided relevant chemical data to support the delineation of contaminated soil and groundwater. The distribution of contaminant mass in the soil and groundwater has been defined using zinc and cadmium isoconcentration contours. The groundwater flow model developed using the results of the slug testing and aquifer pumping test has characterized existing hydrologic conditions in the aquifer, and may aid in the selection and design of the final remedial strategy. Soil geotechnical conditions have been characterized to support the evaluation of future remedial options, and may also be useful to support future development planning.



6.0 REFERENCES

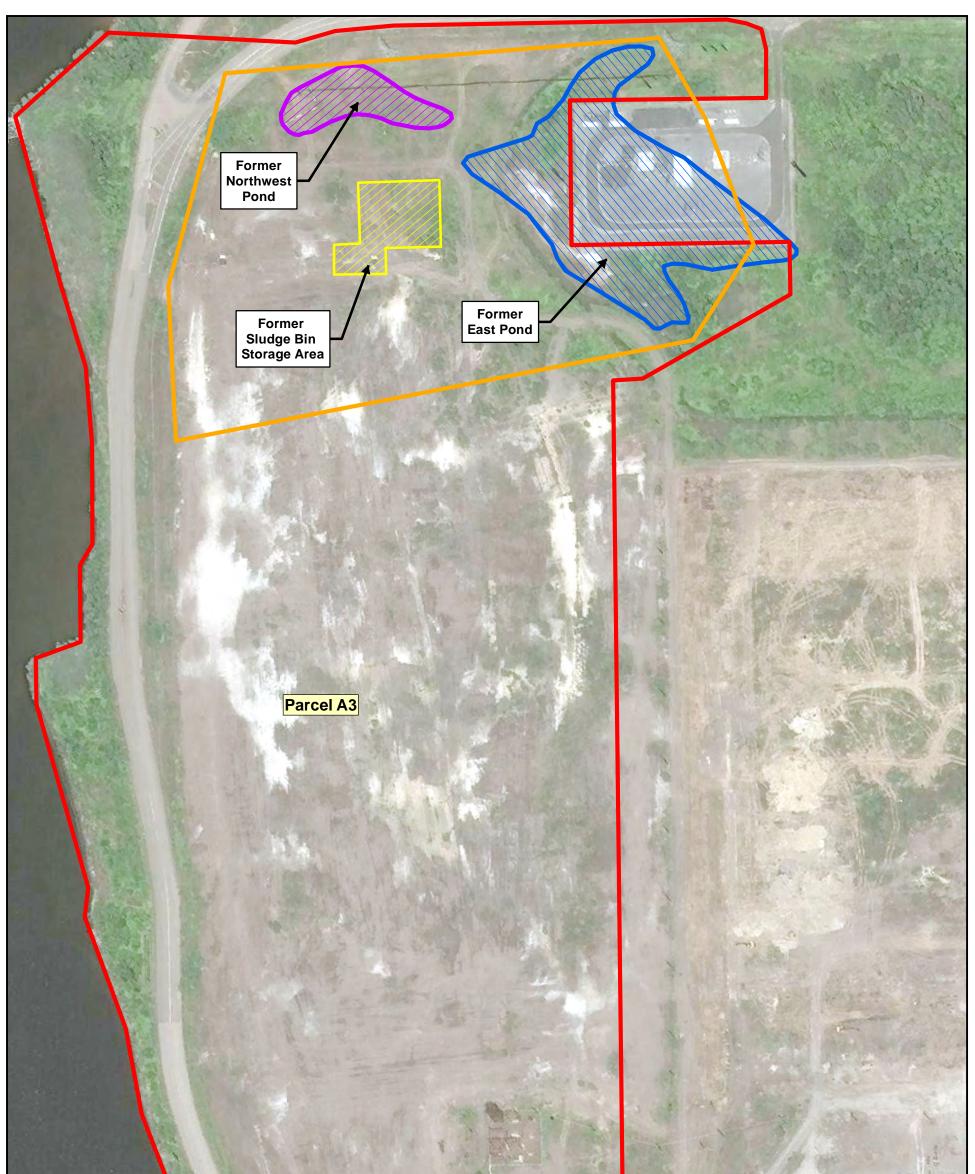
- ARM Group, Inc. (2015). Quality Assurance Project Plan: Sparrows Point Terminal Site. Revision 2. October 2, 2015.
- Bouwer, H. and Rice, R.C. (1976). A slug test for determining hydraulic conductivity of unconfined aquifers with completely or partially penetrating wells. *Water Resources Research*, vol. 12, p. 413-420.
- Cooper, H.H. and Jacob, C.E. (1946). A generalized graphical method for evaluating formation constants and summarizing well-field history. *Transactions, American Geophysical Union*, vol. 27, p. 526-534.
- EnviroAnalytics Group (2015). Phase II and Pre-Design Investigation Work Plan: Parcel A3 Former Rod and Wire Mill Area. Final Draft. September 17, 2015.
- Rust Environmental & Infrastructure (1998). Description of Current Conditions: Bethlehem Steel Corporation. Final Draft. January, 1998.
- Weaver Boos Consultants (2014). Phase I Environmental Site Assessment: Former RG Steel Facility. Final Draft. May 19, 2014.



FIGURES



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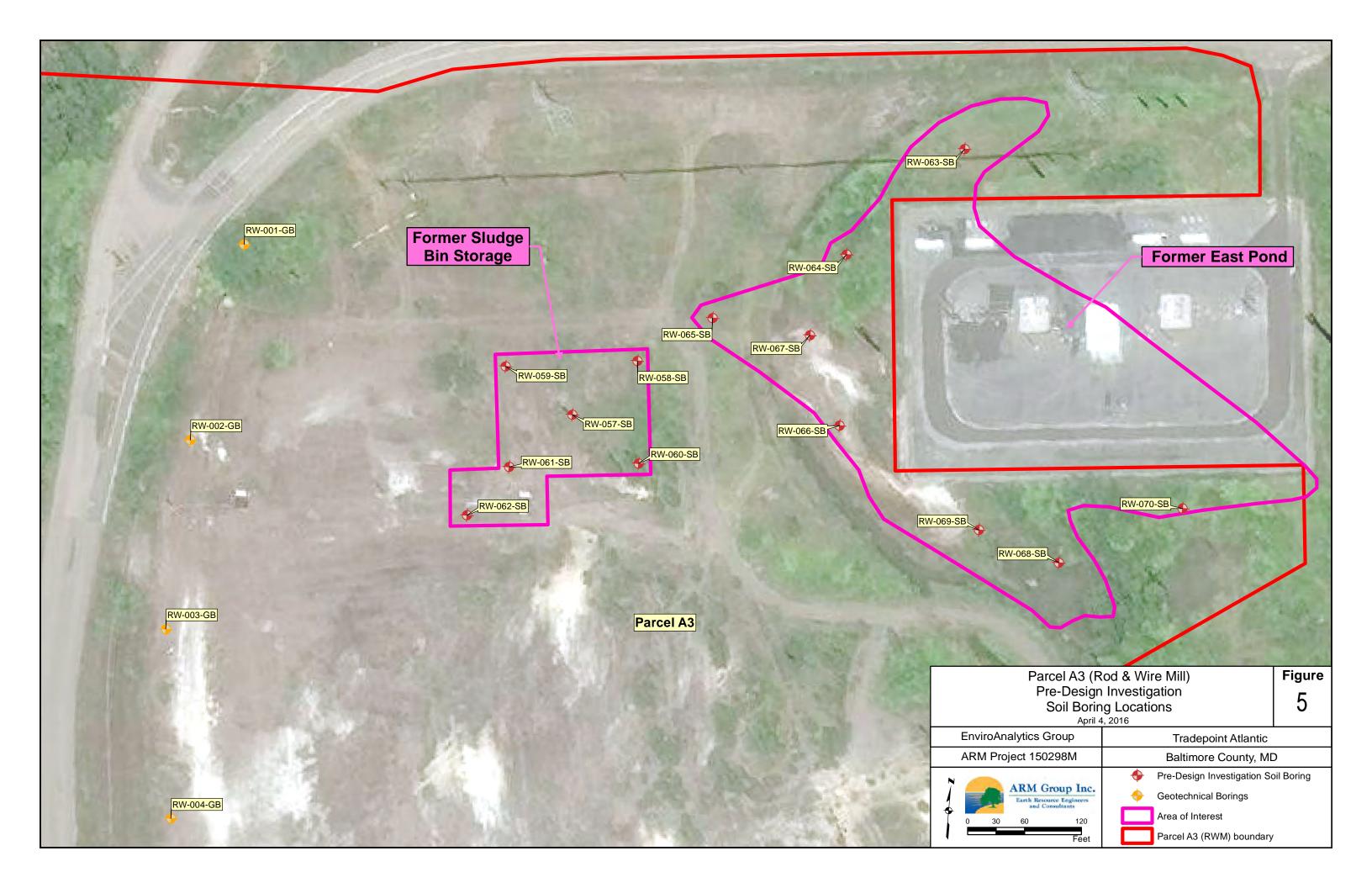


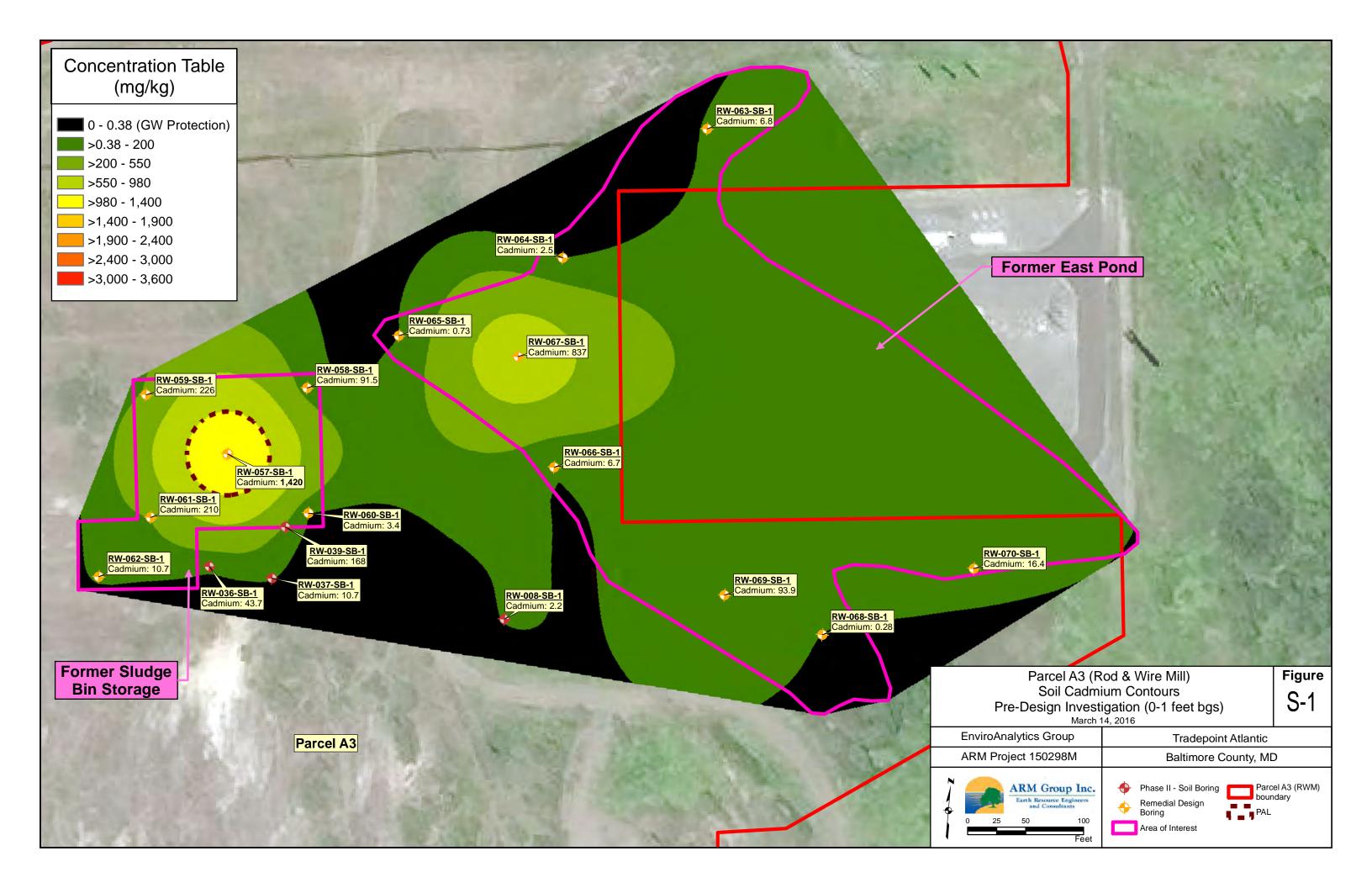
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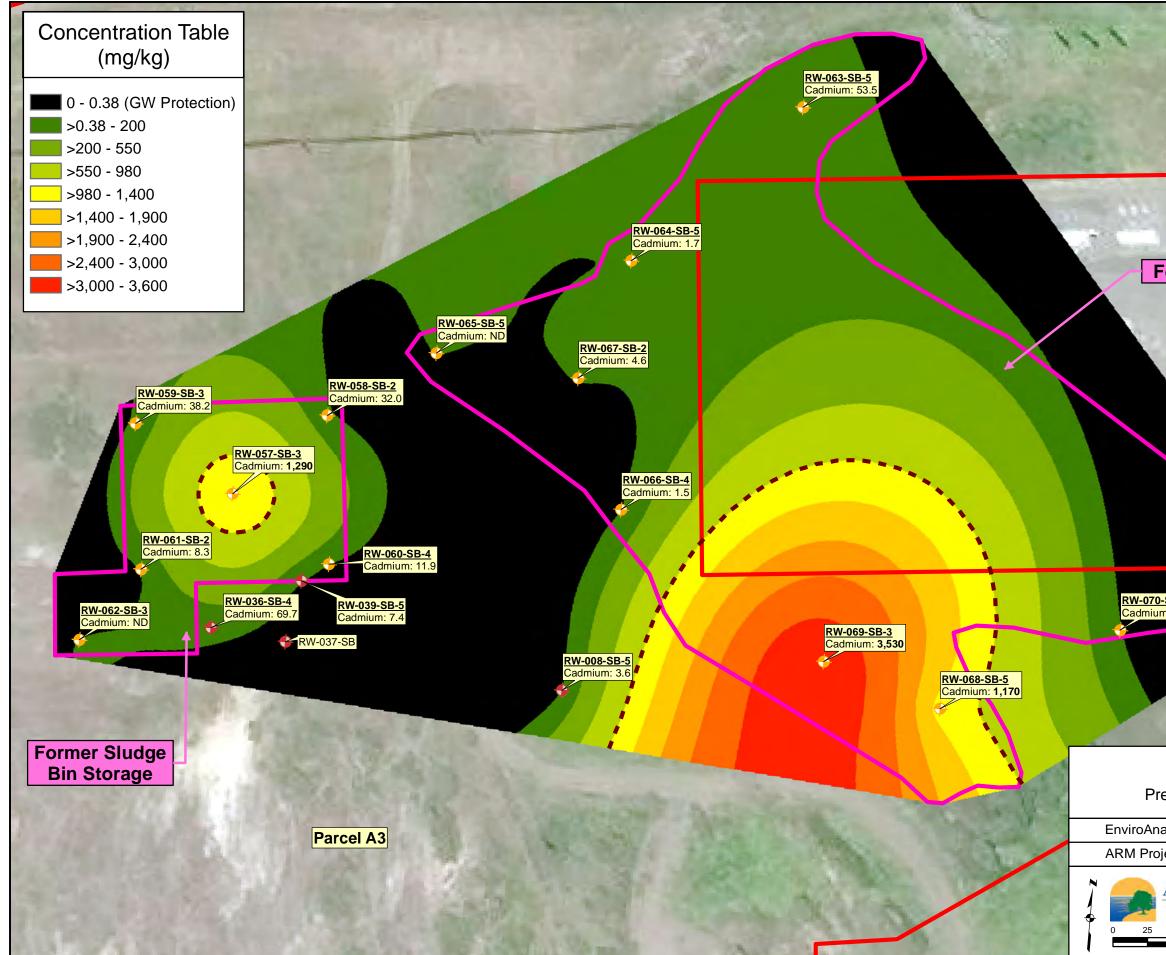


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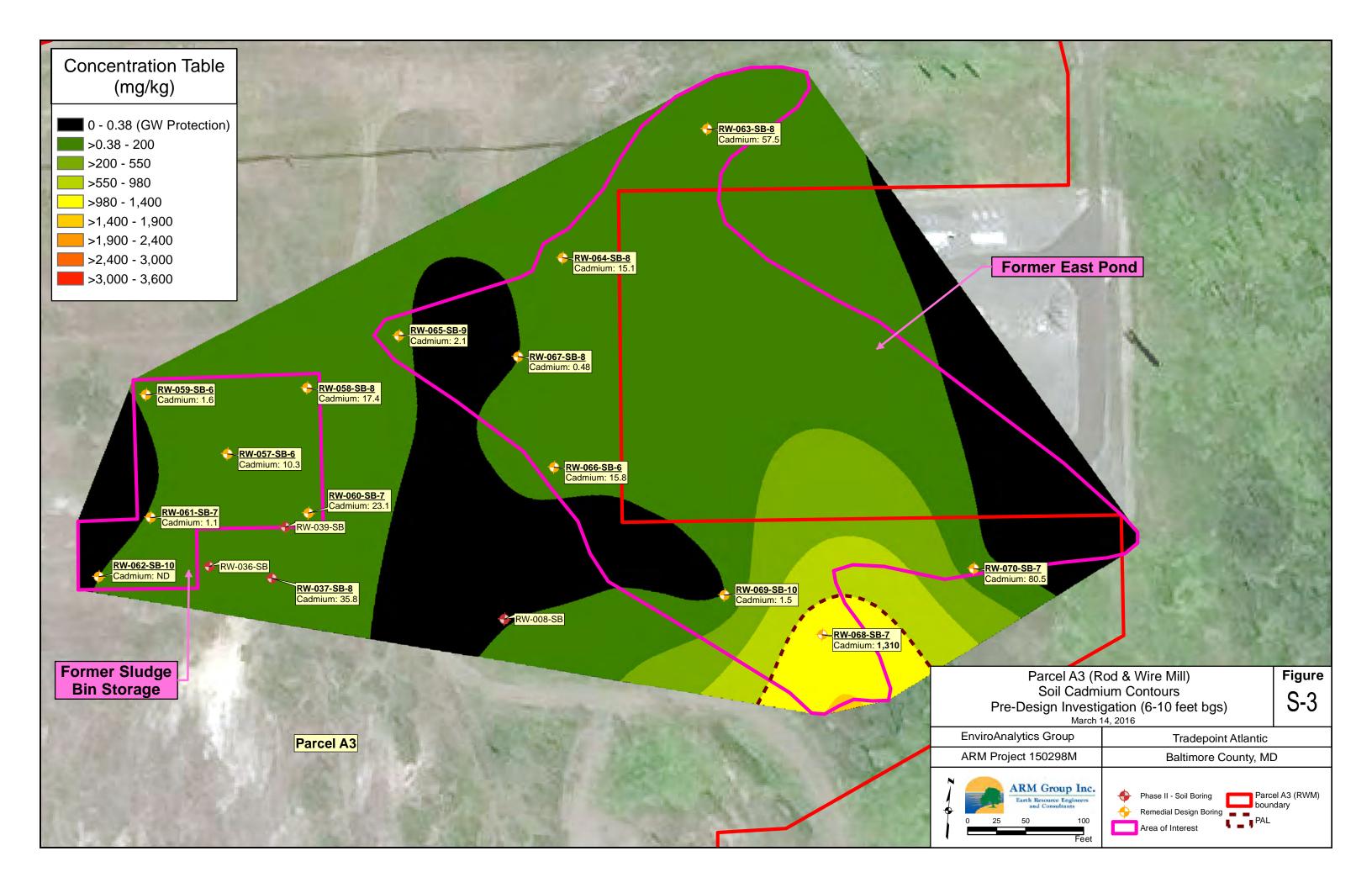


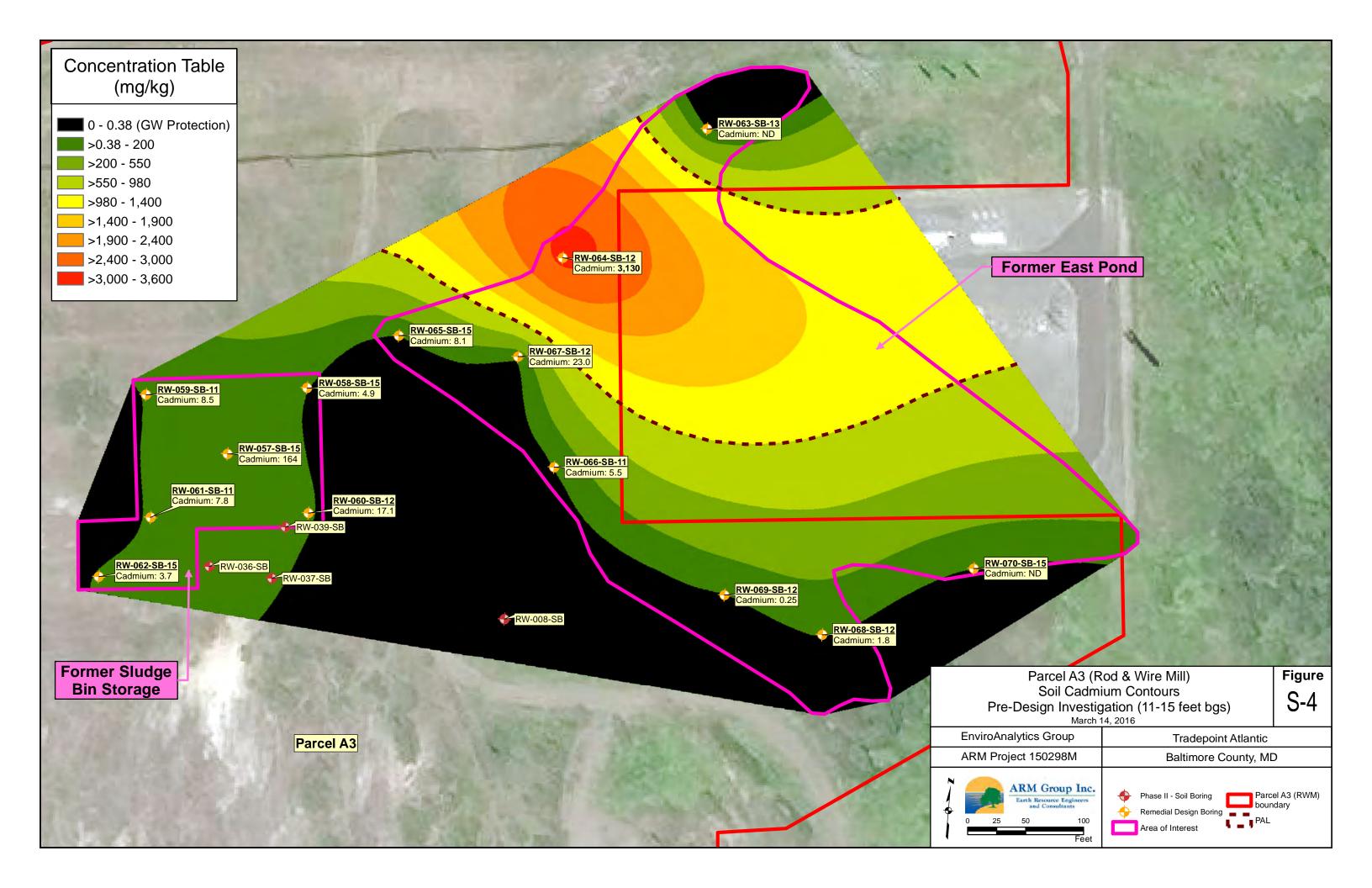


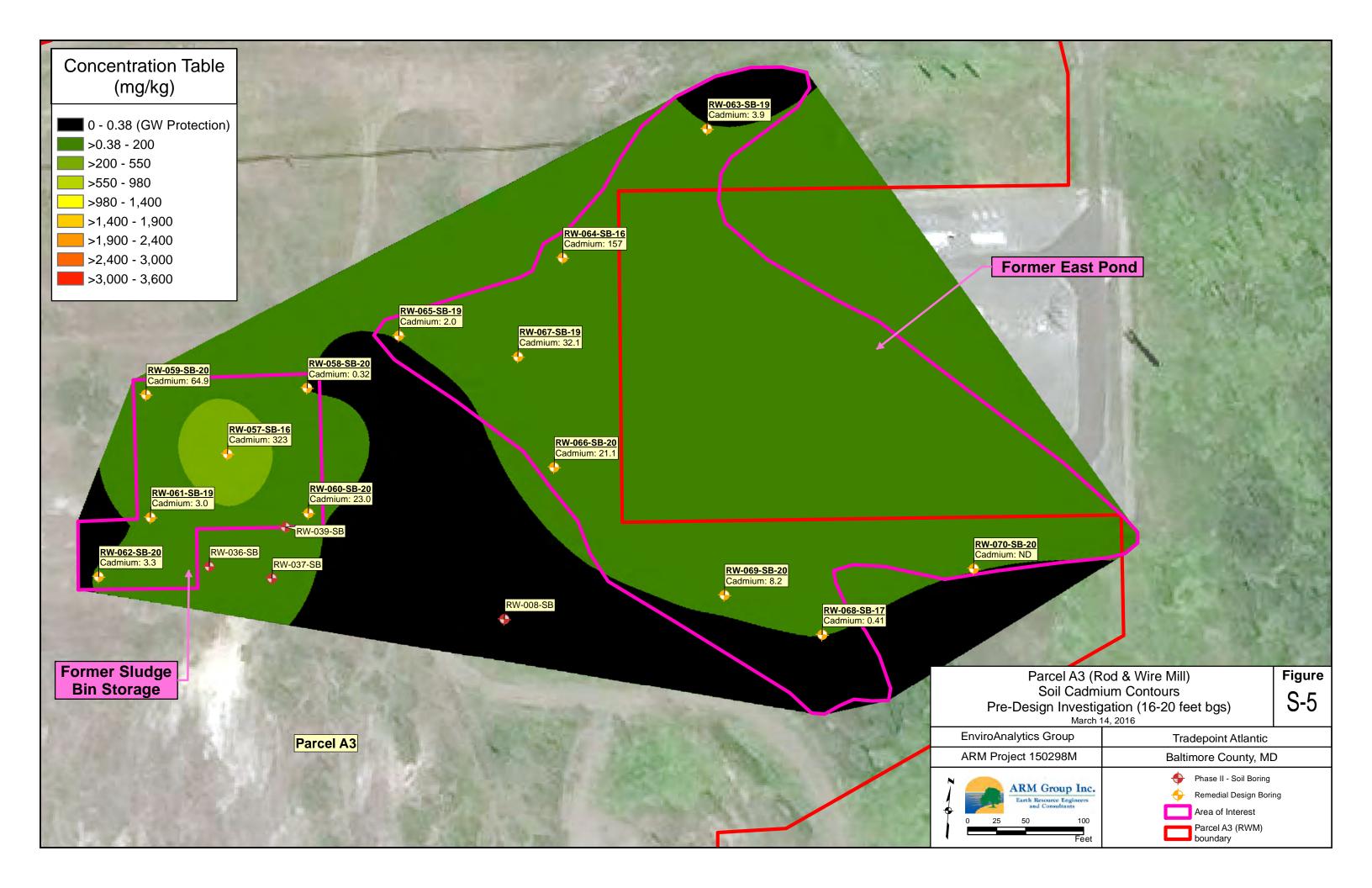


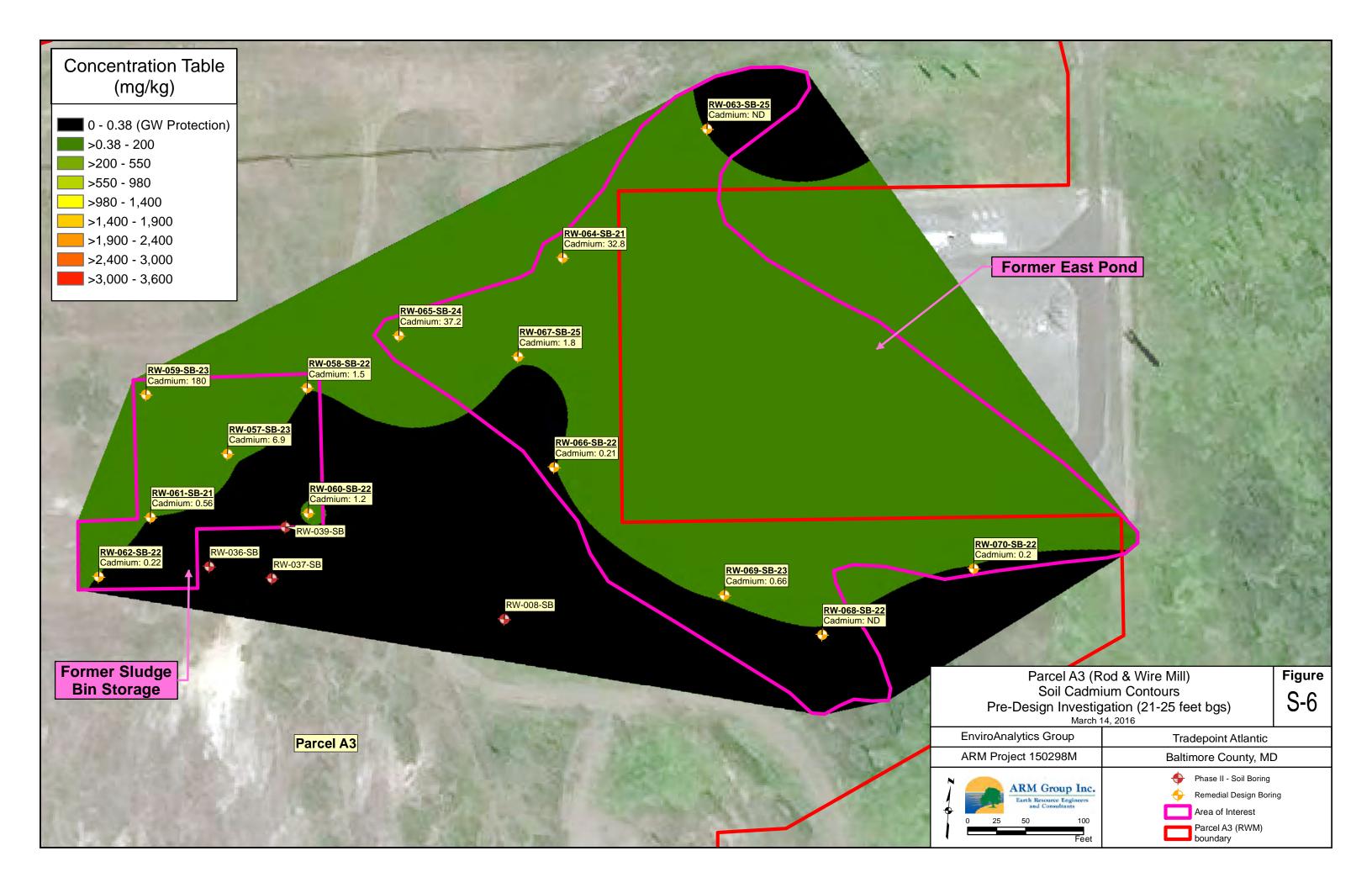


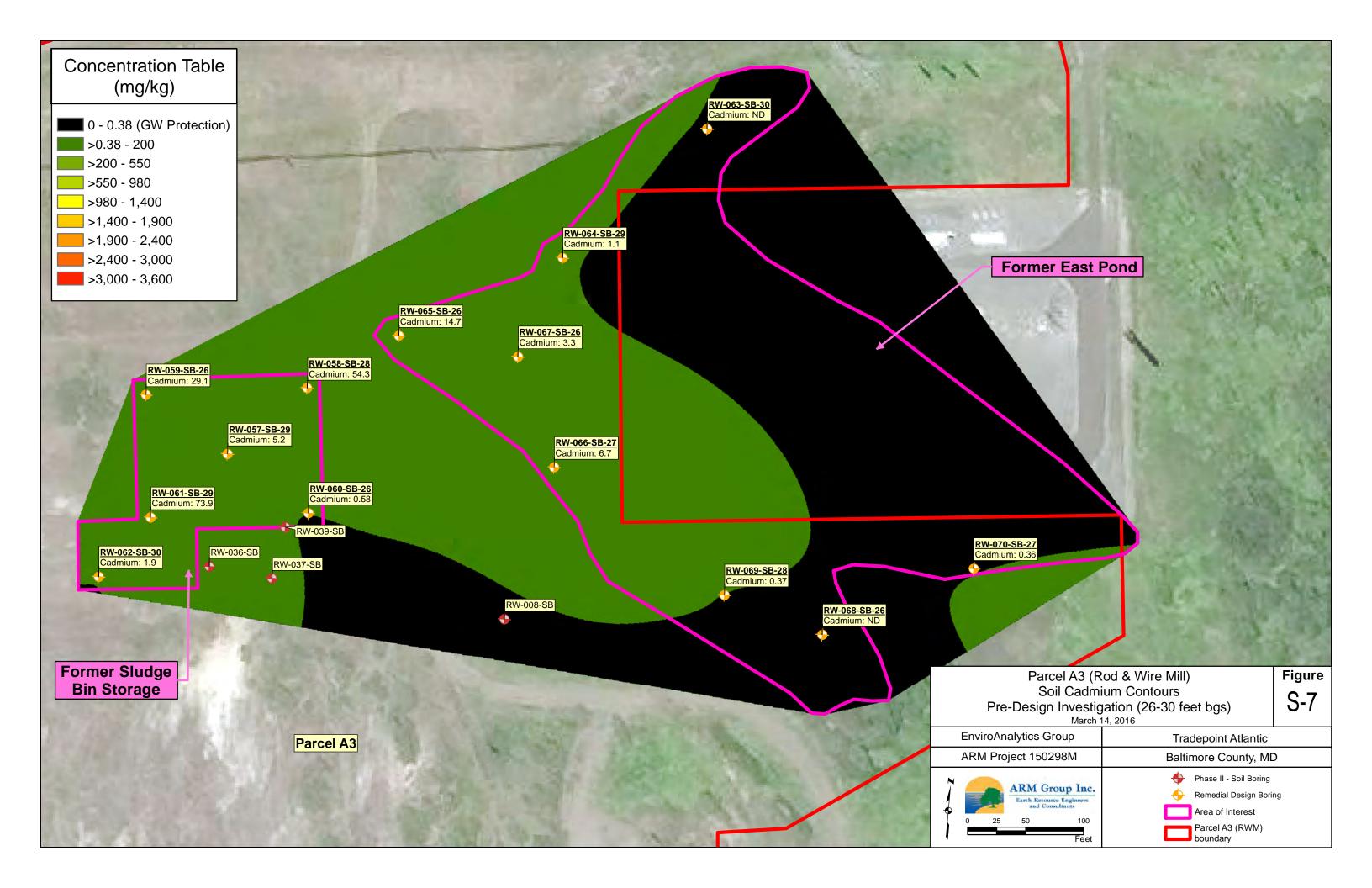
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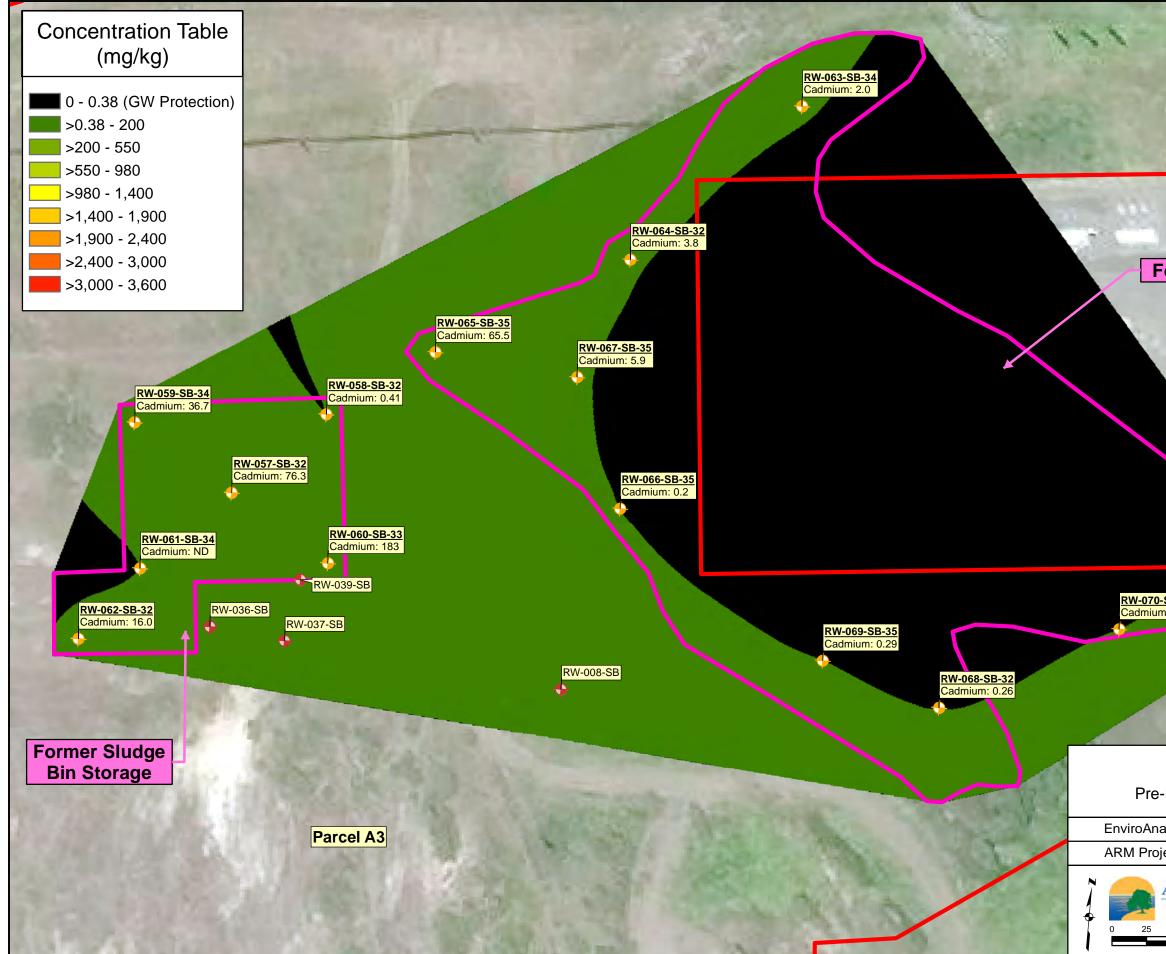




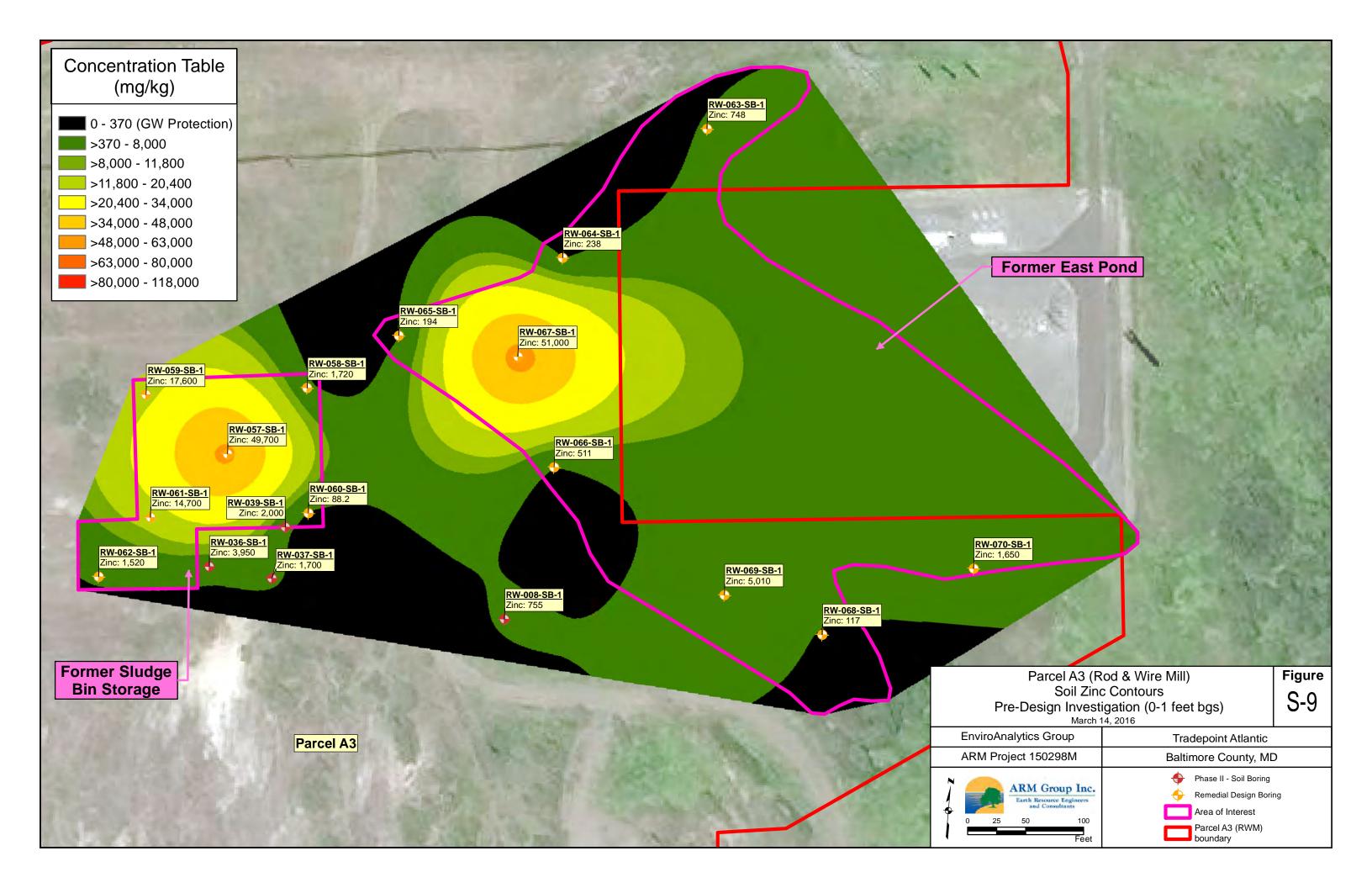


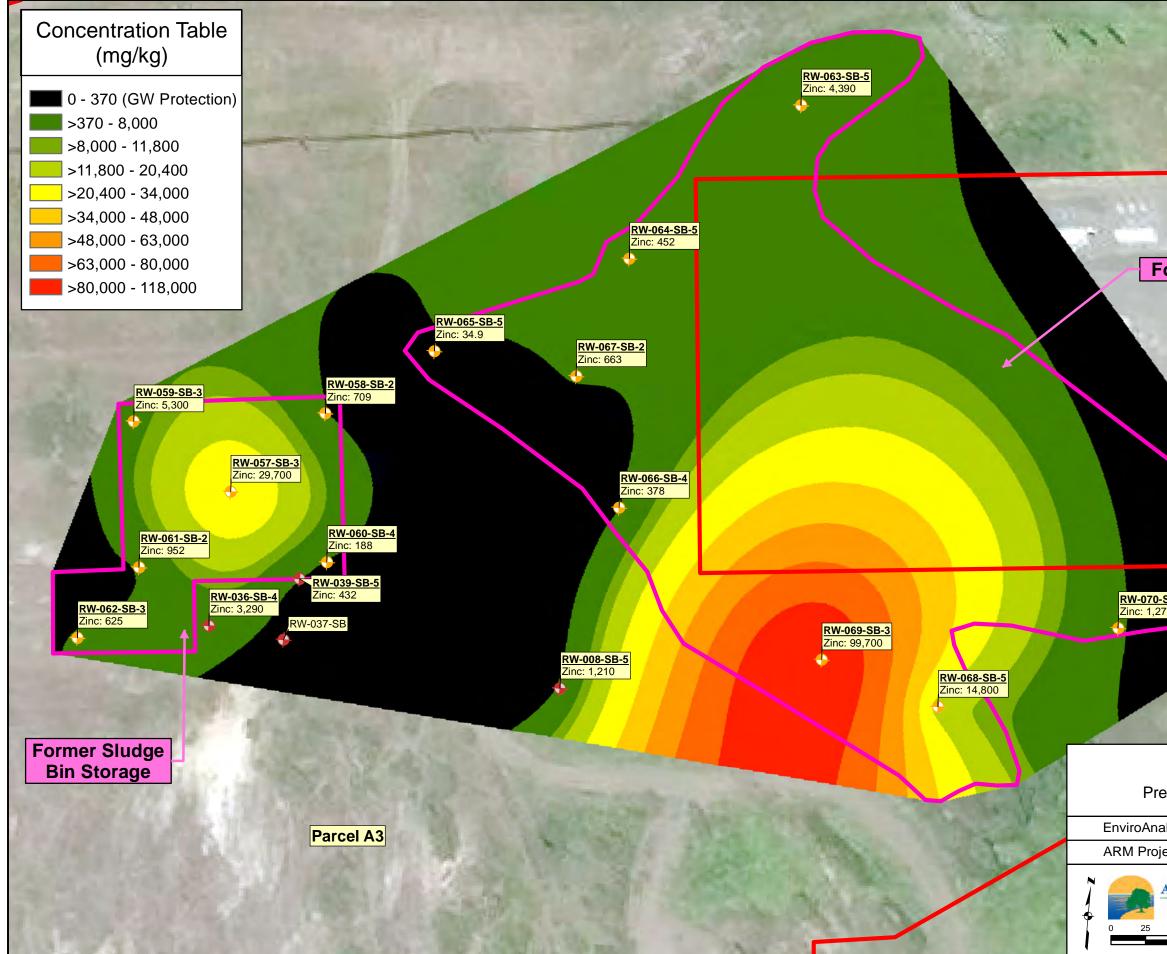




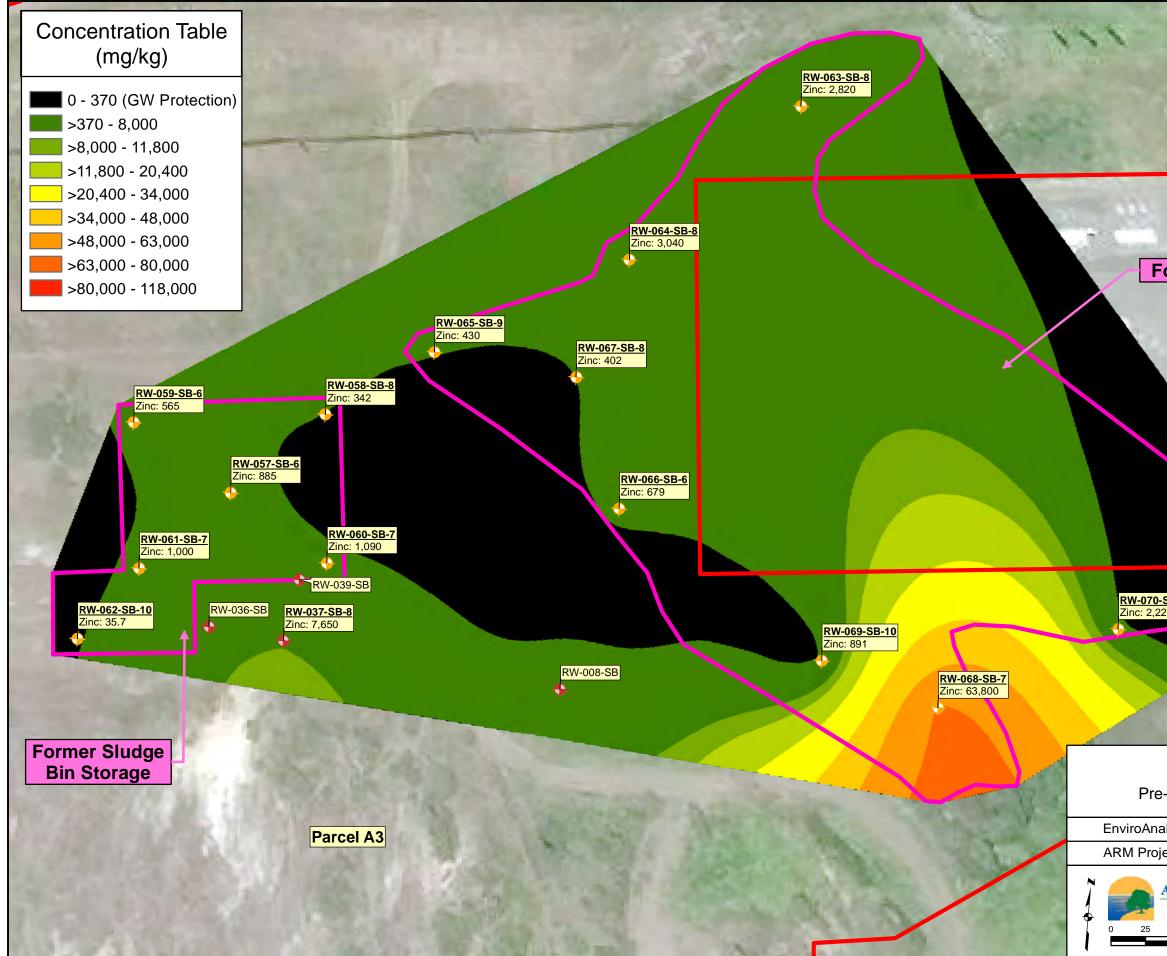


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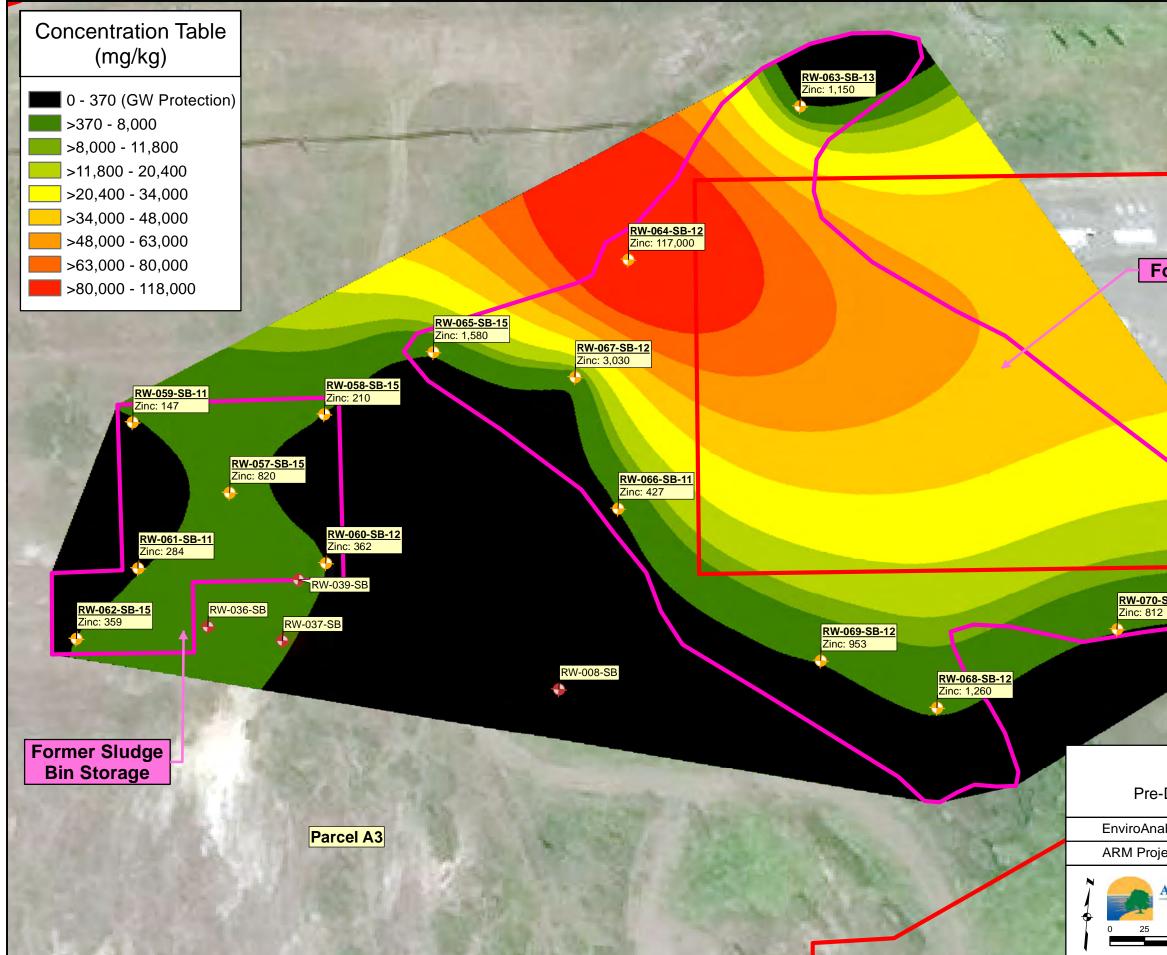




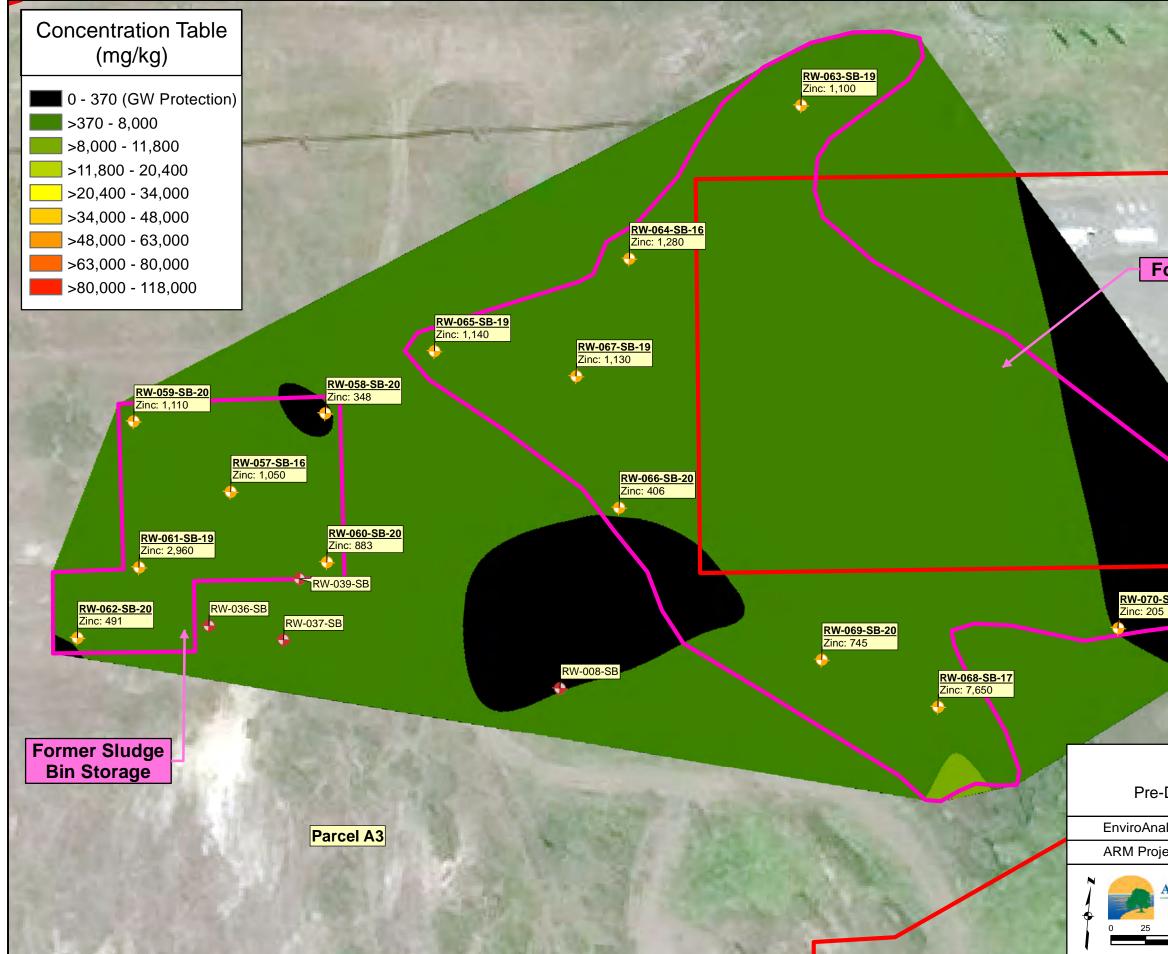
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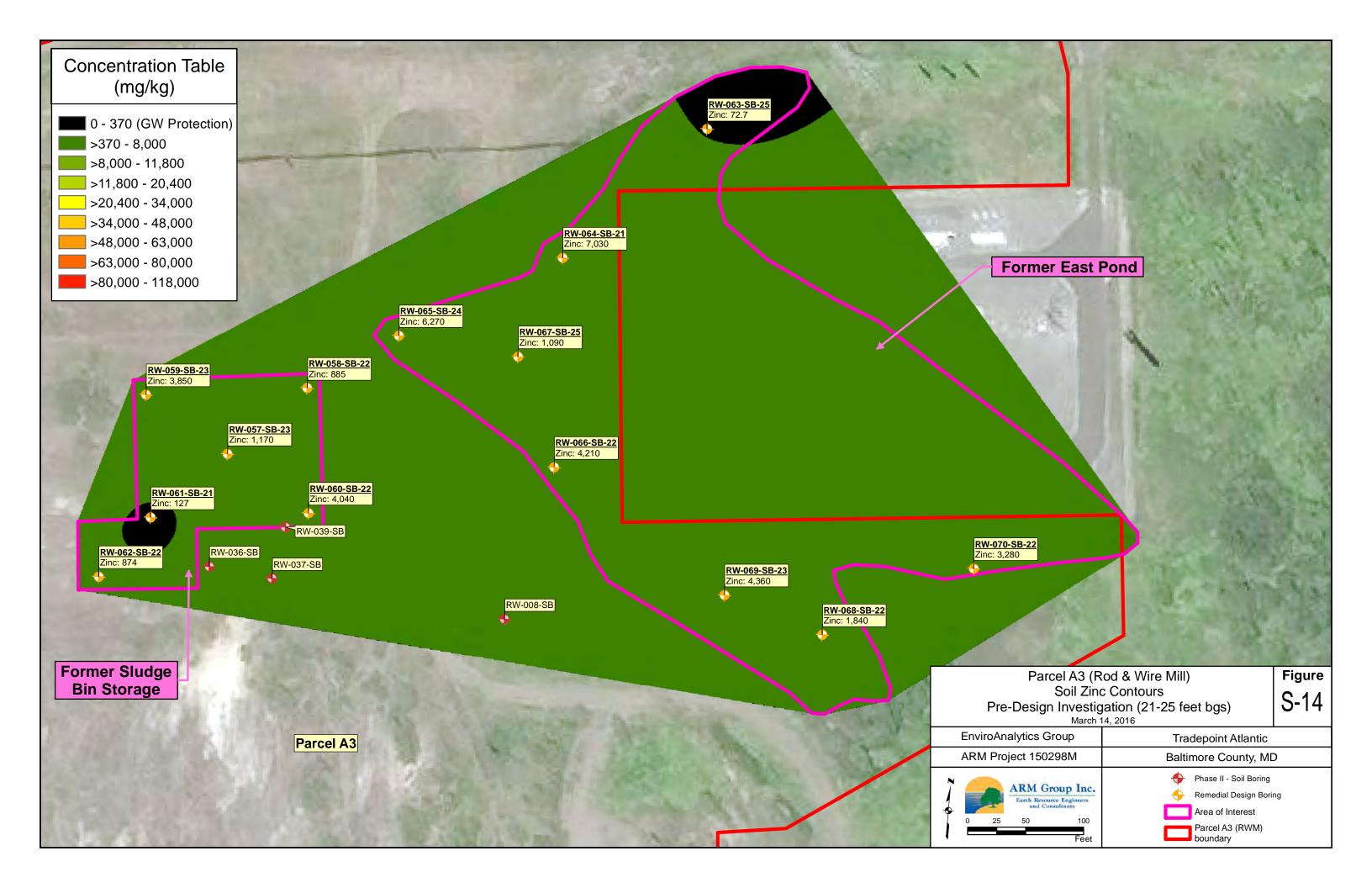
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Earth Resource Engineers and Consultants 50 100	Area of Interest	
Feet	Parcel A3 (RWM) boundary	

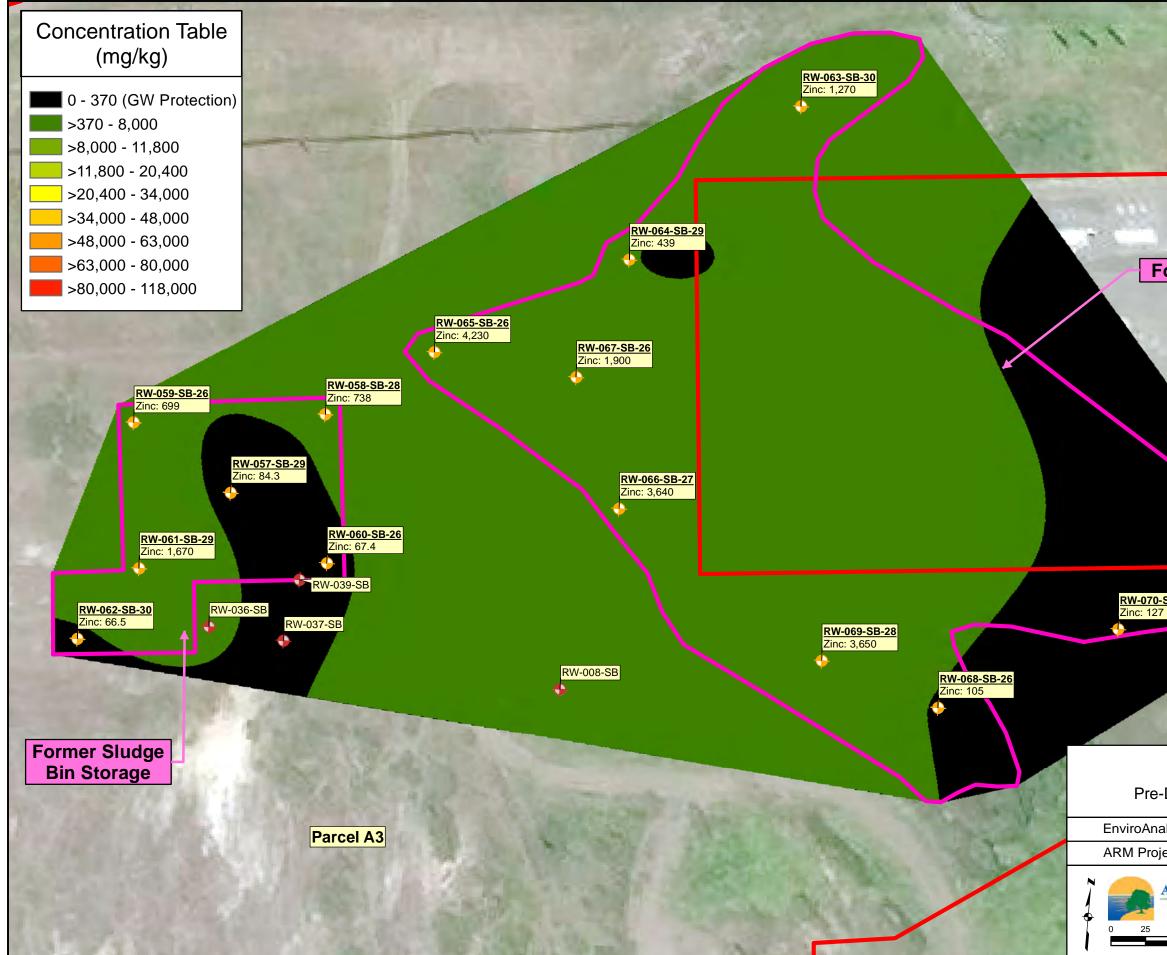


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Soil Zind	c Contours	S-12
e-Design Investig March 1	ation (11-15 feet bgs) 4, 2016	5-12
alytics Group	Tradepoint Atlantic	
oject 150298M	Baltimore County, MI)
ARM Group Inc.	Phase II - Soil Boring	
Earth Resource Engineers and Consultants	Remedial Design Bori	ng
50 100		
Feet	Parcel A3 (RWM) boundary	

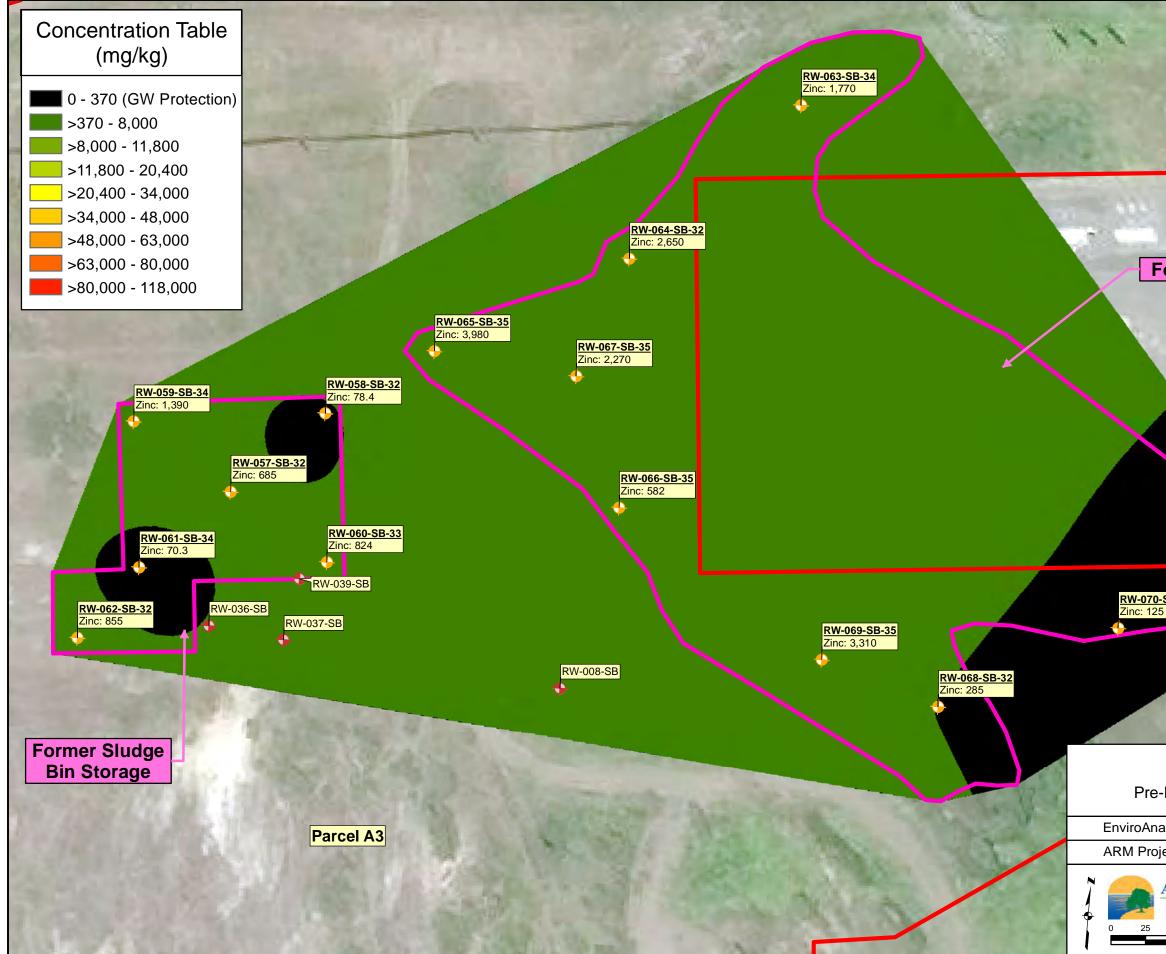


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Parcol A3 (P	od & Wiro Mill)	Figure
Soil Zind	od & Wire Mill) c Contours	S-13
e-Design Investig March 1	ation (16-20 feet bgs) 4, 2016	0-10
alytics Group	Tradepoint Atlantic	
oject 150298M	Baltimore County, ME)
ARM Group Inc. Earth Resource Engineers and Consultants 50 100 Feet	Phase II - Soil Boring Remedial Design Borin Area of Interest Parcel A3 (RWM) boundary	ng

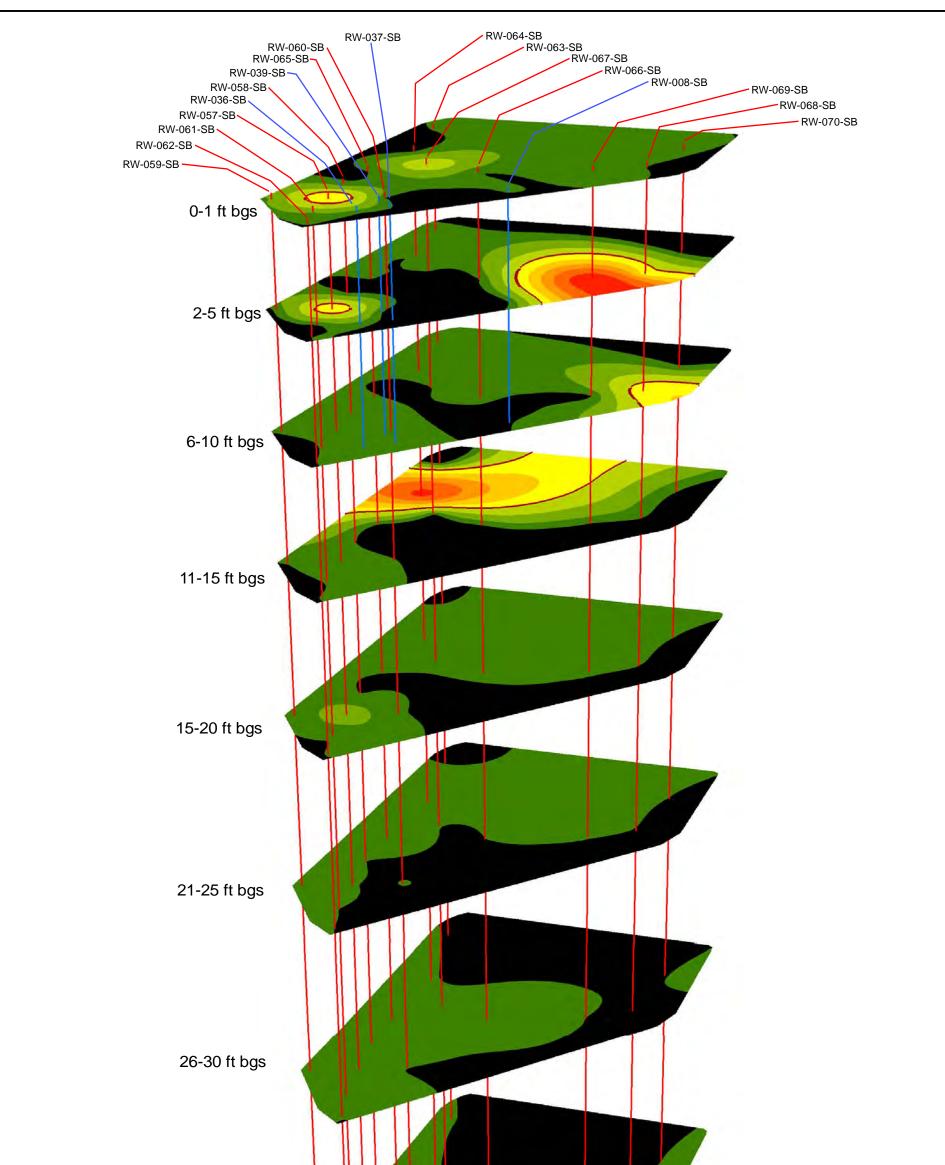


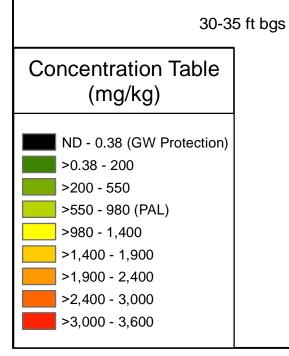


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	od & Wire Mill) c Contours	Figure
-Design Investig	ation (26-30 feet bgs)	S-15
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oject 150298M	Baltimore County, ME)
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ARM Group Inc. Earth Resource Engineers and Consultants	Remedial Design Bori	ng
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Feet	boundary	

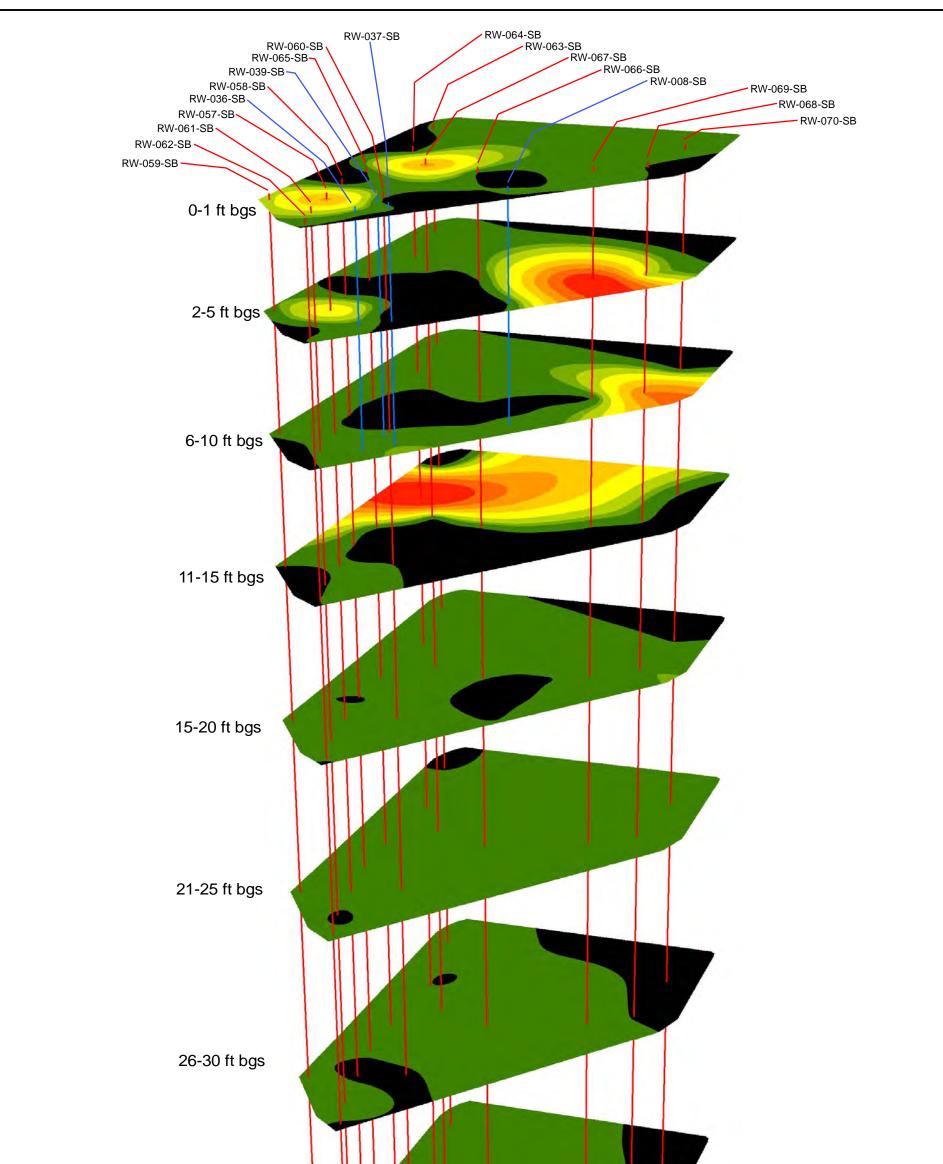


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9 <mark>-SB-32</mark>		NE UNIT
Parcel A3 (R	od & Wire Mill)	Figure
Soil Zind Design Investig-	c Contours Jation (31-35 feet bgs) ^{4, 2016}	S-16
alytics Group	Tradepoint Atlantic	
ARM Group Inc. Earth Resource Engineers and Consultants 50 100 Feet	Baltimore County, ME Phase II - Soil Boring Remedial Design Borin Area of Interest Parcel A3 (RWM) boundary	





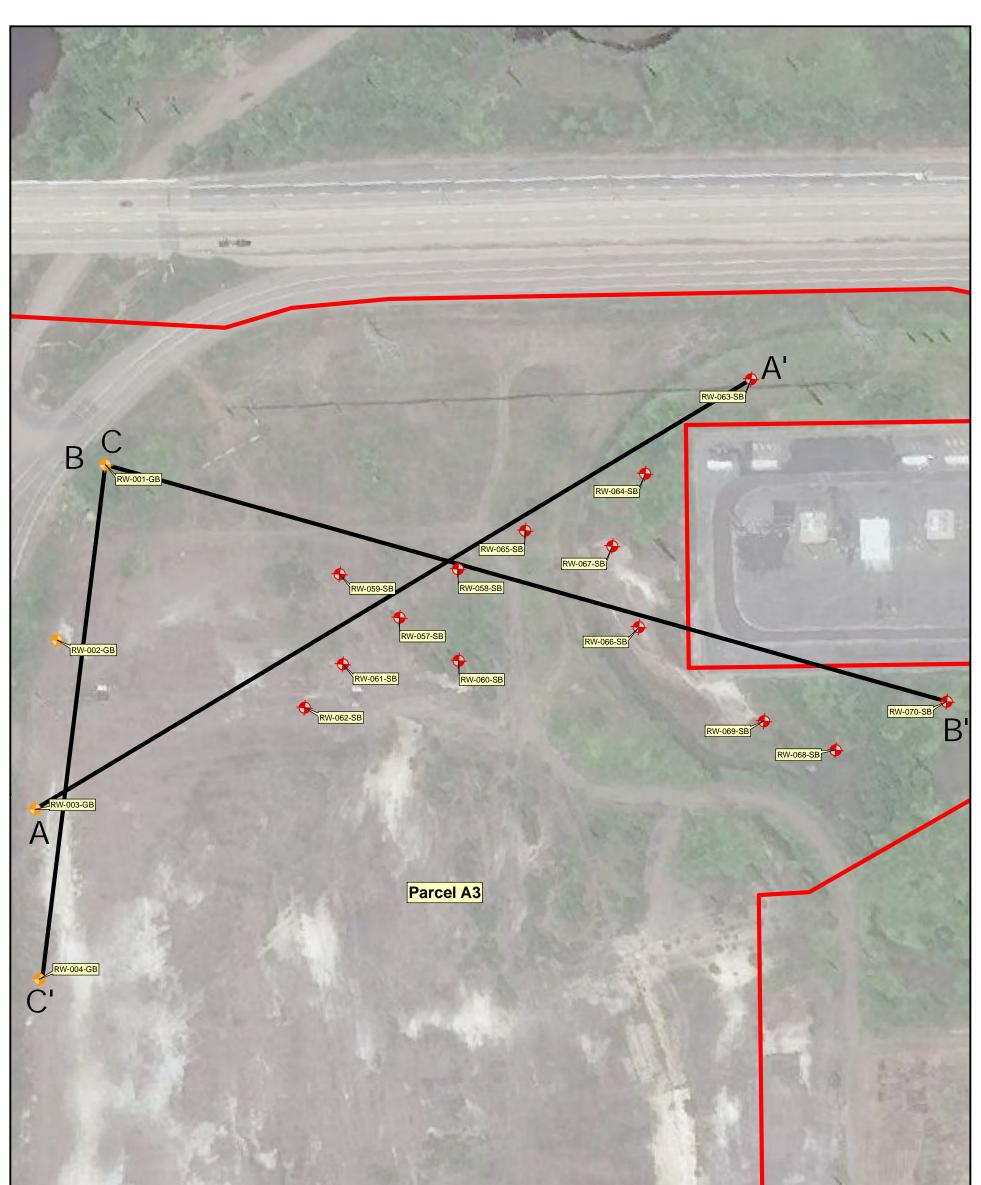
Soil Cadmium C	od & Wire Mill) Contours (mg/kg) gation (All Depths)
EnviroAnalytics Group	Tradepoint Atlantic
ARM Project 150298M	Baltimore County, MD
ARM Group Inc. Earth Resource Engineers and Consultants	 Phase II - Soil Boring Remedial Design Boring PAL Indicator Line



30-35 ft bgs

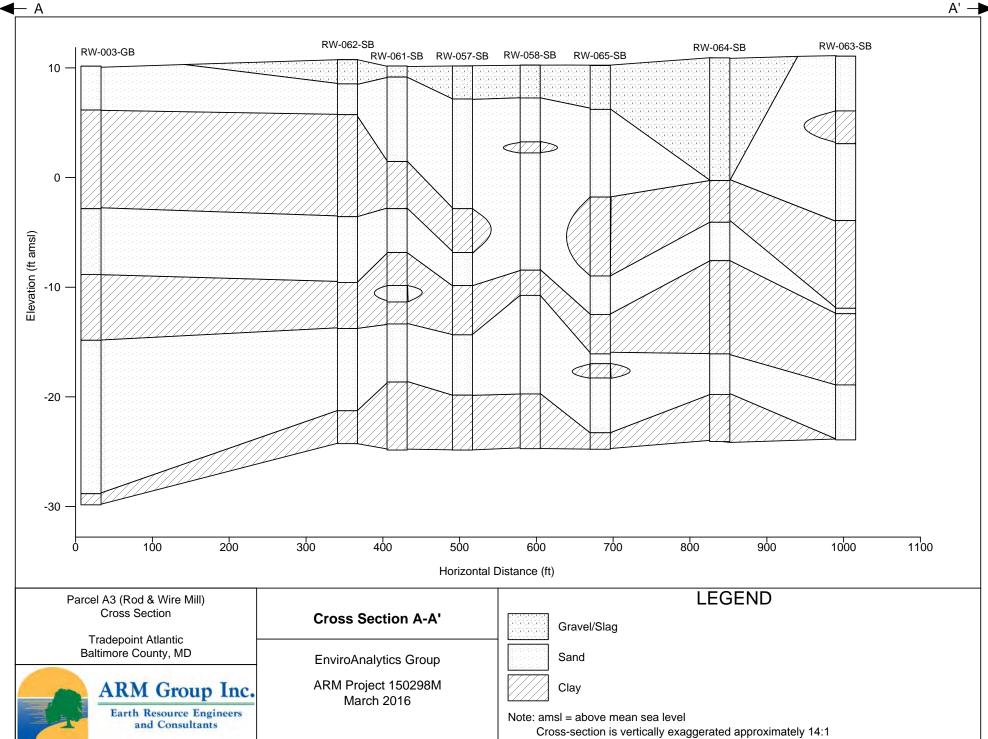
Concentration Table (mg/kg) 0 - 370 (GW Protection) >370 - 8,000 >8,000 - 11,800 >11,800 - 20,400 >20,400 - 34,000 >34,000 - 48,000 >48,000 - 63,000 >63,000 - 80,000 >80,000 - 118,000

Soil Zinc Cor Pre-Design Invest	od & Wire Mill) htours (mg/kg) igation (All Depths)	Figure 7
EnviroAnalytics Group	Tradepoint Atlantic	
ARM Project 150298M	Baltimore County, MI	C
ARM Group Inc.	Phase II - Soil BoringRemedial Design Borin	ng



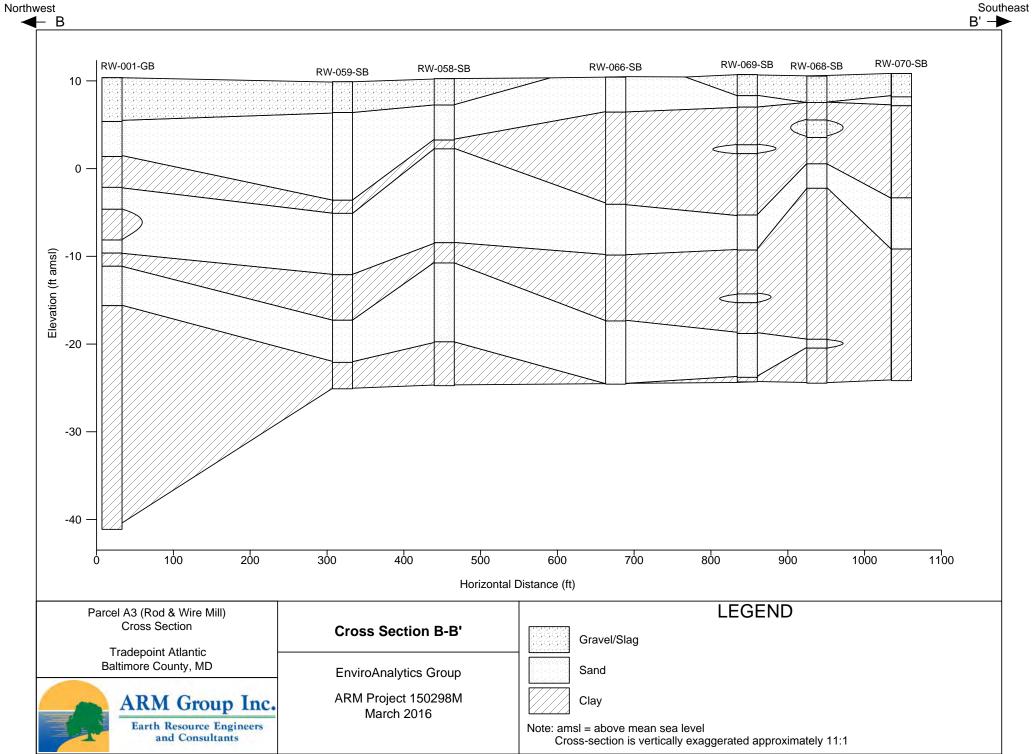
Cross Section	od & Wire Mill) on Map View 4, 2016	Figure 8
EnviroAnalytics Group	Sparrows Point Term	inal
ARM Project 150298M	Baltimore County, N	ИD
ARM Group Inc. Larib Resurve Engineers and Consultants 0 35 70 140 Feet	Remedial Design Approx Borings Section Geotechnical Borings	kimate cross- h line



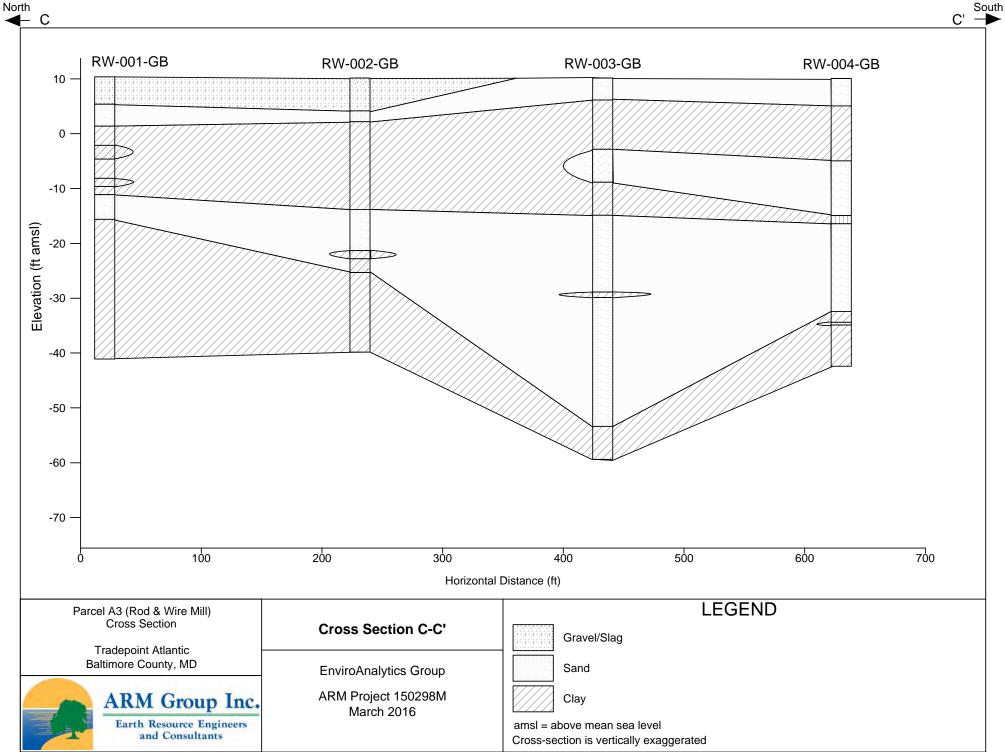


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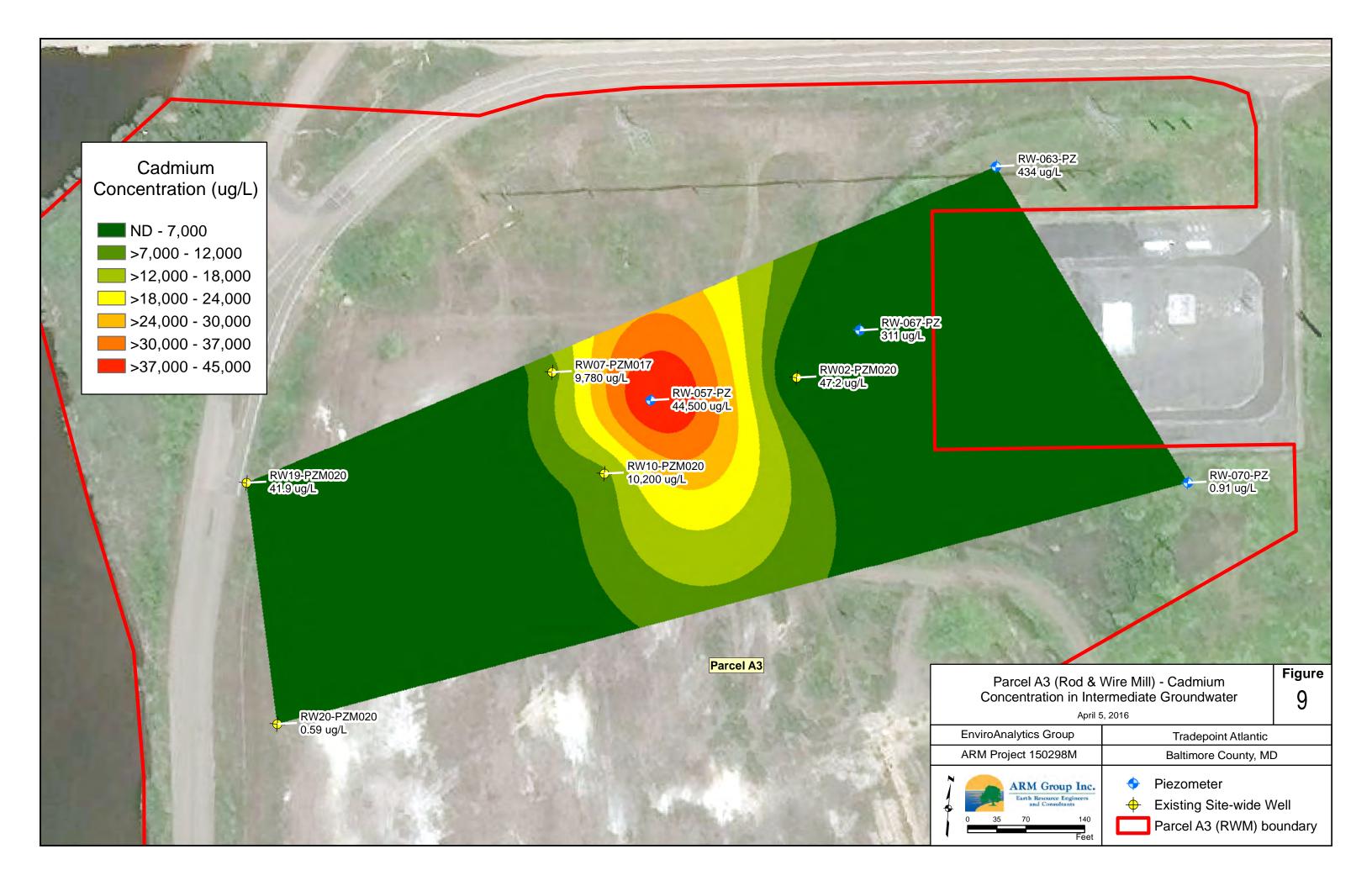
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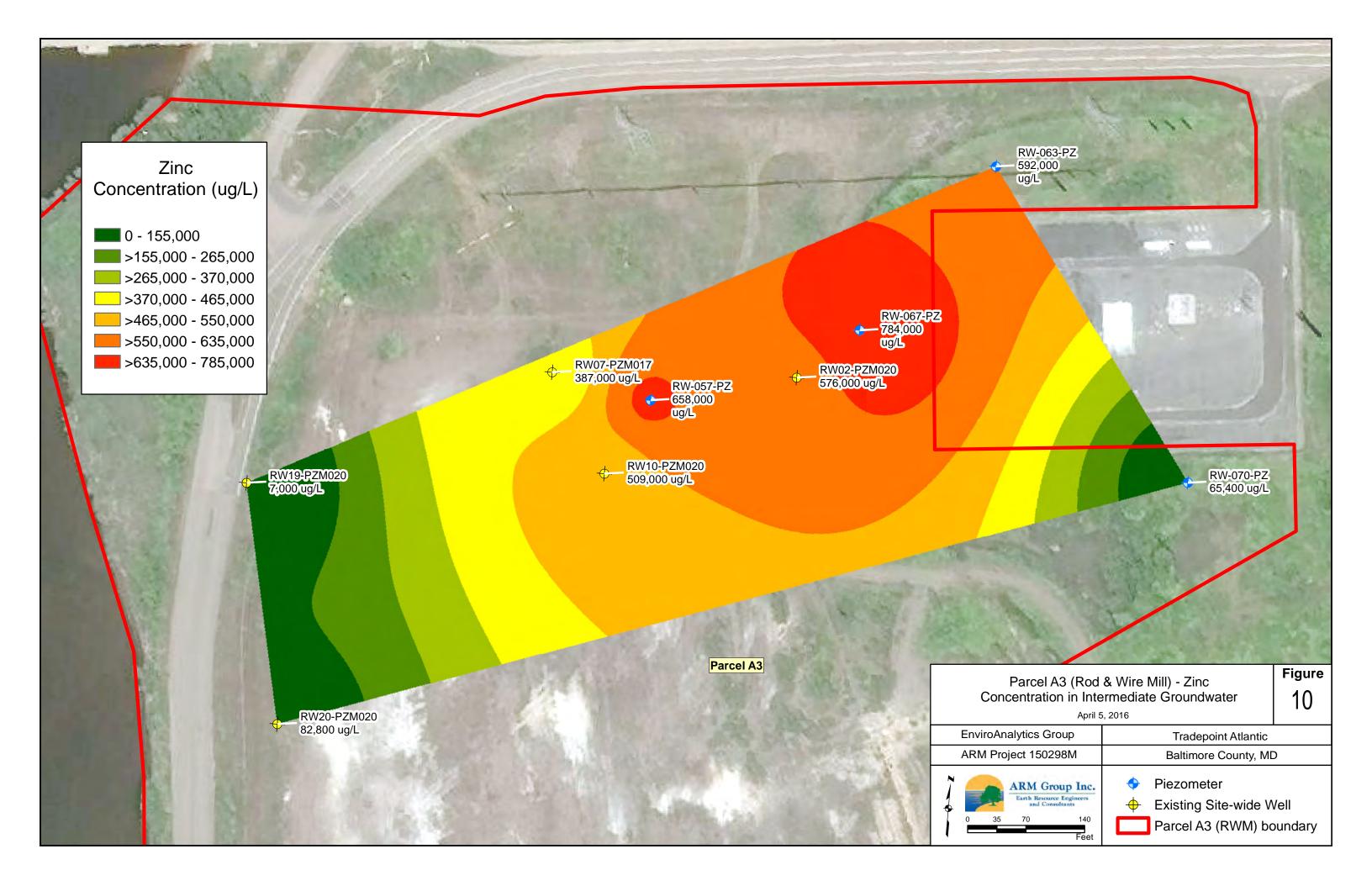


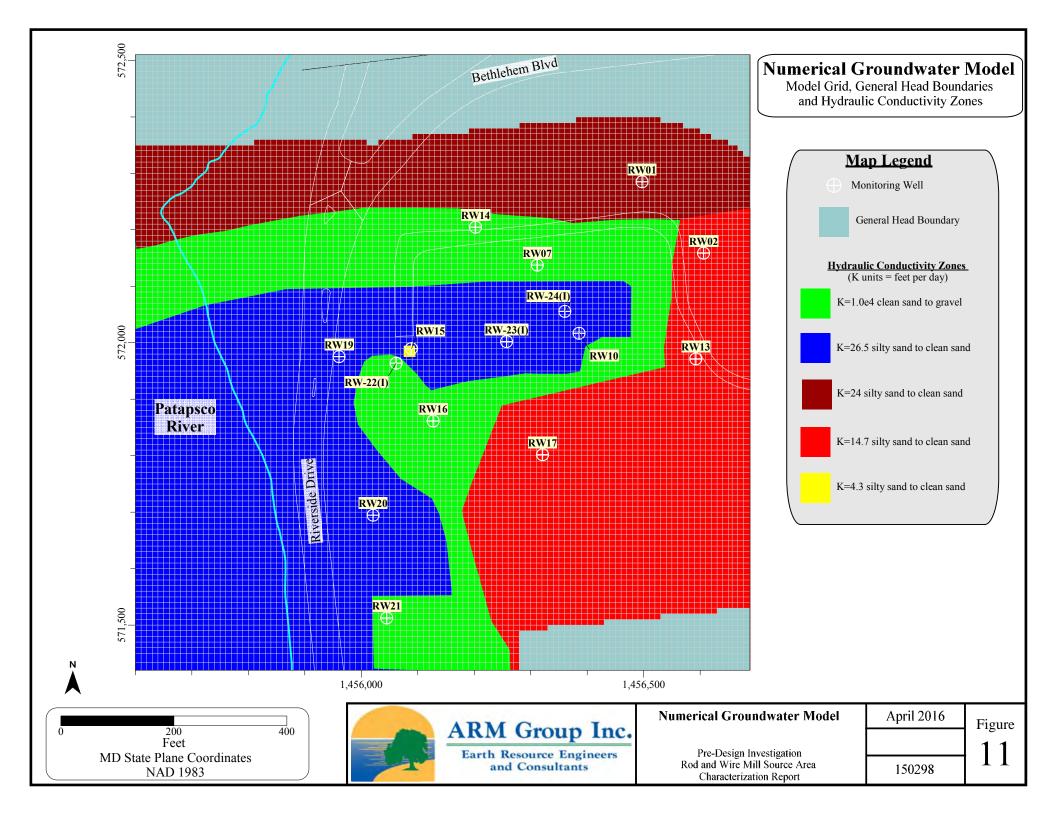
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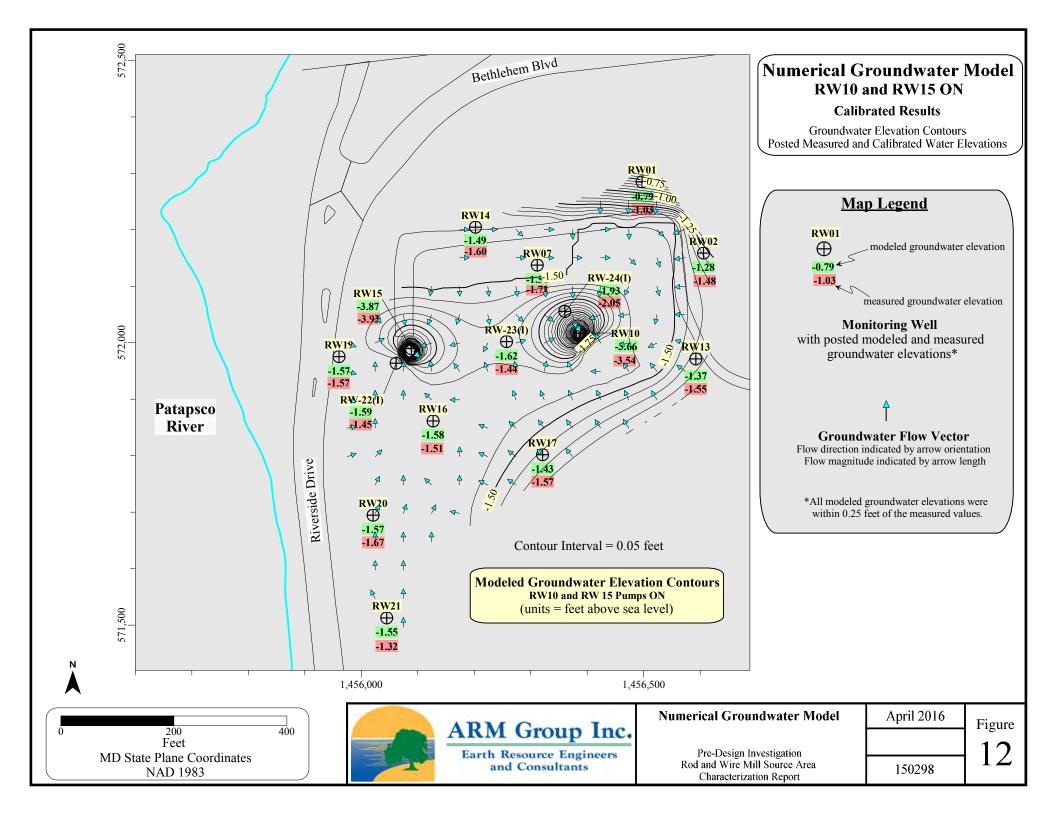


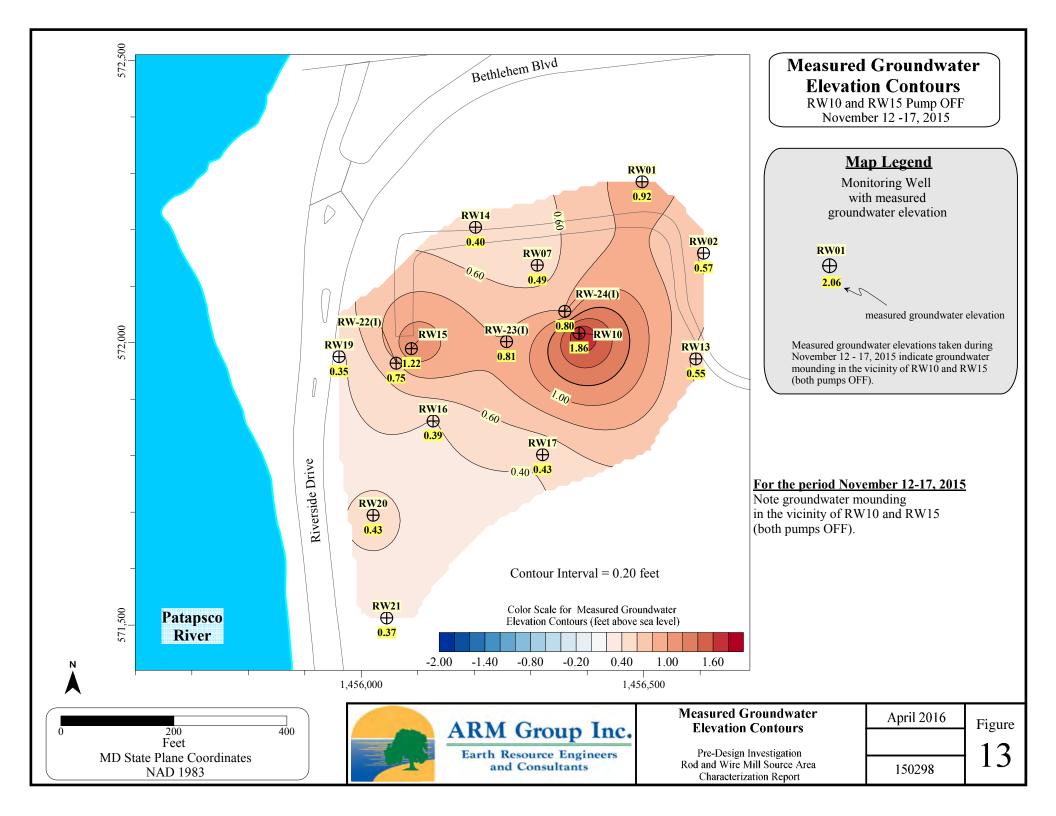
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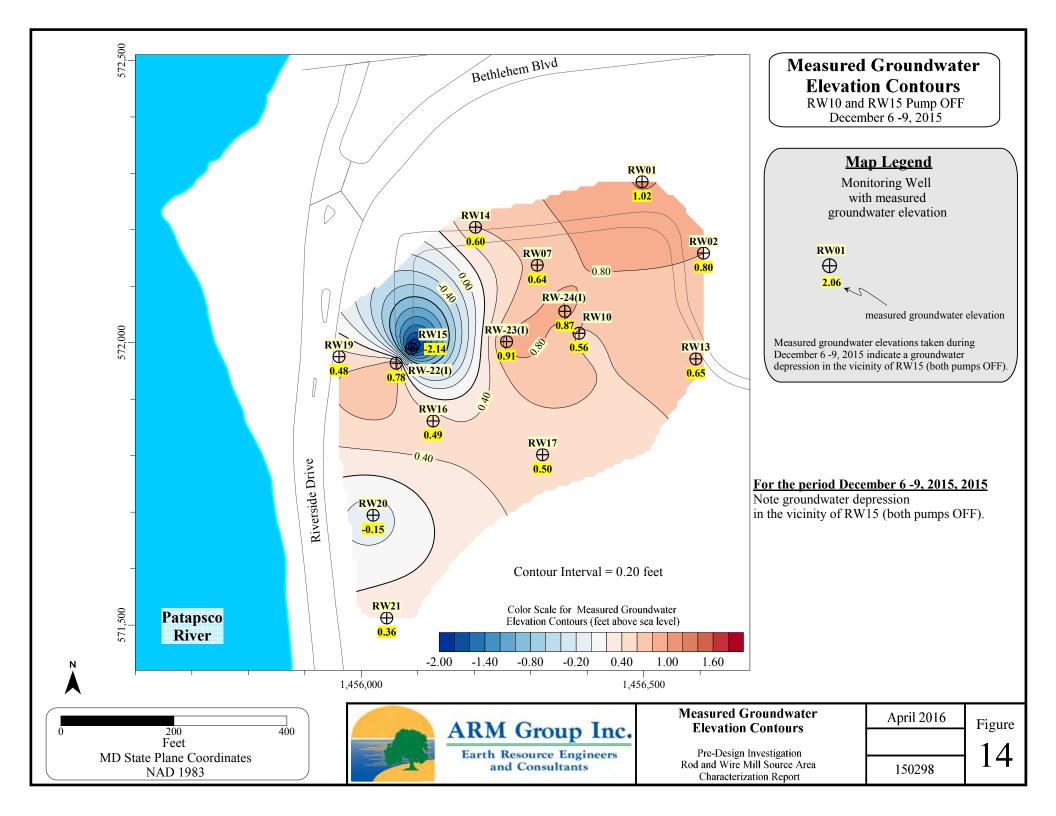


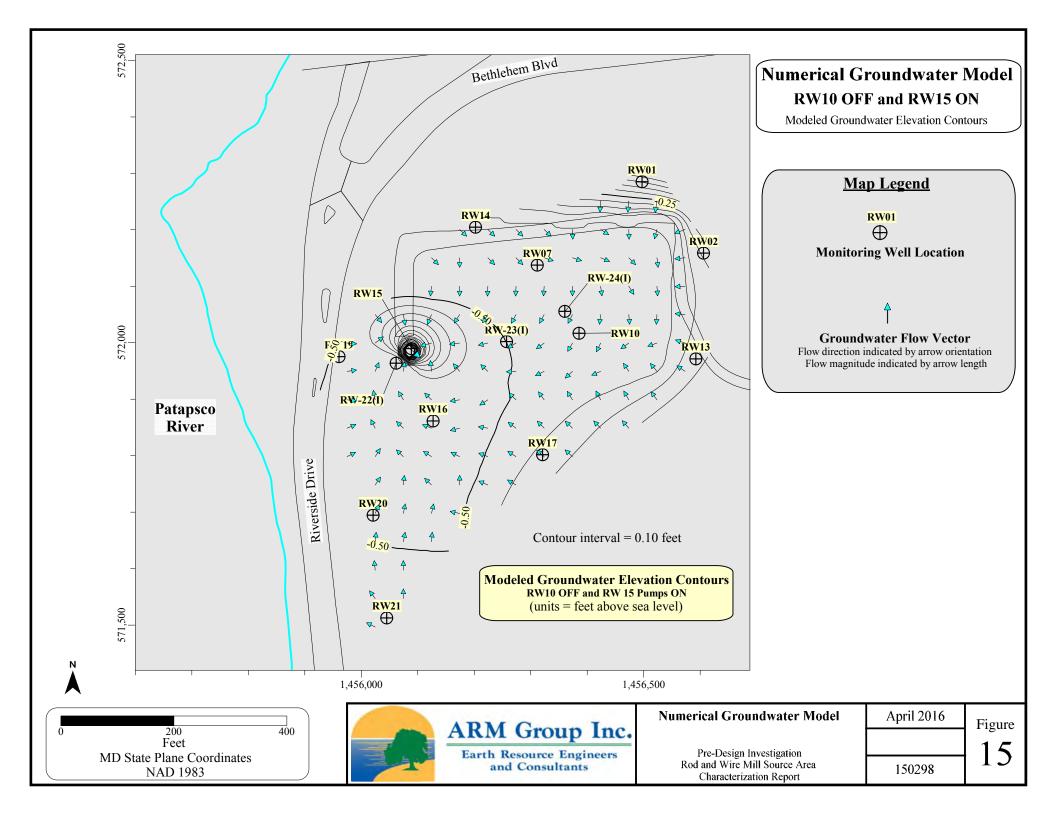


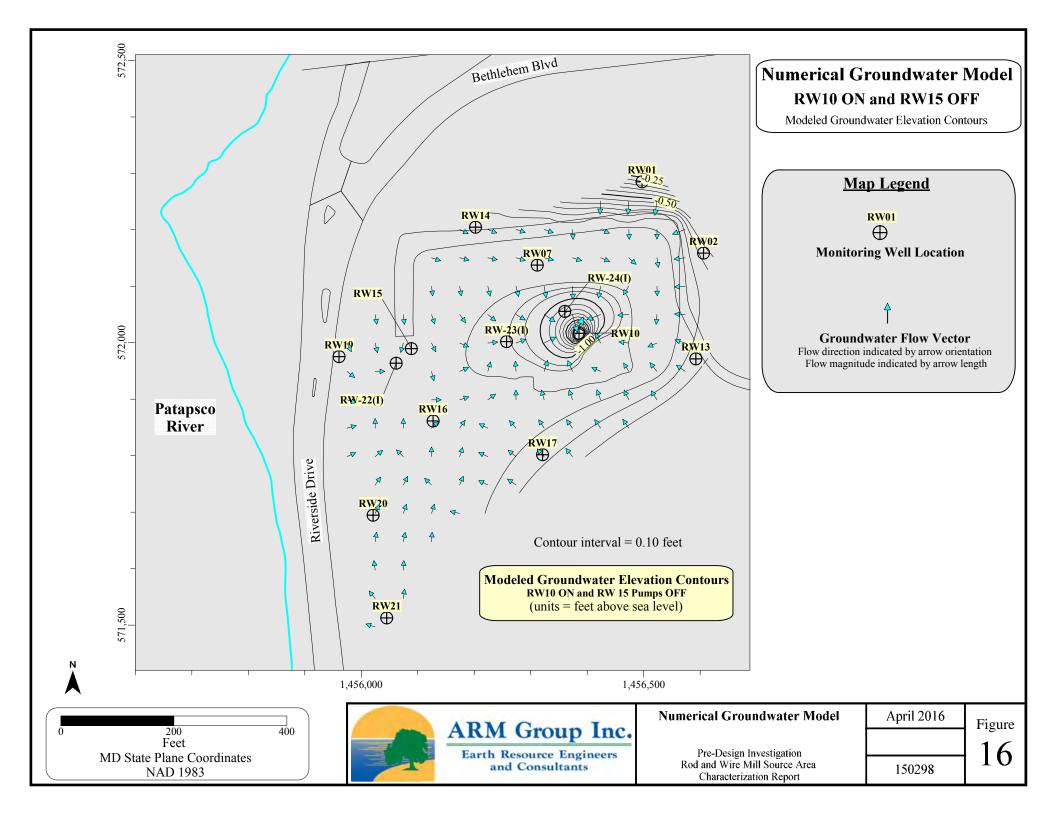


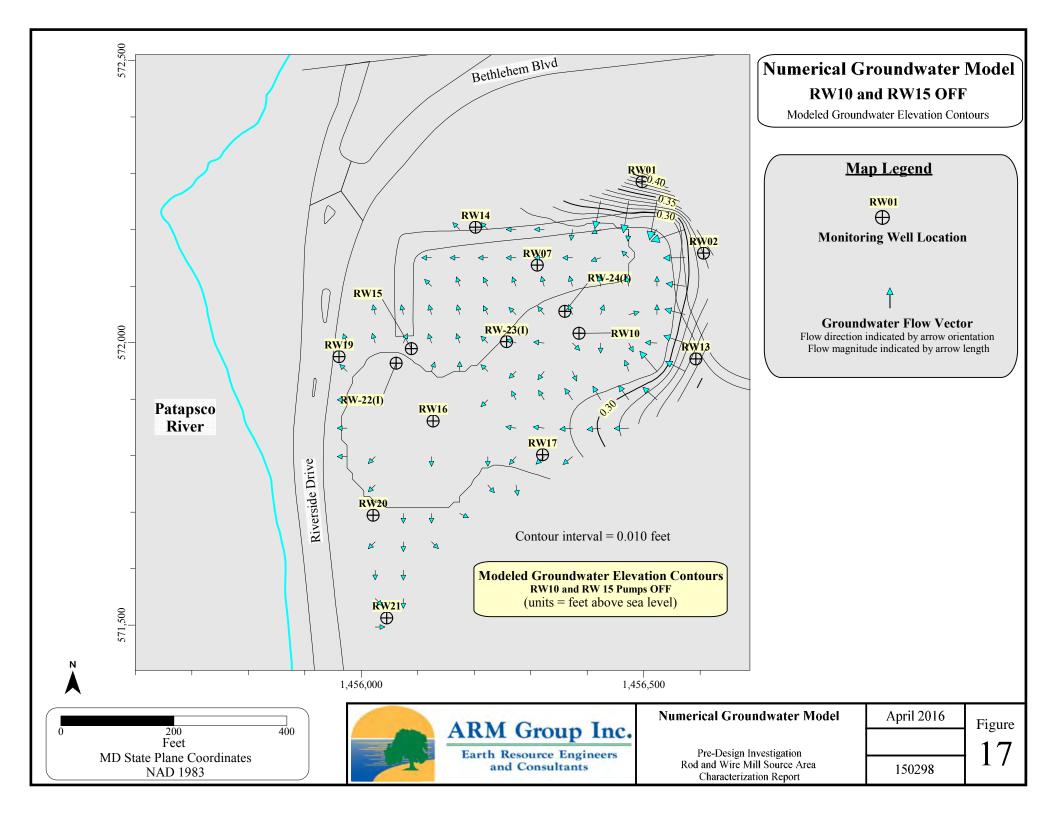


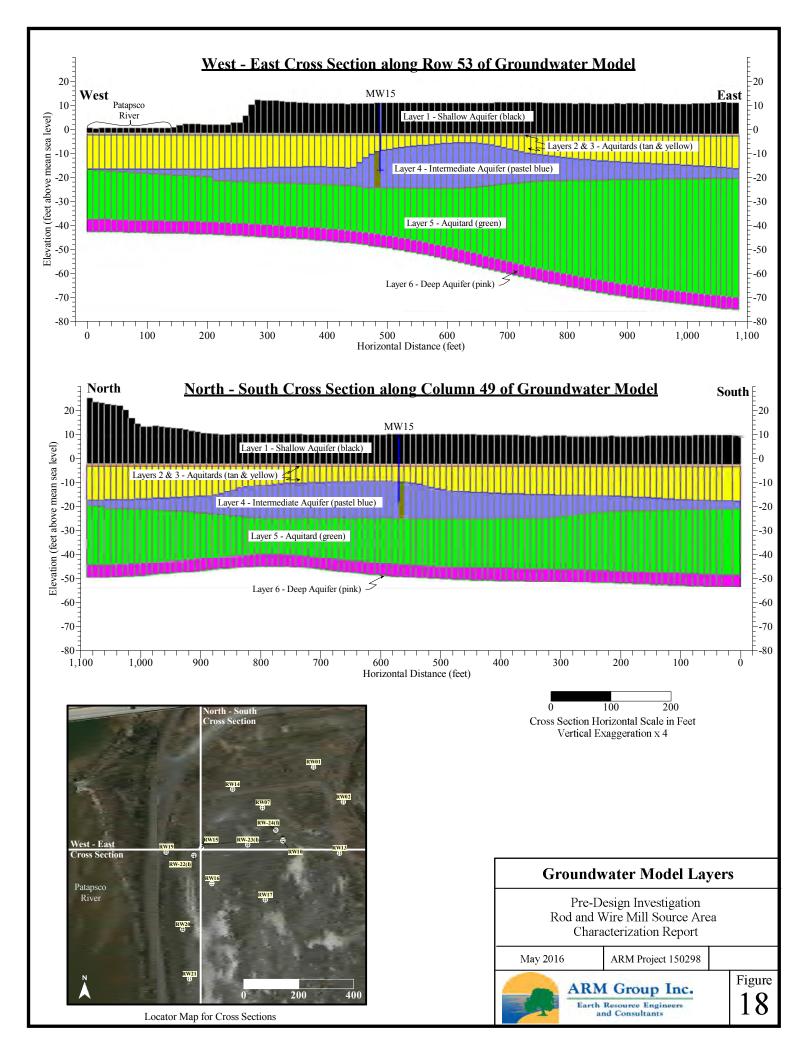


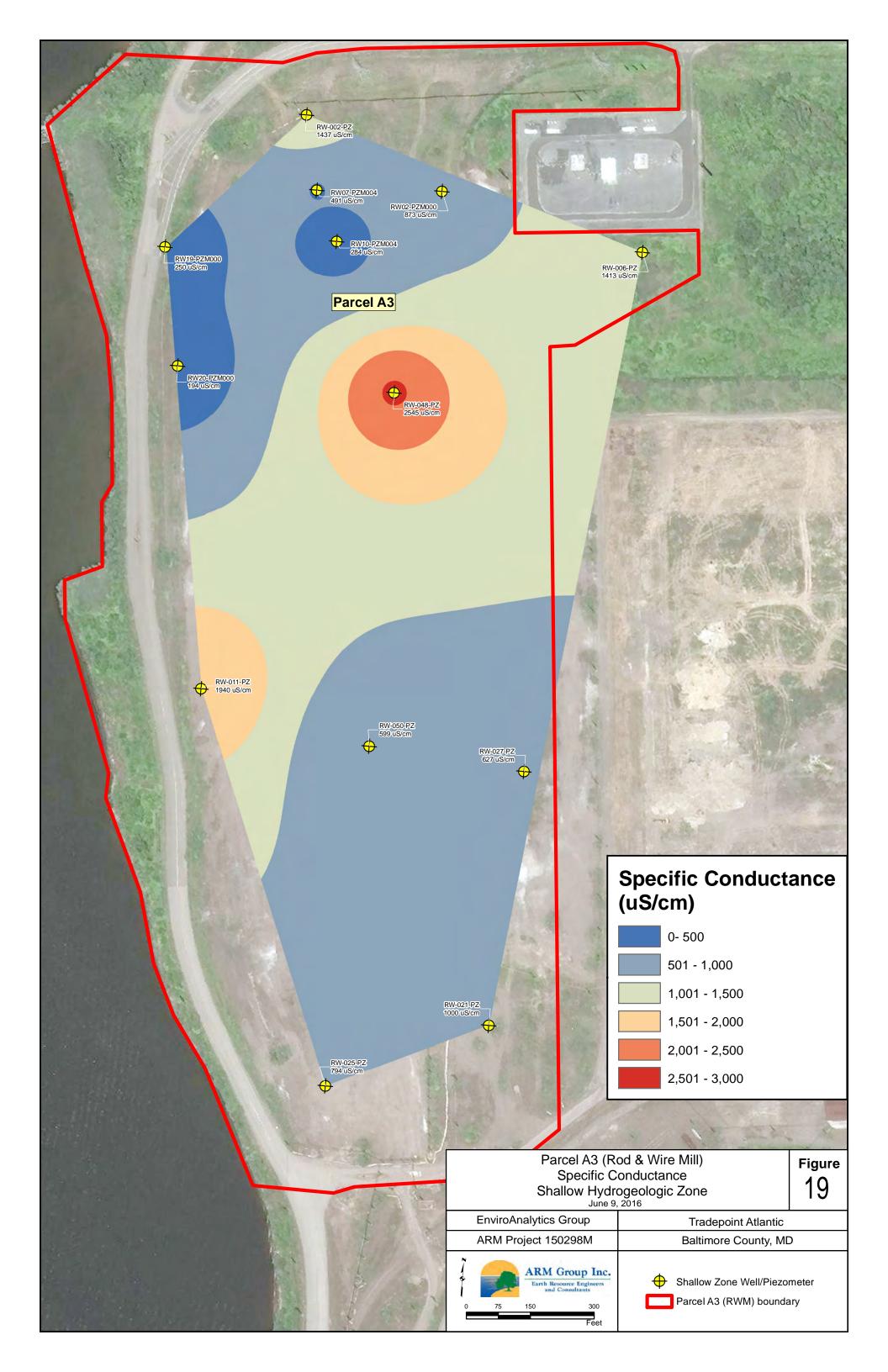


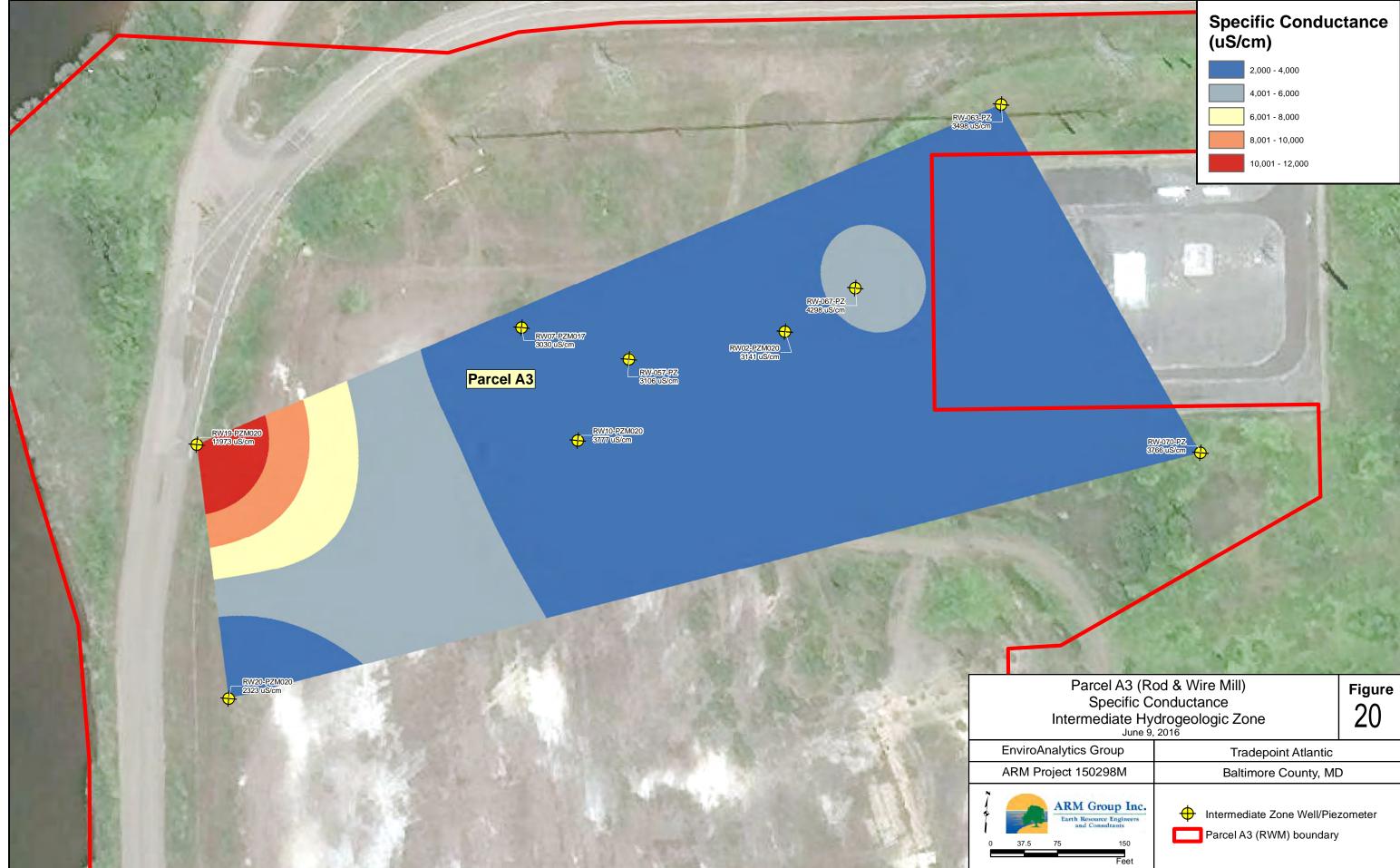












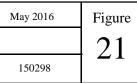
Group	Tradepoint Atlantic
)298M	Baltimore County, MD
Group Inc.	Intermediate Zone Well/Piezomete Parcel A3 (RWM) boundary

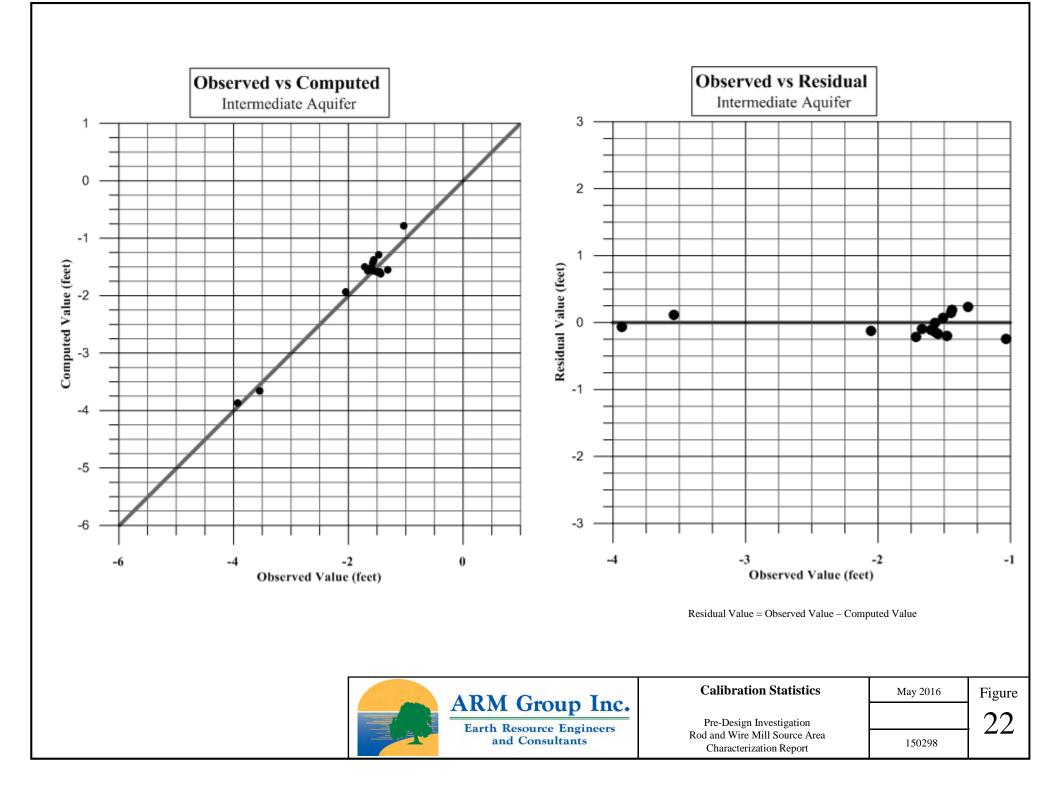
				P	• •	g Test M t below t					
Well Name	тос	Ground Elevation	Period 1 10 ON 15 ON	Period 2 10 OFF 15 OFF	Period 3 10 OFF 15 ON	Period 4 10 ON 15 ON	Period 5 10 OFF 15 OFF	Period 6 10 ON 15 OFF	Period 7 10 ON 15 ON	Period 8 10 ON 15 OFF	Period 9 10 OFF 15 OFF
RW01	12.72	10.15	13.8	11.8	11.75	13.25	11.75	11.75	13.3	12.7	11.7
RW02	13.02	10.27	14.5	12.45	12.3	13.75	12.15	12.35	13.95	13.32	12.22
RW07	12.94	10.71	14.8	12.45	12.4	14	12.2	12.4	14.3	13.4	12.3
RW10	11.86	11.47	15.4	10	9.8	15.07	12.75	12.86	15.05	14.8	11.3
RW13	13.05	11.17	14.6	12.5	12.4	13.95	12.3	12.4	14.22	13.43	12.4
RW14	13.6	11.24	15.2	13.2	13.22	14.55	12.88	12.99	14.89	13.93	13
RW15	12.17	11.84	16.1	10.95	17.04	18.35	14.32	14.34	17.88	15.28	14.31
RW16	13.89	11.65	15.4	13.5	13.45	14.91	13.2	13.21	15.26	14.24	13.4
RW17	13.73	11.43	15.3	13.3	13.25	14.73	13.05	13.05	15.13	14.1	13.23
RW19	13.53	11.28	15.1	13.18	13.1	14.6	12.89	12.9	14.91	13.86	13.05
RW20	13.03	11.14	14.9	12.6	12.6	14.5	n/a	n/a	14.8	n/a	13.18
RW21	12.93	10.86	14.05	12.56	12.5	13.8	12.29	12.3	14.18	13.31	12.57
RW-22(1)	11.25	11.25	12.6	10.5	10.6	12.01	10.24	10.29	12.34	11.28	10.47
RW-23(I)	11.46	11.46	12.9	10.65	10.6	12.23	10.41	10.55	12.55	11.6	10.55
RW-24(I)	11.05	11.05	12.93	10.25	10.27	12	10.05	10.43	12.31	11.5	10.18
red = estimate	d value			1 1 1 1			11.000				
RW10	Ave Pu	mping Rate	6.4	0	0	3	0	3.6	3.6	5	0
RW15		(gpm)	4.2	0	3.7	3.8	0	0	3.4	0	0

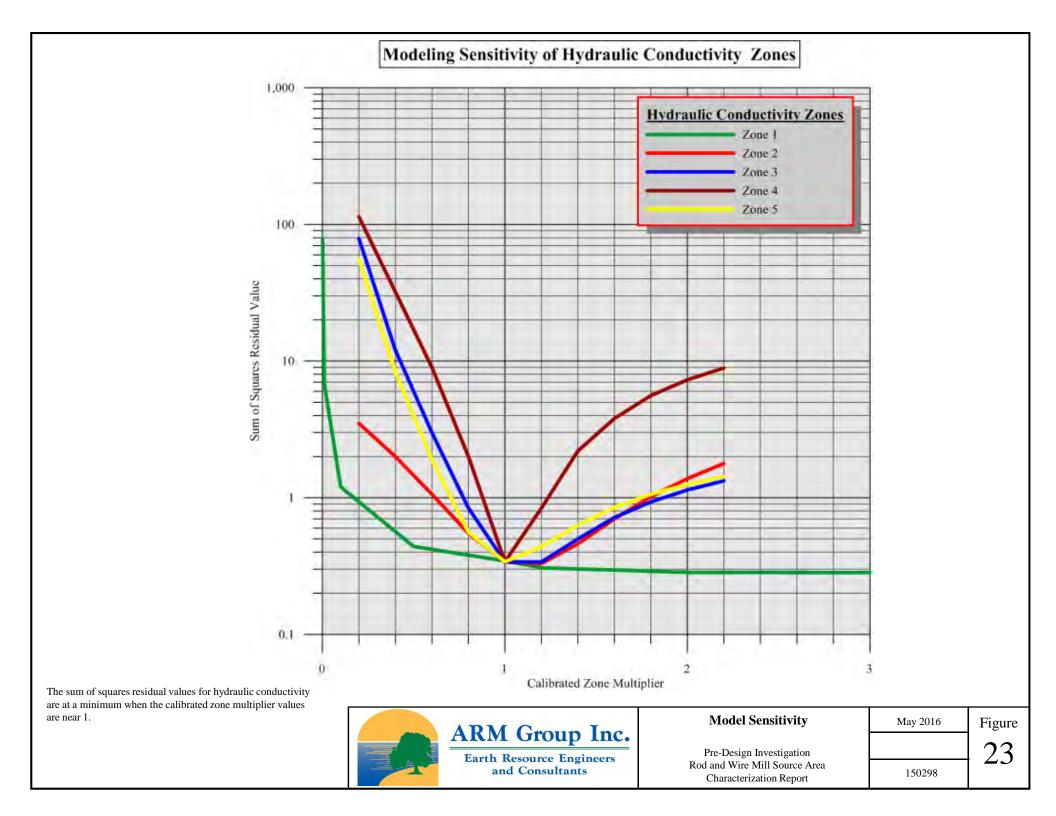


Pumping Test Measured Water Levels

Pre-Design Investigation Rod and Wire Mill Source Area Characterization Report







TABLES

TABLE 1 GROUNDWATER ELEVATION DATA								
Location Name	TOC Elevation (feet AMSL)	Ground Elevation (feet AMSL)	Measured DTW (ft)	Groundwater Elevation (feet AMSL)				
RW-057-PZ	13.14	10.17	13.42	-0.28				
RW-063-PZ	14.19	11.07	12.45	1.74				
RW-067-PZ	13.37	10.68	13.57	-0.20				
RW-070-PZ	14.14	10.84	9.27	4.87				
RW22 50ft	11.25	11.25*	11.60	-0.35				
RW23 50ft	11.46	11.46*	11.85	-0.39				
RW24 50ft	11.05	11.05*	11.55	-0.50				
RW01-PZM020	12.72	10.15	12.81	-0.09				
RW02-PZM020	13.02	10.27	13.34	-0.32				
RW07-PZM017	12.94	10.71	13.58	-0.64				
RW13-PZM020	13.05	11.17	13.50	-0.45				
RW14-PZM020	13.60	11.24	14.13	-0.53				
RW15-PZM020	12.17	11.84	13.87	-1.70				
RW16-PZM020	13.89	11.65	14.41	-0.52				
RW17-PZM019	13.73	11.43	14.26	-0.53				
RW19-PZM020	13.53	11.28	14.11	-0.58				
RW20-PZM020	13.03	11.14	14.09	-1.06				
RW21-PZM023	12.93	10.68	13.43	-0.50				
RW-RWBW-21	15.11	14.75	14.96	0.15				

DTW = Depth to water TOC = Top of casing

r

AMSL = Above mean sea level

* = Identical ground and TOC elevations may be due to survey error.

TABLE 2 FIELD SHIFTED BORING LOCATIONS									
Location ID Sample Target	<u>Proposed Location^{$¥$}</u>		<u>Final Location[¥]</u>		Relocation				
	Sample Target	<u>Northing</u>	<u>Easting</u>	<u>Northing</u>	Easting	Distance & Direction		<u>Rationale</u>	
RW-001-GB	None (geotechnical boring)	572,249	1,456,071	572,264	1,456,076	16 ft	NE	Shifted due to slag/refusal	
RW-068-SB	Former East Pond	571,966	1,456,972	572,004	1,456,961	39 ft	Ν	Standing water	
RW-069-SB	Former East Pond	572,021	1,456,896	572,031	1,456,874	24 ft	NW	Standing water*	

[¥]Reported northings and eastings are not survey accurate. Coordinates are reported in NAD 1983 Maryland State Plane (US feet). *RW-069-SB was shifted to allow for good spatial distribution after RW-068-SB was adjusted due to standing water/flooding.

TABLE 3 TCLP DETECTIONS FOR SOLID IDW								
Parameter	<u>Result (mg/L)</u>	<u>TCLP Limit</u> (mg/L)	<u>TCLP</u> Exceedance	<u>Laboratory</u> <u>Flag</u>	Laboratory LOQ (mg/L)			
2-Butanone (MEK)	0.0069	200	No	JB	5			
Arsenic	0.0045	5	No	J	0.05			
Barium	0.15	100	No	J	1			
Cadmium	0.06	1	No		0.05			
Chromium	0.0046	5	No	J	0.05			
Lead	0.021	5	No	J	0.25			

J = The positive result reported for this analyte is a quantitative estimate below the laboratory PQL.

JB = The positive result reported for this analyte is an estimate with evidence of blank contamination.

TCLP = Toxicity characteristic leaching procedure

LOQ = Limit of Quantitation

	TCI	-	ABLE 4 ONS FOR LIC	QUID IDW		
Location ID	Parameter	<u>Result</u> (mg/L)	TCLP Limit (mg/L)	<u>TCLP</u> Exceedance	<u>Laboratory</u> <u>Flag</u>	Laboratory LOQ (mg/L)
Water Disposal 1	Barium	0.0338	100	No		0.01
Water Disposal 1	Cadmium	0.0006	1	No	J	0.003
Water Disposal 1	Chromium	0.0016	5	No	J	0.005
Water Disposal 2	Barium	0.0811	100	No		0.01
Water Disposal 2	Chloroform	0.0029	6	No		0.001
Water Disposal 2	Chromium	0.0012	5	No	J	0.005
Water Disposal 3	Barium	0.0051	100	No	J	0.01
Water Disposal 3	Chloroform	0.0016	б	No		0.001
Water Disposal 3	Chromium	0.00085	5	No	J	0.005
Water Disposal 4	Arsenic	0.0094	5	No		0.005
Water Disposal 4	Barium	0.101	100	No		0.01
Water Disposal 4	Chloroform	0.0024	б	No		0.001
Water Disposal 4	Chromium	0.0012	5	No	J	0.005
Water Disposal 5	Barium	0.398	100	No		0.01
Water Disposal 5	Cadmium	0.00058	1	No	J	0.003
Water Disposal 5	Chloroform	0.0039	б	No		0.001
Water Disposal 5	Chromium	0.0012	5	No	J	0.005
Water Disposal 6	Barium	2.14	100	No		0.01
Water Disposal 6	Cadmium	0.001	1	No	J	0.003
Water Disposal 6	Chloroform	0.00058	6	No	J	0.001
Water Disposal 7	Barium	0.0889	100	No		0.01
Water Disposal 7	Cadmium	0.00067	1	No	J	0.003
Water Disposal 7	Chloroform	0.00075	6	No	J	0.001
Water Disposal 7	Trichloroethene	0.00065	0.5	No	J	0.001
Water Disposal 8	Barium	0.01	100	No	J	0.01

J = The positive result reported for this analyte is a quantitative estimate below the laboratory PQL.

TCLP = Toxicity characteristic leaching procedure

LOQ = Limit of Quantitation

		RW-057-S	B- 1	RW-057-SI	B-3	RW-057-SI	B-6	RW-057-SB	B -15	RW-057-SI	3-16	RW-057-SF	B- 23	RW-057-SI	3-29	RW-057-SI	B-32
Parameter	Units	Soil		Soil		Soil		Soil		Soil		Soil		Soil		Soil	
		10/1/201	5	10/1/201	5	10/1/201	5	10/1/201	5	10/1/201	5	10/1/201	5	10/1/201	5	10/1/201	15
Validated Metals																	
Arsenic	mg/kg	31.8		6.4		3.2		9.3		1.9	J	1.8	J	2.2	U	1.9	U
Barium	mg/kg	1,670	J	454	J	13.6	J	20.7	J	24.2	J	62.2	J	1.7	В	29.4	J
Cadmium	mg/kg	1,420	J	1,290	J	10.3	J	164	J	323	J	6.9	J	5.2	J	76.3	J
Chromium	mg/kg	16.3	J	22.9	J	6.9	J	10.5	J	13.3	J	38.3	J	1.1	J	27.1	J
Lead	mg/kg	1,730		743		4.5		5		6.3		13		2.2	U	6.3	
Mercury	mg/kg	0.12	U	0.085	J	0.0089	J	0.0087	J	0.017	J	0.03	J	0.11	U	0.0064	J
Selenium	mg/kg	4.3	U	2.5	В	3.2	U	4.6	U	3.8	U	3.5	U	3.5	U	3	U
Silver	mg/kg	4.5		1.7	J	2.4	U	3.5	U	2.8	U	2.6	U	2.6	U	2.3	U
Non-Validated Metals																	
Aluminum	mg/kg	32,300	Е	17,700		4,740		5,700		6,380		14,900		417		5,820	
Antimony	mg/kg	2.6	J	3.2	U	2.4	U	3.5	U	2.8	U	2.6	U	2.6	U	2.3	U
Beryllium	mg/kg	2.3		0.85	J	0.17	J	0.27	J	0.31	J	0.81	J	0.87	U	0.38	J
Cobalt	mg/kg	3.3	J	5.8		1.6	J	6.7		2.3	J	11.1		4.4	U	6.2	
Copper	mg/kg	237		90.1		4.8		5.9		7.8		17.7		4.4	U	12.8	
Iron	mg/kg	31,400	E	18,200		7,340		6,460		4,520		22,800	E	899		3,800	
Manganese	mg/kg	6,840	E	3,150	E	38.9		39		41.4		151		4.7		36.3	
Nickel	mg/kg	14.3		13		3.2	J	7.4	J	5.7	J	30.6		8.7	U	19.9	
Thallium	mg/kg	10.8	U1c	10.7	U1c	8	U1c	11.5	U1c	9.5	U1c	8.8	U1c	8.7	U1c	7.6	U1c
Vanadium	mg/kg	607		107		12.6		12.9		16.8		48.1		1.5	J	21.1	
Zinc	mg/kg	49,700	E	29,700	E	885		820		1,050		1,170		84.3		685	

Detections in bold

		RW-058-S	B-1	RW-058-S	B-2	RW-058-SI	3-8	RW-058-SB	8-15	RW-058-SE	B -20	RW-058-SB	-22	RW-058-SE	-28	RW-058-SH	3-32
Parameter	Units	Soil		Soil		Soil		Soil		Soil		Soil		Soil		Soil	
		10/5/201	5	10/5/201	5	10/5/201:	5	10/5/201	5	10/5/201	5	10/5/201	5	10/5/201	5	10/5/201	5
Validated Metals																	
Arsenic	mg/kg	80.6	J	8.9	J	2.5		4.9	J	2.2	U	6.2	J	1.6	В	5.8	J
Barium	mg/kg	216		53.7		27		16.2		11.5		36.3		33		107	
Cadmium	mg/kg	91.5	J	32	J	17.4		4.9	J	0.32	В	1.5	J	54.3	J	0.41	В
Chromium	mg/kg	37.5	J	15.9	J	11.9		10.6	J	7.7	J	24.5	J	23.1	J	46	J
Lead	mg/kg	29.8	J	10.7	J	4.6		3.4	J	3.6	J	9.6	J	6.6	J	8.9	J
Mercury	mg/kg	0.19		0.062	J	0.0047	J	0.016	J	0.0029	J	0.026	J	0.0062	J	0.045	J
Selenium	mg/kg	3.3	U	3	U	3.5	U	4.7	U	3.5	U	3.3	U	2.9	U	5.1	U
Silver	mg/kg	2.5	U	2.3	U	2.6	U	3.5	U	2.6	U	2.5	U	2.2	U	3.8	U
Non-Validated Metals																	
Aluminum	mg/kg	21,500	E	11,100		9,230		6,770		4,510		9,140		9,420		11,200	
Antimony	mg/kg	2.5	U	2.3	U	2.6	U	3.5	U	2.6	U	2.5	U	2.2	U	3.8	U
Beryllium	mg/kg	1.7		0.42	J	0.35	J	0.21	J	0.88	U	0.37	J	0.42	J	2	
Cobalt	mg/kg	10.8		5.3		2.4	J	1.5	J	1.1	J	2.8	J	4.2		38	
Copper	mg/kg	34.9		7.4		9.4		11.6		4.7		12.7		7.4		33.4	
Iron	mg/kg	30,200	E	15,400	E	6,890		10,100		4,630		28,800	Е	16,100	Е	11,900	
Manganese	mg/kg	569		246		48.1		28		35.1		106		79.1		49.6	
Nickel	mg/kg	20.8		7.6		9		4.2	J	3.2	J	10.6		10.8		35.6	
Thallium	mg/kg	8.3	U	7.6	U	8.7	U	11.7	U	8.8	U	8.2	U	7.4	U	12.7	U
Vanadium	mg/kg	NA		NA		NA		NA		NA		NA		NA		NA	
Zinc	mg/kg	1,720	E	709		342		210		348		885		738		78.4	

Detections in bold

		RW-059-SI	B-1	RW-059-SI	B-3	RW-059-S	B-6	RW-059-SE	8-11	RW-059-SH	3-20	RW-059-SE	B- 23	RW-059-SE	3-26	RW-059-SI	B-34
Parameter	Units	Soil		Soil		Soil		Soil		Soil		Soil		Soil		Soil	
		10/1/201	5	10/1/201	5	10/1/201	5	10/1/201	5	10/1/201	5	10/1/201	5	10/1/201	5	10/1/201	5
Validated Metals																	
Arsenic	mg/kg	235		6.4		4.3		2.2		2.9	U	24.3		3.3	U	2.7	В
Barium	mg/kg	946		166	J	16.3	J	10.8	J	8.8	J	78.3	J	130	J	67.2	J
Cadmium	mg/kg	226		38.2	J	1.6	J	8.5	J	64.9	J	180	J	29.1	J	36.7	J
Chromium	mg/kg	115	J	16.2	J	9.9	J	5	J	6.9	J	67.1	J	35.6	J	50.2	J
Lead	mg/kg	3,130	J	363		4.8		2.7		2.9	U	27.8		21.7		13.1	
Mercury	mg/kg	0.12		0.75		0.015	J	0.0045	J	0.0087	J	0.044	J	0.021	J	0.047	J
Selenium	mg/kg	3	J	3.5	U	4.4	U	2.6	U	4.6	U	5.1	U	5.2	U	2.6	В
Silver	mg/kg	2.4	U	2	J	3.3	U	2	U	3.4	U	3.8	U	3.9	U	3.4	U
Non-Validated Metals																	
Aluminum	mg/kg	34,800	Е	7,030		6,630		2,810		2,040		17,300		19,100		12,300	
Antimony	mg/kg	2.4	U	2.6	U	3.3	U	2	U	3.4	U	3.8	U	3.9	U	3.4	U
Beryllium	mg/kg	2.6		0.59	J	1.1	U	0.15	J	1.1	U	0.79	J	2.4		2.2	
Cobalt	mg/kg	3.3	J	2.2	J	1.2	J	0.61	J	1.2	J	11.8		18.9		36.8	
Copper	mg/kg	228		105		7.1		7.3		5.7	U	345		22.2		28.4	
Iron	mg/kg	20,500	E	10,500		8,950		2,380		1,180		17,700		17,500		16,400	
Manganese	mg/kg	9,550	E	294		104		22.4		26.9		148		162		79.6	
Nickel	mg/kg	18.6		8.1	J	3.2	J	1.9	J	1.9	J	22.5		44.8		40.7	
Thallium	mg/kg	8	U	8.7	U1c	11.1	U1c	6.5	U1c	11.5	U1c	12.7	U1c	13.1	U1c	11.4	U1c
Vanadium	mg/kg	645		17.2		15.4		9.8		6.8		36.9		52.6		67	
Zinc	mg/kg	17,600	E	5,300	E	565		147		1,110		3,850	E	699		1,390	

Detections in bold

		RW-060-SI	B-1	RW-060-SI	B- 4	RW-060-SI	B-7	RW-060-SB	8-12	RW-060-SE	B -20	RW-060-SB	8-22	RW-060-SE	8-26	RW-060-S	B-33
Parameter	Units	Soil		Soil		Soil		Soil		Soil		Soil		Soil		Soil	
		10/5/201	5	10/5/201	5	10/5/201	5	10/5/201	5	10/5/201	5	10/5/201	5	10/5/201	5	10/5/201	5
Validated Metals																	
Arsenic	mg/kg	2.3	J	4.7		5		2.1	J	8		3		3.3		4.6	
Barium	mg/kg	49.2		26		1,590		38.4		18.5		67		6.4	J	58.4	
Cadmium	mg/kg	3.4		11.9		23.1		17.1		23		1.2	В	0.58	В	183	
Chromium	mg/kg	3	В	10.7		27.1		16.1		10.5		40		5.1		36.7	
Lead	mg/kg	150		243		23.8		8		2.7		14.9		2.6	U	7.8	
Mercury	mg/kg	0.14		0.02	J	0.0037	J	0.039	J	0.0095	J	0.026	J	0.11	U	0.03	J
Selenium	mg/kg	4	U	3.6	U	3.8	U	4.1	U	3.6	U	3.4	U	4.2	U	3	U
Silver	mg/kg	3	U	2.7	U	2.9	U	3	U	2.7	U	2.6	U	3.2	U	2.3	U
Non-Validated Metals										-							
Aluminum	mg/kg	1,060		5,880		16,100		10,400		3,860		14,400		1,130		9,600	
Antimony	mg/kg	3	U	2.7	U	2.9	U	2.2	J	2.7	U	2.6	U	3.2	U	2.3	U
Beryllium	mg/kg	1	U	0.15	J	0.54	J	0.39	J	0.47	J	2		1.1	U	0.52	J
Cobalt	mg/kg	5	U	1.7	J	4.5	J	7.2		9.1		19		5.3	U	8.8	
Copper	mg/kg	9.2		17.2		12.5		11.3		5.9		21.8		2.4	J	19.3	
Iron	mg/kg	2,200		12,700		14,800		7,920		4,950		19,700	Е	10,200		9,260	
Manganese	mg/kg	17.3		37		88.5		75.3		34.4		194		28.3		47.8	
Nickel	mg/kg	10	U	5	J	11.5		17.4		10.4		35.1		1	J	16.7	
Thallium	mg/kg	10	U	9.1	U	9.5	U	10.2	U	8.9	U	8.5	U	10.6	U	7.6	U
Vanadium	mg/kg	NA		NA		NA		NA		NA		NA		NA		NA	
Zinc	mg/kg	88.2		188		1,090		362		883		4,040	Е	67.4		824	

Detections in bold

		RW-061-S	B-1	RW-061-SI	3-2	RW-061-SI	B-7	RW-061-SE	8-11	RW-061-SE	8-19	RW-061-SB	-21	RW-061-SE	8-29	RW-061-SI	B-34
Parameter	Units	Soil		Soil		Soil		Soil		Soil		Soil		Soil		Soil	
		10/5/201	5	10/5/201	5	10/5/201	5	10/5/201	5	10/5/201	5	10/5/2013	5	10/5/201	5	10/5/201	5
Validated Metals																	
Arsenic	mg/kg	5.6	J	3.9		11.3		2.2	U	2.3	J	5		6.8		3.4	U
Barium	mg/kg	676		75.1		35.3		39.6		76.6		66.5		54.4		43	
Cadmium	mg/kg	210	J	8.3		1.1	В	7.8		3		0.56	В	73.9		2	U
Chromium	mg/kg	57.5	J	12.5		25.1		18.2		43.1		36.8		43.6		37.9	J
Lead	mg/kg	677	J	102		12.7		16.6		13.8		13.4		12.5		8.5	J
Mercury	mg/kg	0.12	U	0.48		0.029	J	0.02	J	0.02	J	0.026	J	0.028	J	0.021	J
Selenium	mg/kg	2	В	3.1	U	3.9	U	3.5	U	4.3	U	5.2	U	3.8	U	5.4	U
Silver	mg/kg	2.4	U	2.3	U	3	U	2.6	U	3.2	U	3.9	U	2.9	U	4.1	U
Non-Validated Metals																	
Aluminum	mg/kg	39,100	Е	6,810		13,100		10,200		13,700		13,800		12,000		9,110	
Antimony	mg/kg	2.4	U	2.3	U	3	U	2.6	U	3.2	U	3.9	U	2.9	U	4.1	U
Beryllium	mg/kg	2.8		0.53	J	0.52	J	0.39	J	0.79	J	1.6		0.61	J	1.3	J
Cobalt	mg/kg	3.5	J	7.4		3.1	J	3.9	J	6.5		15.3		43		9.3	
Copper	mg/kg	179		89.4		15.2		14.2		23.8		20		30		19.4	
Iron	mg/kg	17,500	E	8,060		19,900	E	6,160		30,300	E	24,100		7,510		56,700	E
Manganese	mg/kg	7,310	E	191		61.1		50.2		170		156		68.1		379	
Nickel	mg/kg	13.7		10.7		10.9		11.1		18.8		29		31		18.1	
Thallium	mg/kg	8	U	7.7	U	9.8	U	8.7	U	10.7	U	12.9	U	9.5	U	13.5	U
Vanadium	mg/kg	NA		NA		NA		NA		NA		NA		NA		NA	
Zinc	mg/kg	14,700	E	952		1,000		284		2,960	Е	127		1,670		70.3	

Detections in bold

		RW-062-S	B-1	RW-062-S	B-3	RW-062-SB	B-10	RW-062-SE	B -15	RW-062-SE	8-20	RW-062-SB	8-22	RW-062-SE	B- 30	RW-062-SE	3-32
Parameter	Units	Soil		Soil		Soil		Soil		Soil		Soil		Soil		Soil	
		10/5/201	5	10/5/201	5	10/5/201:	5	10/5/201	5	10/5/201	5	10/5/201:	5	10/5/201	5	10/5/201	5
Validated Metals																	
Arsenic	mg/kg	15.1	J	4.3	J	8.6	J	5.9	J	2.2	J	3	U	4.2		3.5	
Barium	mg/kg	1,180		32.8		59.7		38		8.9		64.6		4.3	J	73.8	
Cadmium	mg/kg	10.7	J	1.4	U	1.4	U	3.7	J	3.3	J	0.22	В	1.9		16	
Chromium	mg/kg	165	J	14.9	J	23.8	J	17	J	7.9	J	35.3	J	9.2		50	
Lead	mg/kg	901	J	16.3	J	13.3	J	9.6	J	1.5	J	12	J	2.4	U	9.7	
Mercury	mg/kg	0.37		0.079	J	0.016	J	0.022	J	0.007	J	0.022	J	0.1	U	0.034	J
Selenium	mg/kg	4.4	U	3.7	U	3.7	U	3.4	U	3.1	U	4.8	U	3.8	U	4.2	U
Silver	mg/kg	1	В	2.8	U	2.8	U	2.5	U	2.3	U	3.6	U	2.9	U	3.2	U
Non-Validated Metals																	
Aluminum	mg/kg	12,400		9,110		14,100		9,760		2,330		12,800		611		12,600	
Antimony	mg/kg	3.3	U	2.8	U	2.8	U	1.3	J	2.3	U	3.6	U	2.9	U	3.2	U
Beryllium	mg/kg	1.1	J	0.3	J	0.52	J	0.46	J	0.25	J	2		0.96	U	2.2	
Cobalt	mg/kg	6.3		7.6		4.4	J	5.5		0.98	J	16.3		4.8	U	8.8	
Copper	mg/kg	304		7.3		11.5		11.5		3.9		19.5		4.8	U	19.3	
Iron	mg/kg	45,100	E	13,500		15,600		9,490		4,610		41,800	Е	4,450		16,200	
Manganese	mg/kg	2,320	E	148		35		61.2		27.2		578		6		89	
Nickel	mg/kg	41.5		6.7	J	10.8		14		2.6	J	35		9.6	U	20.4	
Thallium	mg/kg	11.1	U	9.3	U	9.3	U	8.4	U	7.7	U	12.1	U	9.6	U	10.6	U
Vanadium	mg/kg	NA		NA		NA		NA		NA		NA		NA		NA	
Zinc	mg/kg	1,520		625		35.7		359		491		874		66.5		855	

Detections in bold

		RW-063-S	B-1	RW-063-S	B-5	RW-063-SI	B-8	RW-063-SB	8-13	RW-063-SE	8-19	RW-063-SE	8-25	RW-063-SE	B- 30	RW-063-SH	B-34
Parameter	Units	Soil		Soil		Soil		Soil		Soil		Soil		Soil		Soil	
		10/6/201	5	10/6/201	5	10/6/201	5	10/6/201	5	10/6/201	5	10/6/201	5	10/6/201	5	10/6/201	5
Validated Metals																	
Arsenic	mg/kg	4.4		8.5		2.8	В	2.6	В	3.3	U	3.6		15.4		3.5	
Barium	mg/kg	71.2		129		30.4		38		31.1		64.6		82		18.4	
Cadmium	mg/kg	6.8		53.5	J	57.5	J	1.7	UJ	3.9	J	1.6	UJ	1.8	UJ	2	J
Chromium	mg/kg	19.6		55.8		7.6		16.5		14.7		36.8		38.7		20.3	
Lead	mg/kg	75.4	J	297	J	15.3	J	7.6	J	7.3	J	12.3	J	20.6	J	6.5	J
Mercury	mg/kg	0.39		0.25		1.5		0.0053	J	0.011	J	0.036	J	0.021	J	0.0089	J
Selenium	mg/kg	3.6	U	3.6	U	4.6	U	4.4	U	5.3	U	4.2	U	4.9	U	3.3	U
Silver	mg/kg	2.7	U	0.91	J	3.5	U	3.3	U	4	U	3.2	U	3.7	U	2.4	U
Non-Validated Metals																	
Aluminum	mg/kg	8,130		10,800		3,550		10,700		7,490		16,300		20,500		6,300	
Antimony	mg/kg	2.7	U	2.7	U	3.5	U	3.3	U	4	U	3.2	U	3.7	U	2.4	U
Beryllium	mg/kg	0.48	J	0.57	J	1.2	U	0.31	J	0.25	J	0.8	J	1.5		0.33	J
Cobalt	mg/kg	4.6		6.3		1.9	J	4.5	J	3.2	J	18.5		22.4		2.2	J
Copper	mg/kg	21.6		112		10.1		10.8		6.9		20.2		23		4	J
Iron	mg/kg	13,400		36,400	E	3,080		10,100		12,000		32,200	E	47,100	E	6,960	
Manganese	mg/kg	405		1,240		30.9		67.1		45.8		133		755		36.2	
Nickel	mg/kg	8.8	J	15.1		4.6	J	12.4		8.2	J	15.4		40.1		5.5	J
Thallium	mg/kg	8.9	U	9	U	11.6	U	11	U	13.2	U	10.6	U	12.3	U	8.2	U
Vanadium	mg/kg	34.4		172		7.8		18.5		16		56.9		38.2		27.2	
Zinc	mg/kg	748		4,390	E	2,820	Е	1,150		1,100		72.7		1,270		1,770	E

Detections in bold

		RW-064-S	B-1	RW-064-SI	3-5	RW-064-SI	3-8	RW-064-SB	-12	RW-064-SE	B- 16	RW-064-SE	B-2 1	RW-064-SH	8-29	RW-064-SI	B-32
Parameter	Units	Soil		Soil		Soil		Soil		Soil		Soil		Soil		Soil	
		10/6/201	5	10/6/201	5	10/6/201	5	10/6/2015	5	10/6/201	5	10/6/201	5	10/6/201	5	10/6/201	15
Validated Metals																	
Arsenic	mg/kg	9.6		17.9		5.7		53.6		2.7	U	16.6		3		17	
Barium	mg/kg	243		4,070		93.6		989		11		66.2		5	J	16.7	
Cadmium	mg/kg	2.5	J	1.7	J	15.1	J	3,130	J	157	J	32.8	J	1.1	J	3.8	
Chromium	mg/kg	332		576		637		49.8		10.1		36.7		4.9		13.1	
Lead	mg/kg	56.8	J	102	J	34.9	J	2,880	J	13.9	J	16.5	J	1.7	J	7.4	
Mercury	mg/kg	0.014	J	0.028	J	0.0095	J	0.11	J	0.0083	J	0.018	J	0.1	U	0.021	J
Selenium	mg/kg	3.8	U	3.2	U	2.7	U	12.7	U	4.3	U	2.1	J	3.1	U	3.2	U
Silver	mg/kg	2.9	U	2.4	U	2	U	58.4		3.2	U	0.41	J	2.3	U	2.4	U
Non-Validated Metals																	
Aluminum	mg/kg	11,100		13,400		4,620		15,600		1,490	M1	14,600		1,340		4,420	
Antimony	mg/kg	2.9	U	2.4	U	2	U	9.5	U	3.2	UM	2.6	U	2.3	U	2.4	U
Beryllium	mg/kg	0.4	J	0.37	J	0.31	J	0.62	J	0.21	J	2.1		0.77	U	0.33	J
Cobalt	mg/kg	6.9		9.8		6.3		14	J	3.9	J	25.7		0.53	J	2.6	J
Copper	mg/kg	80.9		197		45.3		1,350		16.8		22.7		3.9	U	9.9	
Iron	mg/kg	156,000	E	173,000	Е	138,000	Е	126,000	Е	3,020	M1	80,900	Е	1,480		7,430	
Manganese	mg/kg	27,400	E	18,600	Е	9,910	Е	12,900	Е	173	M1	1,070		20.8		70.3	
Nickel	mg/kg	60.8		69.3		33.6		79.3		3.6	J	31.2		1.3	J	4	J
Thallium	mg/kg	9.5	U	7.9	U	6.8	U	31.7	U	10.8	U	8.7	U	7.7	U	7.9	U
Vanadium	mg/kg	492		601		532		28.3		9.9		47.9		2.6	J	17	
Zinc	mg/kg	238		452		3,040	Е	117,000	Е	1,280	M1	7,030	Е	439		2,650	Е

Detections in bold

		RW-065-S	B-1	RW-065-SI	3-5	RW-065-SI	3-9	RW-065-SE	8-15	RW-065-SE	8-19	RW-065-SB	8-24	RW-065-SE	8-26	RW-065-S	B-35
Parameter	Units	Soil		Soil		Soil		Soil		Soil		Soil		Soil		Soil	
		9/18/201	5	9/18/201	5	10/8/201	5	10/8/201	5	10/8/201	5	10/8/201	5	10/8/201	5	10/8/202	15
Validated Metals																	
Arsenic	mg/kg	7.9		6.6		3.1		5.2		2.1		8.4		3.3		14.7	J
Barium	mg/kg	256		58.7		9.9		54.7		54.6		71.8		60.3		37.5	J
Cadmium	mg/kg	0.73	В	1.3	U	2.1		8.1		2		37.2		14.7		65.5	J
Chromium	mg/kg	197		10.5		7.3		24.9		29.3		38		34.3		20.7	
Lead	mg/kg	175		64.9		1.9	В	8.1		17		12.6		13		7.4	
Mercury	mg/kg	0.39		1.6		0.013	J	0.019	J	0.034	J	0.0073	J	0.031	J	0.12	UJ
Selenium	mg/kg	2.9	В	3.5	U	3.5	U	4	U	2.7	U	3.4	U	3.6	U	3.7	U
Silver	mg/kg	2.4	U	2.7	U	2.6	U	3	U	2	U	2.6	U	2.7	U	2.8	U
Non-Validated Metals																	
Aluminum	mg/kg	24,600	Е	5,720		3,250		12,000		14,400	Е	17,700	Е	14,900		9,150	M1
Antimony	mg/kg	2.4	U	2.7	U	2.6	U	3	U	2	U	2.6	U	2.7	U	2.8	UM
Beryllium	mg/kg	1.2		0.33	J	0.87	U	0.62	J	0.65	J	2.8		2.4		1.4	
Cobalt	mg/kg	4.7		2.9	J	1.4	J	4.3	J	4.4		37.3		18.6		18.9	
Copper	mg/kg	45.2		13.5		3.2	J	12.3		16.5		21.4		20.1		13	
Iron	mg/kg	27,200	Е	7,320		5,600		12,000		9,280		16,800		29,000	Е	11,900	M1
Manganese	mg/kg	5,150	E	159		53.6		60.5		66		160		298		100	
Nickel	mg/kg	19.8		5.7	J	2.9	J	10.1		11.6		81.4		41.2		36.2	M1
Thallium	mg/kg	7.9	U	8.8	U	8.7	U	9.9	U	6.7	U	8.6	U	8.9	U	9.4	U
Vanadium	mg/kg	878		14		40.1		31.1		36.9		49.5		45		27.5	
Zinc	mg/kg	194		34.9		430		1,580		1,140		6,270	E	4,230	E	3,980	M1

Detections in bold

		RW-066-S	B-1	RW-066-S	B-4	RW-066-SI	B-6	RW-066-SB	B- 11	RW-066-SE	B -20	RW-066-SE	B -22	RW-066-SE	B -27	RW-066-S	B-35
Parameter	Units	Soil		Soil		Soil		Soil		Soil		Soil		Soil		Soil	
		10/7/201	5	10/7/201	5	10/7/201	5	10/7/201	5	10/7/201	5	10/7/201	5	10/7/201	5	10/7/201	15
Validated Metals																	
Arsenic	mg/kg	2.3	U	4.4		1.6	В	5.1		5.9		4.6		11.7		4.1	
Barium	mg/kg	26.8	J	21.6	J	27.9	J	35.3	J	9.7	J	68.9	J	60.3	J	2.6	J
Cadmium	mg/kg	6.7		1.5	В	15.8		5.5		21.1		0.21	J	6.7		0.2	JB
Chromium	mg/kg	4.7		10.9		15.8		18.2		8		40.1		31.1		3.8	
Lead	mg/kg	5.5		5.3		20.2		13		2.7		15.6		20.2		2.3	U
Mercury	mg/kg	0.0081	J	0.013	J	0.011	J	0.009	J	0.0083	J	0.015	J	0.01	J	0.11	U
Selenium	mg/kg	3.7	U	3.2	U	3.1	U	4.5	U	2.8	U	4.5	U	3.7	U	3.7	U
Silver	mg/kg	2.8	U	2.4	U	2.3	U	3.4	U	2.1	U	3.4	U	2.8	U	2.8	U
Non-Validated Metals																	
Aluminum	mg/kg	3,530		8,200		9,750		11,500		2,720		15,800		15,600		646	
Antimony	mg/kg	2.8	U	2.4	U	2.3	U	3.4	U	2.1	U	3.4	U	2.8	U	2.8	U
Beryllium	mg/kg	0.2	J	0.38	J	0.32	J	0.46	J	0.23	J	1.4		1.4		0.94	U
Cobalt	mg/kg	3.3	J	2.2	J	2.1	J	4.3	J	24.9		18.7		22.4		4.7	U
Copper	mg/kg	5		5.7		9.6		15.5		3.4	J	22.1		21.6		2	J
Iron	mg/kg	3,680		12,200		8,140		9,870		2,220		24,000	E	46,800	E	1,470	
Manganese	mg/kg	71.7		42.7		42.9		52.6		26.9		338		657		21.7	
Nickel	mg/kg	4.3	J	6.3	J	4.3	J	10.2	J	34.2		36.1		37		9.4	U
Thallium	mg/kg	9.3	U	8	U	1.2	J	11.2	U	7.1	U	11.2	U	9.3	U	9.4	U
Vanadium	mg/kg	6.6		20.8		30.4		18.1		9.4		49.2		30.3		1.9	J
Zinc	mg/kg	511		378		679		427		406		4,210	Е	3,640	E	582	

Detections in bold

		RW-067-S	B-1	RW-067-SI	3-2	RW-067-SI	3-8	RW-067-SB	8-12	RW-067-SB	-19	RW-067-SB	-25	RW-067-SB	8-26	RW-067-SI	B-35
Parameter	Units	Soil		Soil		Soil		Soil		Soil		Soil		Soil		Soil	
		10/7/201	5	10/7/201	5	10/7/201	5	10/7/201	5	10/7/201	5	10/7/201	5	10/7/201	5	10/7/201	5
Validated Metals																	
Arsenic	mg/kg	5.2		8.7		2.3	J	4.1		7.2		9.3		5.6		3.3	
Barium	mg/kg	77	J	75	J	12	J	36.7	J	21.5	J	13.1	J	29.8	J	19.5	J
Cadmium	mg/kg	837		4.6		0.48	J	23		32.1		1.8		3.3		5.9	
Chromium	mg/kg	11.6		15.8		7.2		27.1		13.1		7.8		14.6		14.9	
Lead	mg/kg	107		137		3.6		12.4		3.9		3.7		3.3		5.3	
Mercury	mg/kg	0.0062	J	2.6		0.0028	J	0.018	J	0.0032	J	0.0083	J	0.0065	J	0.003	J
Selenium	mg/kg	3.7	U	4.4	U	4.1	U	4.1	U	3.1	U	2.7	U	5	U	2.8	U
Silver	mg/kg	4.3		3.3	U	3.1	U	3.1	U	2.3	U	2.1	U	3.7	U	2.1	U
Non-Validated Metals																	
Aluminum	mg/kg	7,150		5,750		4,220		14,300		4,310		2,860		4,520		6,550	
Antimony	mg/kg	1.7	J	3.3	U	3.1	U	3.1	U	2.3	U	2.1	U	3.7	U	2.1	U
Beryllium	mg/kg	0.35	J	0.33	J	0.19	J	0.66	J	0.41	J	0.25	J	0.22	J	0.23	J
Cobalt	mg/kg	3.1	J	3.7	J	0.82	J	4.4	J	8.2		11.3		1.1	J	2.4	J
Copper	mg/kg	227		35.3		3.1	J	7.4		5.5		4.7		4.8	J	5.8	
Iron	mg/kg	12,300		11,200		5,740		14,100		7,960		6,670		49,600	E	6,110	
Manganese	mg/kg	531		223		20.9		70.5		53.2		51.9		69.3		80.3	
Nickel	mg/kg	8.6	J	8.5	J	2.7	J	12		17.5		8.9		3.9	J	6.6	J
Thallium	mg/kg	9.2	U	10.9	U	10.2	U	10.2	U	7.7	U	6.8	U	12.4	U	7	U
Vanadium	mg/kg	21.3		13.7		12.1		28.8		12.4		8.5		21.4		23.6	
Zinc	mg/kg	51,000	Е	663		402		3,030	E	1,130		1,090		1,900		2,270	E

Detections in bold

		RW-068-S	B-1	RW-068-S	B-5	RW-068-SI	B-7	RW-068-SB	8-12	RW-068-SE	B -17	RW-068-SE	B-22	RW-068-SB	-26	RW-068-SE	3-32
Parameter	Units	Soil		Soil		Soil		Soil		Soil		Soil		Soil		Soil	
		10/7/201	5	10/7/201	5	10/7/201	5	10/7/201	5	10/7/201	5	10/7/201	5	10/7/201	5	10/7/201	5
Validated Metals																	
Arsenic	mg/kg	4.1		32.8		46.9		3.2		4.2		1.8	J	10.5		10.8	
Barium	mg/kg	83		168		403		28.2		38.4		56.4		74.1		87.4	
Cadmium	mg/kg	0.28	В	1,170		1,310		1.8		0.41	В	1.2	UB	2.2	U	0.26	В
Chromium	mg/kg	16.2		294		146		61.6		10.6		30.4		34.5		40	
Lead	mg/kg	69.8		597		448		12.1		5.8		12.2		18.5		21.4	
Mercury	mg/kg	0.14		0.34		0.49		0.1	J	0.21	U	0.017	J	0.017	J	0.0072	J
Selenium	mg/kg	3.3	U	5.5	U	5.2	U	4.7	U	6.6	U	3.1	U	6	U	5.6	U
Silver	mg/kg	2.5	U	6.5		3.9	U	3.6	U	4.9	U	2.3	U	0.49	В	4.2	U
Non-Validated Metals																	
Aluminum	mg/kg	10,500		8,870		8,680		3,640		7,200		10,500		18,700		21,800	
Antimony	mg/kg	2.5	U	4.2	U	3.9	U	3.6	U	4.9	U	2.3	U	4.5	U	4.2	U
Beryllium	mg/kg	0.7	J	0.79	J	0.99	J	0.25	J	0.77	J	0.91		1.4	J	1.6	
Cobalt	mg/kg	5.1		5.8	J	18		3.1	J	10.2		6.1		17.3		21.5	
Copper	mg/kg	19.6		329		265		12.9		7.8	J	9.8		22.5		26.4	
Iron	mg/kg	14,100		29,100	E	78,200	Е	12,200		13,500		9,380		57,800	E	51,100	E
Manganese	mg/kg	460		838		1,310		1,240		84.2		84.2		1,660		1,050	
Nickel	mg/kg	11.5		15.3		678		8.8	J	11.9	J	17.2		36.4		44.2	
Thallium	mg/kg	8.2	U	13.8	U	13.1	U	11.8	U	16.4	U	7.7	U	14.9	U	14	U
Vanadium	mg/kg	24		63.9		142		102		12.7		35.5		35.2		39.7	
Zinc	mg/kg	117		14,800	E	63,800	Е	1,260		7,650	E	1,840	E	105		285	

Detections in bold

		RW-069-S	B-1	RW-069-S	B-3	RW-069-SH	B-10	RW-069-SE	B -12	RW-069-SE	B -20	RW-069-SE	B -23	RW-069-SH	B -28	RW-069-SI	B-35
Parameter	Units	Soil		Soil		Soil		Soil		Soil		Soil		Soil		Soil	
		10/7/201	5	10/7/201	5	10/7/201	5	10/7/201	5	10/7/201	5	10/7/201	5	10/7/201	5	10/7/201	15
Validated Metals																	
Arsenic	mg/kg	199		6.9		3.1	D6	3	U	1.6	J	2.2		10.2		11.9	
Barium	mg/kg	560	J	66.4	J	18.3		64		17.2		61.7		68.5		30.8	
Cadmium	mg/kg	93.9		3,530		1.5		0.25	J	8.2		0.66	JB	0.37	В	0.29	В
Chromium	mg/kg	52.3		12.5		10		25.6		8.8		36.5		33.1		19.3	
Lead	mg/kg	353		400		4.5	D6	13.6		2.9		14.4		17.5		9.9	
Mercury	mg/kg	0.31		0.028	J	0.02	J	0.025	J	0.004	J	0.018	J	0.14	U	0.11	U
Selenium	mg/kg	3.4	U	4.2	U	3.9	U	4.8	U	2.9	U	3	U	4.2	U	4.7	U
Silver	mg/kg	2.6	U	18.5		2.9	U	3.6	U	2.2	U	2.2	U	0.95	В	3.5	U
Non-Validated Metals																	
Aluminum	mg/kg	19,000	Е	2,410		6,880		13,100		3,240		13,700		17,500		9,500	
Antimony	mg/kg	2.6	U	6.3		2.9	U	3.6	U	2.2	U	2.2	U	3.2	U	3.5	U
Beryllium	mg/kg	2		1.1	U	0.38	J	0.52	J	0.5	J	1.4		1.7		0.96	J
Cobalt	mg/kg	7.3		5.4		1.5	J	4.7	J	3.3	J	17.2		18.2		23.5	
Copper	mg/kg	73		672		4.8	J	11		5		20.2		20.8		11.5	
Iron	mg/kg	26,100	E	28,100	E	8,950		9,640		1,740		20,500	Е	65,400	E	18,200	
Manganese	mg/kg	4,290	E	1,420		26.1		58.1		22.5		216		1,560		312	
Nickel	mg/kg	15.5		16.4		4.6	J	13.7		6.2	J	30.7		36.9		41	
Thallium	mg/kg	8.5	U	10.6	U	9.8	U	12	U	7.2	U	7.4	U	10.6	U	11.7	U
Vanadium	mg/kg	142		9		15.9		26.1		11.9		47.2		33.7		20.3	
Zinc	mg/kg	5,010	E	99,700	E	891		953		745		4,360	E	3,650	E	3,310	E

Detections in bold

		RW-070-SI	B-1	RW-070-SI	3-3	RW-070-SI	B-7	RW-070-SB	-15	RW-070-SE	8-20	RW-070-SB	B -22	RW-070-SE	B -27	RW-070-SH	3-32
Parameter	Units	Soil		Soil		Soil		Soil									
		10/8/201	5	10/8/201	5	10/8/201	5	10/8/201	5	10/8/201	5	10/8/201	5	10/8/201	5	10/8/201	5
Validated Metals																	
Arsenic	mg/kg	14.3		184		12.2		2.6	U	2.7	U	22.8		8.6		8.9	
Barium	mg/kg	219		107		74.3		74		5.6	J	72.5		70.6		76.3	
Cadmium	mg/kg	16.4		11.8		80.5		1.5	U	1.6	U	0.2	В	0.36	В	0.42	В
Chromium	mg/kg	272		121		36		18.3		7.4		40.3		33.7		34.7	
Lead	mg/kg	97		481		86.7		7.9		2.7	U	17.7		16.1		17.5	
Mercury	mg/kg	0.08	J	0.26		0.13		0.0064	J	0.0092	J	0.028	J	0.011	J	0.013	J
Selenium	mg/kg	3.7	U	7		4.1	U	4.1	U	4.3	U	3.8	U	4.9	U	4.9	U
Silver	mg/kg	1.8	В	8		3.1	U	3.1	U	3.2	U	2.8	U	3.7	U	0.41	В
Non-Validated Metals																	
Aluminum	mg/kg	15,000		13,200		11,800		11,700		1,430		16,800		17,900		18,700	
Antimony	mg/kg	2.8	U	2.4	U	3.1	U	3.1	U	3.2	U	2.8	U	3.7	U	3.7	U
Beryllium	mg/kg	1		0.8	J	0.61	J	0.76	J	0.35	J	1.6		1.3		1.4	
Cobalt	mg/kg	7.2		37.9		3.7	J	3.7	J	5.4	U	17.9		17.4		17.5	
Copper	mg/kg	59		233		48.4		9.2		3.3	J	24.3		22.1		22.6	
Iron	mg/kg	94,700	E	201,000	Е	20,600	Е	7,120		10,200		24,000	Е	47,300	E	51,300	Е
Manganese	mg/kg	17,200	E	5,040	Е	355		40.8		15.3		210		897		1,280	
Nickel	mg/kg	23.6		29.4		10.1	J	10.3		1.3	J	32.6		35.8		36.3	
Thallium	mg/kg	9.2	U	3.3	J	10.3	U	10.2	U	10.8	U	9.4	U	12.3	U	12.2	U
Vanadium	mg/kg	352		219		78.8		20.1		3.2	J	48.5		33.5		34.1	
Zinc	mg/kg	1,650		1,270		2,220	Е	812		205		3,280	Е	127		125	

Detections in bold

 TABLE 6

 SOIL CLASSIFICATION AND GEOTECHNICAL DATA

Date Collected	ARM/EAG Sample ID	PACE/Geotechnics Sample ID	TOC (mg/kg)	Qual.	Percent Moisture		USCS Symbol	USCS Classification	% greater than #4 sieve	% between #4 and #200 sieve		Avg. Specific Gravity @ 20C	Avg. Permeability (cm/sec) @ 20C	Unit Wet Wt. (g/cm3)	Unit Dry Wt. (g/cm3)	Porosity
	RW-057-SB-1	30160869001			Wioisture	Solids		silty gravel with sand	47.37	39.82	12.81	Gravity (a) 200	(()) 200	(g/enic)	(g/enic)	
	RW-057-SB-3	30160869002					gm	silty gravel with sand	42.03	35.61	22.36					
	RW-057-SB-6	30160869003					0	silty sand	0.27	75.92	23.81					
	RW-057-SB-15	30160869004					cl	sandy lean clay	0.00	31.42	68.57					
10/1/2015	RW-057-SB-16	30160869005					cl	sandy lean clay	0.00	37.73	62.27					
10/1/2015	RW-057-SB-23	30160869006					cl	lean clay	0.00	5.61	94.39					
	RW-057-SB-29	30160869007					sp	poorly graded sand	1.17	97.11	1.72					
	RW-057-SB-32	30160869008					sm	silty sand	0.43	50.35	49.21					
	RW-058-SB-1	30161133025					sw-sm	well-graded sand with silt and gravel	29.17	61.72	9.11					
	RW-058-SB-2	30161133026					sc	clayey sand	0.12	68.66	31.22					
	RW-058-SB-8	30161133027					cl	sandy lean clay	0.02	44.96	55.02					
	RW-058-SB-15	30161133030						clayey sand	0.38	74.65	24.97					
	RW-058-SB-20	30161133031					cl	sandy lean clay	0.00	41.39	58.61					
	RW-058-SB-22	30161133032						clayey sand	1.91	80.74	17.35					<u> </u>
	RW-058-SB-28	30161133033					cl	lean clay with sand	0.06	18.49	81.45					
	RW-058-SB-32	30161133034					cl	lean clay with sand	1.66	26.36	71.97					
	RW-059-SB-1	30160869009						poorly graded gravel with silt and sand	47.80	42.86	9.33					
	RW-059-SB-3	30160869010						sandy lean clay	2.00	42.53 63.57	55.46 36.43					
	RW-059-SB-6	30160869011						silty sand	0.00							
	RW-059-SB-11 RW-059-SB-20	30160869012 30160869013					sm	silty sand silty sand	0.00 2.56	73.03 79.67	26.97 17.76					
	RW-059-SB-20 RW-059-SB-23	30160869013					sm ml	silt	0.00	5.78	94.22					
	RW-059-SB-26	30160869014					cl	lean clay	0.25	12.88	86.86					
	RW-059-SB-20 RW-059-SB-34	30160869015					sm	silty sand	0.23	50.39	48.70					
	RW-060-SB-1	30161133003						clayey sand	3.77	59.89	36.34					
	RW-060-SB-4	30161133003					cl	sandy lean clay	0.00	44.71	55.29					
	RW-060-SB-7	30161133005					cl	lean clay	0.15	6.07	93.78					
	RW-060-SB-12	30161133006					cl	lean clay	0.00	9.09	90.91					
	RW-060-SB-20	30161133007					cl	sandy lean clay	0.35	48.06	51.60					
	RW-060-SB-20 RW-060-SB-22	30161133008					cl	lean clay	0.07	8.99	90.94					
	RW-060-SB-26	30161133009					sc	clayey sand	2.23	61.46	36.31					
	RW-060-SB-33	30161133010						clayey sand	0.70	66.33	32.97					
	RW-061-SB-1	30161133035						well-graded sand with silt and gravel	25.42	62.99	11.59					
	RW-061-SB-2	30161133011						clayey sand	10.89	60.35	28.76					
	RW-061-SB-7	30161133012					cl	lean clay with sand	0.28	18.88	80.84					
	RW-061-SB-11	30161133013					cl	lean clay	0.00	8.01	91.99					
	RW-061-SB-19	30161133014					cl	lean clay	0.00	7.45	92.55					
10/5/2015	RW-061-SB-21	30161133015					cl	sandy lean clay	0.00	44.34	55.66					
	RW-061-SB-29	30161133017						clayey sand	1.51	61.52	36.97					
10/5/2015	RW-061-SB-34	30161133018					cl	lean clay with sand	0.06	19.72	80.22					
10/5/2015	RW-062-SB-1	30161133019					SW	well-graded sand with gravel	46.96	50.56	2.48					
10/5/2015	RW-062-SB-3	30161133020					sc	clayey sand	2.13	54.68	43.19					
10/5/2015	RW-062-SB-10	30161133021					cl	lean clay	0.17	10.65	89.18					
10/5/2015	RW-062-SB-15	30161133022					cl	sandy lean clay	0.06	41.75	58.19					
	RW-062-SB-20	30161133023					sc	clayey sand	1.43	53.53	45.05					
	RW-062-SB-22	30161133024						lean clay	0.00	10.81	89.19					
	RW-062-SB-30	30161133001					sw-sm	well-graded sand with silt	6.61	84.31	9.08					
	RW-062-SB-32	30161133002					cl	lean clay	0.03	4.29	95.68					
	RW-063-SB-1	30161228009	12000		1.8	98		clayey sand	12.95	42.03	45.02					
	RW-063-SB-5	30161228010	15000		3.6	96		clayey sand	11.48	47.27	41.25					
	RW-063-SB-8	30161228011	8800		5.9	94		silty sand	0.29	62.67	37.03					
	RW-063-SB-13	30161228012	270	$ \downarrow \downarrow$	2.2	98	ml	silt with sand	0.03	21.93	78.04					
	RW-063-SB-19	30161228013	340	$ \downarrow \downarrow$	3.2	97		silty sand	1.17	76.17	22.66					
	RW-063-SB-25	30161228014	3800	$ \downarrow \downarrow$	2.5	97	ml	sandy silt	0.42	38.42	61.16					
	RW-063-SB-30	30161228015	30000	$ \downarrow \downarrow$	8.3	92	cl	lean clay	0.00	3.20	96.80					
10/6/2015	RW-063-SB-34	30161228016	270		3.4	97	cl	sandy lean clay	1.77	33.33	64.90					

 TABLE 6

 SOIL CLASSIFICATION AND GEOTECHNICAL DATA

Date	ARM/EAG Sample ID	PACE/Geotechnics	TOC (mg/kg)	Qual.	Percent			USCS Classification	% greater than	% between #4		U .				Porosity
Collected		Sample ID	× 8 8,	-	Moisture		Symbol		#4 sieve	and #200 sieve		Gravity @ 20C	(cm/sec) @ 20C	(g/cm3)	(g/cm3)	· · ·
	RW-064-SB-1 RW-064-SB-5	30161228018 30161228019	15000 9200		2.2	98 96		clayey sand with gravel well-graded sand with clay and gravel	25.13 40.55	38.50 50.47	36.37 8.98					
	RW-064-SB-5	30161228020	3500		2.9	97		well-graded sand with citay and gravel well-graded sand with silt and gravel	40.33	48.97	8.33					
	RW-064-SB-12	30161228021	23000		32	68	ml	sandy silt	4.26	38.44	57.30					
10/6/2015	RW-064-SB-16	30161228022	1200		4.4	96	sm	silty sand	0.93	72.72	26.35					
10/6/2015	RW-064-SB-21	30161228023	11000		5.6	94	cl	lean clay	0.00	7.59	92.41					
	RW-064-SB-29	30161228024	250	U	1.6	98	sp	poorly graded sand	1.65	95.37	2.98					
	RW-064-SB-32	30161228025	260	U	3	97		sandy silt	0.00	37.84	62.16					
	RW-065-SB-1	30161487009	7500		6.2	94		well-graded gravel with clay and sand	45.17	44.06	10.77					\square
	RW-065-SB-5	30161487010	390	J	0.92	99		clayey sand	0.01	67.21	32.78					
	RW-065-SB-9 RW-065-SB-15	30161487011 30161487013	580 710	J J	0.25	100 99		silty sand lean clay with sand	0.02	85.82 24.52	14.16 75.48					
	RW-065-SB-15 RW-065-SB-19	30161487013	3000	J	0.94	99 99		sandy lean clay	0.00	33.13	66.87					+
	RW-065-SB-24	30161487015	7700		2.6	99 97	cl	lean clay	0.00	7.82	92.18					
	RW-065-SB-26	30161487016	12000		2.0	97	cl	lean clay	0.00	7.11	92.89					
	RW-065-SB-35	30161487017	32000		3.7	96	cl	sandy lean clay	0.00	30.07	69.93					
	RW-066-SB-1	30161351010	7800		3.3	97	sm	silty sand	2.14	66.62	31.24					
	RW-066-SB-4	30161351012	340		2.1	98	cl	sandy lean clay	0.00	39.92	60.08					
	RW-066-SB-6	30161351011	2600		2.1	98	cl	sandy lean clay	0.75	35.13	64.12					
	RW-066-SB-11	30161351014	1300		2.3	98	cl	lean clay	0.00	6.24	93.76					
	RW-066-SB-20	30161351015	3500		2	98	sm	silty sand	2.16	79.35	18.49					4
	RW-066-SB-22	30161351013	6800		3.4	97	cl	lean clay	0.00	6.79	93.21					4
	RW-066-SB-27 RW-066-SB-35	30161351016	28000		4.7	95	cl	lean clay silty sand	0.00 2.08	5.38 85.36	94.62 12.55					
	RW-060-SB-35 RW-067-SB-1	30161351017 30161351002	1100 12000		5 6.8	97 93	sm sm	silty sand with gravel	2.08	47.33	25.95					+
	RW-067-SB-2	30161351002	15000		1.9	98		clayey sand	1.14	53.90	44.96					
	RW-067-SB-8	30161351004	280		3	97		silty sand	0.00	83.70	16.30					
	RW-067-SB-12	30161351005	1200		2.4	98	cl	lean clay	0.06	10.85	89.09					
10/7/2015	RW-067-SB-19	30161351006	9500		3.6	96	cl	lean clay with sand	0.08	24.29	75.64					
	RW-067-SB-25	30161351007	12000		2.6	97	cl	sandy lean clay	1.59	34.80	63.61					
	RW-067-SB-26	30161351008	22000		4.7	95	cl	lean clay with sand	2.19	15.50	82.31					
	RW-067-SB-35	30161351009	260	U	3.1	97	cl	lean clay with sand	0.00	24.47	75.53					
	RW-068-SB-1	30161351025	11000		2.1	98		clayey sand with gravel	34.42	49.29	16.30					4
	RW-068-SB-5 RW-068-SB-7	30161351026	16000		1.3	99		clayey sand	10.79 5.49	45.90	43.32 50.52					
	RW-068-SB-7 RW-068-SB-12	30161351027 30161351028	24000 5300		2.1 0.68	98 99		sandy lean clay clayey sand	0.10	43.99 50.26	49.64					+
	RW-068-SB-17	30161351028	130000		6.8	93		silty sand	0.95	57.26	49.04					
	RW-068-SB-22	30161351030	1700		2	98		lean clay	0.14	13.79	86.08					
	RW-068-SB-26	30161351031	26000		2.2	98	cl	lean clay	0.05	5.94	94.01					
	RW-068-SB-32	30161351032	30000		2.5	98	cl	lean clay	0.00	2.44	97.56					
	RW-069-SB-1	30161351018	14000		2.5	98	sm	silty sand with gravel	17.66	59.75	22.58					
	RW-069-SB-3	30161351019	11000		2.2	98		silty sand	3.73	73.34	22.93					
	RW-069-SB-10	30161351020	250	U	1.4	99		sandy lean clay	0.00	38.28	61.72					
	RW-069-SB-12	30161351021	810		1.4	99	cl	lean clay	0.00	12.81	87.19					
	RW-069-SB-20 RW-069-SB-23	30161351022 30161351023	2900 6500		0.82 2.5	99 98	sm cl	silty sand lean clay	3.53 0.00	82.38 5.73	14.09 94.27					
	RW-069-SB-23 RW-069-SB-28	30161351023	31000		3.2	98 97	cl cl	lean clay	0.00	3.85	94.27 96.15					
	RW-069-SB-28 RW-069-SB-35	30161351024	6800		1.1	97 99		silty sand	0.32	62.58	37.09					
	RW-009-5B-55 RW-070-SB-1	30161487001	12000		9	91		clayey sand with gravel	24.71	50.63	24.66					
	RW-070-SB-3	30161487002	3400		2.3	98		clayey sand	11.09	54.73	34.18					
	RW-070-SB-7	30161487003	25000		4.6	95		clayey sand	0.82	57.60	41.58					
	RW-070-SB-15	30161487004	1500		1.6	98	cl	sandy lean clay	0.00	39.60	60.40					
	RW-070-SB-20	30161487005	270	J	0.41	100	1	poorly graded sand with silt	1.71	89.21	9.08					
	RW-070-SB-22	30161487006	8500		2.2	98		lean clay	0.00	4.57	95.43					
	RW-070-SB-27	30161487007	4700		1.3	99		clayey sand	4.33	59.34	36.33					
10/8/2015	RW-070-SB-32	30161487008	20000		2.7	97	cl	lean clay	0.05	3.40	96.55					

 TABLE 6

 SOIL CLASSIFICATION AND GEOTECHNICAL DATA

Date Collected	ARM/EAG Sample ID	PACE/Geotechnics Sample ID	TOC (mg/kg)	Qual.	Percent Moisture	Percent Solids	USCS Symbol	USCS Classification	% greater than #4 sieve	% between #4 and #200 sieve		Avg. Specific Gravity @ 20C		Unit Wet Wt. (g/cm3)	Unit Dry Wt. (g/cm3)	Porosity
	RW-01-GB-SS-1 (1-3)	30163058022	4600		1.4	99	Symbol				n200 sieve			(g/ child)	(g/enie)	
	RW-01-GB-SS-2 (5-7)	30163058023	4700		7.6	92										
10/21/2015	RW-01-GB-SS-3 (10-12)	30163058024	1000	J	12	88										
10/21/2015	RW-01-GB-SS-4 (16-18)	30163058001	930	J	17	83										
	RW-01-GB-SS-6 (20.5-22.5)	30163058002	1200		19	81										
10/22/2015	RW-01-GB-SS-7 (25-27)	30163058003	1400		14	86										
10/22/2015	RW-01-GB-SS-8 (29.5-31.5)	30163058004	1200		29	71										
10/22/2015	RW-01-GB-SS-9 (34.5-36.5)	30163058005	18000		33	67										
10/22/2015	RW-01-GB-SS-10 (39.5-41.5)	30163058006	41000		48	52										
10/22/2015	RW-01-GB-SS-11 (44.5-46.5)	30163058007	19000		38	62										
10/21/2015	RW-01-GB-ST-1 (0-1.1)	30163058013					gw	well-graded gravel with sand	19.74	76.57	3.69	2.22	8.10E-04	1.60	1.42	0.36
10/21/2015	RW-01-GB-ST-2 (12-13.2)	30163058014					cl	lean clay with sand	0.33	21.83	77.84	2.69	1.80E-07	2.09	1.73	0.36
10/21/2015	RW-01-GB-ST-3 (15-16)	30163058015					cl	lean clay	1.15	8.17	90.68	2.67	1.30E-07	2.07	1.73	0.35
10/22/2015	RW-01-GB-ST-4 (22.5-25)	30163058016					sc	clayey sand	0.34	55.99	43.67	2.67	2.60E-04	2.03	1.69	0.37
10/22/2015	RW-01-GB-ST-5 (27-29.5)	30163058017					cl	lean clay	0.23	4.22	95.55	2.73	1.60E-07	1.76	1.18	0.56
10/22/2015	RW-01-GB-ST-6 (32-34.5)	30163058018					cl	lean clay with sand	0.19	16.12	83.69	2.58	6.00E-07	1.80	1.30	0.50
	RW-01-GB-ST-7 (37-39.5)	30163058019					cl	lean clay	0.30	8.20	91.50	2.39	2.50E-07	1.43	0.72	0.70
10/22/2015	RW-01-GB-ST-8 (42-44.5)	30163058020					cl	lean clay	0.00	7.04	92.96	2.47	1.70E-06	1.49	0.81	0.67
10/22/2015	RW-01-GB-ST-9 (47-49.5)	30163058021					cl	lean clay	0.00	2.52	97.48	2.6	4.00E-07	1.60	0.96	0.63
10/23/2015	RW-02-GB-SS-2 (3-5)	30163058008	24000		19	81										
10/23/2015	RW-02-GB-SS-4 (8-10)	30163058025	310	J	12	88										
10/23/2015	RW-02-GB-SS-5 (12.5-14.5)	30163058009	970	J	16	84										
10/23/2015	RW-02-GB-SS-6 (17.5-19.5)	30163058010	5200		13	87										
10/23/2015	RW-02-GB-SS-7 (22.5-24.5)	30163058027	15000		23	77										
	RW-02-GB-SS-8 (26-28)	30163058028	1100	U	13	87										
	RW-02-GB-SS-9 (30'-32')	30163718001	1800		22	78										
	RW-02-GB-SS-10 (37.5'-39.5')	30163718002	51000		46	54										
10/26/2015	RW-02-GB-SS-11 (42.5-44.5')	30163718003	38000		48	52										
	RW-02-GB-SS-12 (48'-50')	30163718004	19000		36	64										
	RW-02-GB-ST-1 (10-12.5)	30163058011					cl	lean clay	0.00	5.30	94.70	2.68	3.90E-08	2.06	1.71	0.36
	RW-02-GB-ST-2 (15-17.5)	30163058012					cl	lean clay with sand	0.18	25.09	74.73	2.64	2.20E-07	2.02	1.72	0.35
	RW-02-GB-ST-3 (20-22.5)	30163058026					cl	lean clay	0.00	5.19	94.81	2.67	5.50E-08	1.94	1.47	0.45
	RW-02-GB-ST-4 (35'-37.5')	30163718005					cl	lean clay	0.00	2.67	97.33	2.54	6.30E-07	1.48	0.80	0.68
10/26/2015	RW-02-GB-ST-5 (40'-42.5')	30163718006					cl	lean clay	0.11	8.91	90.98	2.39	6.00E-07	1.39	0.69	0.71
10/26/2015	RW-02-GB-ST-6 (45'-47.5')	30163718007					cl	lean clay	0.03	2.91	97.05	2.56	3.50E-07	1.60	1.00	0.61

 TABLE 6

 SOIL CLASSIFICATION AND GEOTECHNICAL DATA

Date	ARM/EAG Sample ID	PACE/Geotechnics	TOC (mg/kg)	Oual	Percent		USCS	USCS Classification	% greater than			Avg. Specific			•	Porosity
Collected	-	Sample ID	(8 8/	Zuun	Moisture	Solids	Symbol		#4 sieve	and #200 sieve	#200 sieve	Gravity @ 20C	(cm/sec) @ 20C	(g/cm3)	(g/cm3)	rorosity
	RW-03-GB-SS-1 (1-3')	30163718028	11000		13	87										
	RW-03-GB-SS-2 (5-7')	30163718029	1800		14	86										
	RW-03-GB-SS-3 (10-12')	30163718030	1700		16	84										
	RW-03-GB-SS-4 (16-18')	30163718031	900	J	17	83										
	RW-03-GB-SS-5 (22.5-24.5')	30163718032	7700		25	75										
	RW-03-GB-SS-6 (27-29)	30163718033	540	J	11	89			11.0.6	0.0.40	Z 0.1					
	RW-03-GB-SS-6 (27-29)	30163718048						8	11.06	83.63	5.31					
	RW-03-GB-SS-7 (30-32)	30163718049					sp	poorly graded sand with gravel	11.37	85.74	2.89					
	RW-03-GB-SS-8 (35-36)	30163718050	0.00	-			sp	poorly graded sand with gravel	26.56	71.58	1.86					
	RW-03-GB-SS-8 (35-37)	30163718035	830	J	8.9	91										
	RW-03-GB-SS-10 (40-42)	30163718036	730	J	13	87		1. 1	0.00	<0.05	20.05					
	RW-03-GB-SS-11 (44-45)	30163718051	1.400		14	0.6	sm	silty sand	0.00	60.95	39.05					
	RW-03-GB-SS-12 (45-47)	30163718037	1400		14	86	1	1 11.	0.00	22.01	66.00					
	RW-03-GB-SS-13 (48-50)	30163718052	1.600		10	00	ml	sandy silt	0.00	33.91	66.09					
	RW-03-GB-SS-14 (52.5-54.5)	30163718038	1600		12	88										
	RW-03-GB-SS-15 (57.5-59.5)	30163718039	1800		13	87										
	RW-03-GB-SS-16 (62.5-64.5)	30163718040	17000		32	68	1	1 11	0.71	25.71	(2.50					
	RW-03-GB-SS-16 (62.5-64.5)	30163718053	15000		25	75	ml	sandy silt	0.71	35.71	63.58					
	RW-03-GB-SS-17 (67.5-69.5)	30163718041	15000		25	75		1	0.00	0.07	00.12	2.62	2 205 07	2.00	1 77	0.22
	RW-03-GB-ST-1 (12-14.5) RW-03-GB-ST-2 (15-16)	30163718042					cl	lean clay	0.00	9.87 92.02	90.13 7.93	2.63 2.58	3.30E-07	2.08 1.92	1.77	0.33
		30163718043 30163718044					sp-sm	poorly graded sand with silt	0.05	4.02	7.93 95.98		2.60E-04	1.92	1.58	0.39
	RW-03-GB-ST-3 (20-22.5) RW-03-GB-ST-5 (50-52.5)	30163718044					cl	lean clay	0.00	<u>4.02</u> 50.34	95.98 49.66	2.62 2.63	1.60E-07	2.12	1.39 1.84	0.47 0.30
	× /						sc	clayey sand				2.63	4.00E-07			
	RW-03-GB-ST-6 (55-57.5) RW-03-GB-ST-7 (65-67.5)	30163718046 30163718047					sc cl	clayey sand	<u>1.70</u> 1.77	67.88 46.49	30.42 51.74	2.62	4.90E-06 2.10E-07	2.17 1.83	1.89 1.35	0.28 0.49
	RW-03-GB-SS-1 (1'-3')	30163718008	10000		11	89	CI	sandy lean clay	1.//	40.49	51.74	2.04	2.10E-07	1.65	1.55	0.49
	RW-04-GB-SS-1 (1-3) RW-04-GB-SS-2 (5'-7')	30163718008	1400		11	89										
	RW-04-GB-SS-2 (3-7) RW-04-GB-SS-3 (8'-10')	30163718009	1400		13	87										
	RW-04-GB-SS-4 (12.5'-14.5')	30163718010	4800		20	80										
	RW-04-GB-SS-5 (16.5'-18.5')	30163718012	2700		18	82										
	RW-04-GB-SS-6 (22.8'-24.5')	30163718012	11000		27	73										
	RW-04-GB-SS-7 (26.5'-28.5')	30163718014	11000		9.4	91										
	RW-04-GB-SS-8 (32.5'-34.5')	30163718014	1100). 4 11	89										
	RW-04-GB-SS-9 (36.1-38.1)	30163718016	940	J	11	89										
	RW-04-GB-SS-10 (41.5-43.5)	30163718017	2400		17	83										
	RW-04-GB-SS-11 (46.8-48.8)	30163718018	5600		17	88										
	RW-04-GB-ST-1 (10-12.5)	30163718019	2 3 6 6				cl	lean clay	0.08	5.10	94.83	2.65	3.00E-08	2.03	1.66	0.38
	RW-04-GB-ST-2 (15-16.5)	30163718020						poorly graded sand with silt	0.25	89.46	10.29	2.6	6.70E-04	1.95	1.57	0.40
	RW-04-GB-ST-3 (20-22.5)	30163718021						clayey sand	0.11	58.50	41.40	2.62	1.30E-07	1.89	1.37	0.48
	RW-04-GB-ST-4 (25-26.5)	30163718022						silt with sand	6.58	16.25	77.17	2.57	1.20E-07	1.84	1.31	0.49
	RW-04-GB-ST-5 (30-31.3)	30163718023					sc	clayey sand	1.48	68.73	29.78	2.64	3.10E-05	1.93	1.54	0.42
	RW-04-GB-ST-6 (35-36.1)	30163718024					sc	clayey sand	0.46	69.09	30.46	2.6	1.10E-06	2.16	1.85	0.29
	RW-04-GB-ST-7 (40-41.5)	30163718025					sc	clayey sand	0.00	60.99	39.01	2.6	9.20E-06	2.07	1.77	0.32
	RW-04-GB-ST-8 (45-46.8)	30163718026					cl	sandy lean clay	0.00	40.65	59.35	2.61	1.00E-05	2.06	1.65	0.37
	RW-04-GB-ST-9 (50-52.5)	30163718027					cl	lean clay	0.00	2.89	97.11	2.6	8.50E-08	1.75	1.19	0.54

= Parameter not requested for this sample ID.

Table 7Summary of Parameters Detected in GroundwaterParcel A3Tradepoint AtlanticSparrows Point, Maryland

	I	RW-057-	PZ	RW-063-	PZ	RW-067-	PZ	RW-070-	·PZ	RW02-PZN	A020	RW07-PZN	4017	RW10-PZN	A020	RW19-PZN	M020	RW20-PZN	M 020
Parameter	Units	Groundwa		Groundwa		Groundwa		Groundw		Groundwa		Groundwa	ater	Groundwa		Groundw	ater	Groundwa	ater
		11/9/201	15	11/9/201	5	11/9/201	15	11/9/20		11/13/20	15	11/13/20	15	11/12/20	15	11/12/20	15	11/17/20	15
Total Metals		•		•				•		•		•		•		•			
Aluminum	μg/L	230		22.8	J	50	U	50	U	32.5	В	38.1	В	206		35.5	В	24.1	В
Antimony	μg/L	17.9		8.6		16.3		6	U	11		7.3		7.9		6	U	6	U
Arsenic	μg/L	12		60.2		4.5	В	5	U	6.9		5	U	3.3	J	5	U	3.7	J
Barium	μg/L	13		13.7		16.3		16.6		8.1	В	9.9	В	13.7		34.3		28.7	
Beryllium	μg/L	0.42	В	1	U	1	U	0.45	В	0.39	В	1	U	1	U	1	U	1	U
Cadmium	μg/L	44,500		434		311		0.91	J	47.2		9,780		10,200		41.9		0.59	J
Chromium	μg/L	5	U	5	U	5	U	5	U	5	U	5	U	5	U	0.89	J	5	U
Cobalt	μg/L	238		76.3		142		13		113		144		114		38.5		53.1	
Copper	μg/L	5	U	2.5	В	5	U	5	U	5	U	1.5	J	7.8		12		6	
Iron	μg/L	134,000	J	159,000	J	400,000	J	713,000	J	443,000		283,000		202,000		37,000		226,000	
Lead	μg/L	5	U	5	U	5	U	5	U	5	U	5	U	5	U	25	U	5	U
Manganese	μg/L	16,400		26,600		28,200		33,300		19,000		17,500		18,000		2,580		9,210	
Mercury	μg/L	0.2	U	0.2	U	0.2	U	0.2	U	0.2	U	0.2	U	0.2	U	0.2	U	0.2	U
Nickel	μg/L	287		42.2		94		11.5		63.2		109		92.8		12.6		40	
Selenium	μg/L	8	U	8	U	8	U	8	U	8	U	8	U	8	U	8	U	8	U
Silver	μg/L	2.4	J	4.3	J	7.3		11.5		7.6		5.2	В	4.1	В	0.62	В	4.5	J
Thallium	μg/L	10	U	10	U	10	U	10	U	10	U	10	U	10	U	50	U	10	U
Vanadium	μg/L	5	U	5	U	5	U	5	U	7.5		5.9		5.6		1.5	В	4	В
Zinc	μg/L	658,000	J	592,000	J	784,000	J	65,400	J	576,000		387,000		509,000		7,000		82,800	
Additional Water Quality Param	neters	-				-		_		-	-	-		-	•	_		-	
Alkalinity, Total as CaCO3	μg/L	32		98		24		142		19	J-	22	J-	10		40		12	
BOD, 5 day	μg/L	10	U	10	U	15.2		23.9		31.9		20	U	10	U	10		17.5	<u> </u>
Chemical Oxygen Demand	μg/L	61		86.5		114		170		106		78		86.5		38.5	J	86.5	<u> </u>
Dissolved Oxygen	μg/L	0.21		0.18		0.22		0.04		0.17		0.25		0.82		0.30		0.18	<u> </u>
Iron, Ferrous	μg/L	0.14	J-	0.13	J-	0.17	J-	727	J-	0.33	J-	0.48	J-	0.26	J-	40.5	J-	NS	<u> </u>
Nitrate as N	μg/L	0.04	J	0.033	J	0.044	J	0.037	J	0.044	J	0.036	J	0.032	J	0.1	U	0.1	U
Nitrite as N	μg/L	0.0044	J	0.0031	J	0.0028	J	0.0074	J	0.01	U	0.01	U	0.0052	J	0.01	U	0.0058	J
Oxidation-Reduction Potential	μg/L	-49.3		-59.4		-10.3		-28.4		-107.0		-64.1		-85.3		-71.3		-167.7	
рН	μg/L	4.33		4.90		4.47		5.10		4.17		4.1		6.74		5.65		3.06	<u> </u>
Sulfate	μg/L	2,270	В	2,590	В	3,350		2,580	В	3,420		2,380	В	2,000	В	742	В	NS	<u> </u>
Sulfide	μg/L	1	U	0.4	J	1	U	1	U	0.4	J-	0.6	J-	1	U	1	U	1	U
Total Dissolved Solids	μg/L	4,240		4,680		5,780		4,280		5,840		3,930		4,190		8,250		1,990	<u> </u>
Total Organic Carbon	μg/L	3.3		5.8		4.2		6.6		3.7	J-	3.3	J-	2.9		1.2	В	2.6	В

Detections in bold

Qualifier Keys can be viewed in the attached validation reports

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APPENDIX A

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Table 2 Pre-Design Investigation Borings

				Analyt	ical Parameters	
Sample Location	REC or Source Area	Boring Depth	Sample Depth	Soil	Groundwater	Rationale
RW-001-GB	Possible PRB Wall Alignment	50 feet	0-1'	FOC, Bulk Density, Total Porosity and Grain Size Analysis		Characterize soil to evaluate viability of possible
KW-001-0B	TOSSIDIE TIKD wan Anglinient	50 1001	Every 5' to 50'	TOC, Burk Density, Total Tolosity and Orani Size Analysis		PRB wall for groundwater treatment
RW-002-GB	Possible PRB Wall Alignment	50 feet	0-1'	FOC, Bulk Density, Total Porosity and Grain Size Analysis		Characterize soil to evaluate viability of possible
Rti 002 GB		50 1000	Every 5' to 50'	Toe, Burk Density, Total Torosity and Grain Size Thiarysis		PRB wall for groundwater treatment
RW-003-GB	Possible PRB Wall Alignment	50 feet	0-1'	FOC, Bulk Density, Total Porosity and Grain Size Analysis		Characterize soil to evaluate viability of possible
	gg		Every 5' to 50'	,		PRB wall for groundwater treatment
RW-004-GB	Possible PRB Wall Alignment	50 feet	0-1'	FOC, Bulk Density, Total Porosity and Grain Size Analysis		Characterize soil to evaluate viability of possible
			Every 5' to 50'	,		PRB wall for groundwater treatment
RW-057-SB	SMWU 27 (REC 6A)	35 feet	0-1'	COPI List (RCRA) Metals and Grain Size Analysis	TOC, TDS, BOD, COD, Total Metals, pH, ORP, Sulfide, Ferrous	Characterize soil and groundwater to define nature
	Sludge Bin Storage Area		Every 5' to 35'		Iron, DO, Sulfate, Nitrate (as N) and Alkalinity (CaCO3)	and extent of suspected source area
RW-058-SB	SMWU 27 (REC 6A)	35 feet	0-1'	COPI List (RCRA) Metals and Grain Size Analysis		Characterize soil to define nature and extent of
	Sludge Bin Storage Area		Every 5' to 35'			suspected source area
RW-059-SB	SMWU 27 (REC 6A)	35 feet	0-1'	COPI List (RCRA) Metals and Grain Size Analysis		Characterize soil to define nature and extent of
	Sludge Bin Storage Area		Every 5' to 35'	· · · · ·		suspected source area
RW-060-SB	SMWU 27 (REC 6A)	35 feet	0-1'	COPI List (RCRA) Metals and Grain Size Analysis		Characterize soil to define nature and extent of
	Sludge Bin Storage Area		Every 5' to 35'			suspected source area Characterize soil to define nature and extent of
RW-061-SB	SMWU 27 (REC 6A)	35 feet	0-1'	COPI List (RCRA) Metals and Grain Size Analysis		
	Sludge Bin Storage Area		Every 5' to 35'			suspected source area Characterize soil to define nature and extent of
RW-062-SB	SMWU 27 (REC 6A)	35 feet	0-1'	COPI List (RCRA) Metals and Grain Size Analysis		
	Sludge Bin Storage Area		Every 5' to 35'		TOC TDS DOD COD Total Matale all ODD Sulfide Formance	suspected source area
RW-063-SB	SWMU 29 (REC 6C) East Pond	35 feet	0-1' Every 5' to 35'	COPI List (RCRA) Metals, FOC and Grain Size Analysis	TOC, TDS, BOD, COD, Total Metals, pH, ORP, Sulfide, Ferrous Iron, DO, Sulfate, Nitrate (as N) and Alkalinity (CaCO3)	Characterize soil and groundwater to define nature and extent of suspected source area
	SWMU 29 (REC 6C)		0-1'		fion, DO, Suffate, Millate (as N) and Alkannity (CaCOS)	Characterize soil to define nature and extent of
RW-064-SB	East Pond	35 feet	Every 5' to 35'	COPI List (RCRA) Metals, FOC and Grain Size Analysis		suspected source area
	SWMU 29 (REC 6C)		0-1'			Characterize soil to define nature and extent of
RW-065-SB	East Pond	35 feet	Every 5' to 35'	COPI List (RCRA) Metals, FOC and Grain Size Analysis		suspected source area
	SWMU 29 (REC 6C)		0-1'			Characterize soil to define nature and extent of
RW-066-SB	East Pond	35 feet	Every 5' to 35'	COPI List (RCRA) Metals, FOC and Grain Size Analysis		suspected source area
	SWMU 29 (REC 6C)		0-1'		TOC, TDS, BOD, COD, Total Metals, pH, ORP, Sulfide, Ferrous	Characterize soil and groundwater to define nature
RW-067-SB	East Pond	35 feet	Every 5' to 35'	COPI List (RCRA) Metals, FOC and Grain Size Analysis	Iron, DO, Sulfate, Nitrate (as N) and Alkalinity (CaCO3)	and extent of suspected source area
	SWMU 29 (REC 6C)		0-1'			Characterize soil to define nature and extent of
RW-068-SB	East Pond	35 feet	Every 5' to 35'	COPI List (RCRA) Metals, FOC and Grain Size Analysis		suspected source area
	SWMU 29 (REC 6C)	25.6	0-1'			Characterize soil to define nature and extent of
RW-069-SB	East Pond	35 feet	Every 5' to 35'	COPI List (RCRA) Metals, FOC and Grain Size Analysis		suspected source area
DUL 070 CD	SWMU 29 (REC 6C)	25.6	0-1'		TOC, TDS, BOD, COD, Total Metals, pH, ORP, Sulfide, Ferrous	Characterize soil and groundwater to define nature
RW-070-SB	East Pond	35 feet	Every 5' to 35'	COPI List (RCRA) Metals, FOC and Grain Size Analysis	Iron, DO, Sulfate, Nitrate (as N) and Alkalinity (CaCO3)	and extent of suspected source area
			2		TOC, TDS, BOD, COD, Total Metals, pH, ORP, Sulfide, Ferrous	Characterize groundwater to evaluate possible
RW02-PZM020	Existing Monitoring Well		25 feet		Iron, DO, Sulfate, Nitrate (as N) and Alkalinity (CaCO3)	remedial technologies
RW07-PZM017	Existing Monitoring Well				TOC, TDS, BOD, COD, Total Metals, pH, ORP, Sulfide, Ferrous	Characterize groundwater to evaluate possible
			25 feet		Iron, DO, Sulfate, Nitrate (as N) and Alkalinity (CaCO3)	remedial technologies
RW10-PZM020	Existing Monitoring Well		07.0		TOC, TDS, BOD, COD, Total Metals, pH, ORP, Sulfide, Ferrous	Characterize groundwater to evaluate possible
			25 feet		Iron, DO, Sulfate, Nitrate (as N) and Alkalinity (CaCO3)	remedial technologies
RW19-PZM020	Existing Monitoring Well		25 fast		TOC, TDS, BOD, COD, Total Metals, pH, ORP, Sulfide, Ferrous	Characterize groundwater to evaluate possible
			25 feet		Iron, DO, Sulfate, Nitrate (as N) and Alkalinity (CaCO3)	remedial technologies
RW20-PZM020	Existing Monitoring Well		25 feet		TOC, TDS, BOD, COD, Total Metals, pH, ORP, Sulfide, Ferrous	Characterize groundwater to evaluate possible
	- -		25 1001		Iron, DO, Sulfate, Nitrate (as N) and Alkalinity (CaCO3)	remedial technologies

Soil Borings Sampling Density Requirements (from Worksheet 17 - Sampling Design and Rationale) See Table 1 Footnotes n n n n n n n n n

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APPENDIX B

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Project ARM P Client Site		: S : 1 : E : S on : F	(Sparrow 50298N EnviroAr Sparrow Parcel A	/I nalytics Group s Point - Area 3	Date/ Time Completed : 10/22/2015 - 15:00 Easting Logged By : PNV Surface Checked By : ESM Depth t Driller : Mike Waller - Allied Total D Drill Rig Type/Method : Dietrich B-120 Depth t Bit/Auger Size : 8" (4.25" ID) HSA Easting	g (US ft) (US ft) Elevation (ft) o Refusal (ft) epth (ft bgs) o Water (ft bgs	: 572,264.00 : 1,456,076.19 : 10.37 : NA : 51.5 :) : 9
Weathe	er	: C	Clear, 68	5 F			
Depth (ft.)	Sample No:	Recovery (%)	PID (PPM):	Blow Count	DESCRIPTION	nscs	REMARKS
0-	ST-1	100	-	-	0-5' SAND with gravel slag, dark gray to black, dry to moist		ST-1 @ 0-1.1'
2-	SS-1	74	0.6	6-4-5-5		SW-GW	SS-1 @ 1-3'
4					5-9' SAND with gravel, dark gray to black, some yellow		SS-2 @ 5-7'
6	SS-2	70	0.9	3-5-6-25	gravel and white crystalline material	SW	
8-					9-11.5' CLAY, light brown to gray, with fine sand and gravel		_
10	SS-3	80	0.0	3-1-2-1		CL	SS-3 @ 10-12'
12-	07.0	400			11.5-12.5' CLAY, lean with sand, gray to brown	CL	ST-2 @ 12-13.2'
- - 14-	ST-2	100	-	-	12.5-15' Clayey SAND, gray, fine-grained, mottled	SC	
	ST-3	100	-		15-18.5' CLAY, lean, gray		ST-3 @ 15-16'
16	SS-4	80	0.0	4-7-8-10		CL	SS-4 @ 16-18'
18-							SS-5 @ 18-20'
20-	SS-5	100	-	2-3-3-5	18.5-20' Clayey SAND, light brown to gray, fine to coarse grained sand with gravels	sc	
					20-21.5' Silty CLAY, gray	ML/CL	
22-	SS-6	80	-	-	21.5-24' Clayey SAND, gray, fine grained	SC	ST-4 @ 22.5-25'
24-	ST-4	100	-	-	24-26' SAND, tan, fine grained with trace gravel	SW	SS-7 @ 25-27'
26-	SS-7	100	0.0	3-2-1-2	26-34.5' CLAY, lean		ST-5 @ 27-29.5'
28-	ST-5	92	-	-		CL	
30-	SS-8	100	0.0	3-2-3-3			SS-8 @ 29.5-31.5'

t Name Project No.	: 5 : 1 : E : 5 on : F	(Sparrow: 50298N EnviroAr Sparrow: Parcel A	page 2 of 2 s Point A halytics Group s Point - Area 3	Date/ Time Completed: 10/22/2015 - 15:00Logged By: PNVChecked By: ESMDriller: Mike Waller - AlliedDrill Rig Type/Method: Dietrich B-120Bit/Auger Size: 8" (4.25" ID) HSA	Easting (US ft) Surface Elevation (ft) Depth to Refusal (ft) Total Depth (ft bgs)	: 572,264.00 : 1,456,076.19 : 10.37 : NA : 51.5) : 9
Sample No:	Recovery (%)	:(WAA) OIA	Blow Count	DESCRIPTION	nscs	REMARKS
SS-8	100	0.0	3-2-3-3			
ST-6	92	-	-		CL	ST-6 @ 32-34.5'
- SS-9	100	0.0	2-2-3-4			SS-9 @ 34.5-36.5'
ST-7	92	-	-			ST-7 @ 37-39.5'
SS-10	100	0.0	2-2-2-3		CL	SS-10 @ 39.5-41.5'
ST-8	94	-	-			ST-8 @ 42-44.5'
SS-11	100	0.0	1-2-3-4	44.5-51.5' CLAY, lean, dark gray		SS-11 @ 44.5-46.5'
ST-9	92				CL	Terminated auger use at 47' ST-9 @ 47-49.5'
SS-10	100	0.0	3-3-3-3			SS-10 @ 49.5-51.5' no sample collected
-				End of Boring at 51.5' bgs	I	<u> </u>
- - - - - - -						
	Name Project No. De Locatic er SS-8 SS-8 SS-8 SS-9 ST-7 SS-10 ST-7 SS-10 ST-8 SS-11 ST-8 SS-11	t Name : S Project No. : 1 : E : S ole Location : F er : C Name : C Name : C SS-8 100 SS-8 100 SS-9 100 ST-7 92 SS-10 100 ST-8 94 SS-11 100 ST-9 92 SS-11 100 ST-9 92	Name : Sparrow Project No. : 150298N : EnviroAr : Sparrow Del Location : Parcel A er : Clear, 65 SS-8 100 0.0 SS-8 100 0.0 SS-8 100 0.0 SS-9 100 0.0 ST-7 92 - SS-10 100 0.0 ST-8 94 - SS-11 100 0.0 ST-9 92 -	Project No. : 150298M : EnviroAnalytics Group : Sparrows Point - Area A : Parcel A3 : Clear, 65 F Image: Series Image: Series	Boring ID: RW-001-GB (page 2 of 2) Description Name : Sparrows Point 'roject No. : Sparrows Point : Sparrows Point - Area A is EnviroAnalytics Group : Sparrows Point - Area A is clear, 65 F Description : Sike Waller - Allied Driller Division Completed : 10/22/2015 - 15:00 Logged By Division V Sparrows Point : Sparrows Point - Area A is clear, 65 F Description : Sike Waller - Allied Driller Division V V Str.6 92 . . Description SS-8 100 0.0 3-2-3-3 34.5-44.5' CLAY, lean, dark gray 0.5' sand lens at 36.2' bgs ST-7 92 ST-7 92 ST-7 92 . . . ST-7 92 . . . ST-8 94 . . . ST-9 92 . . . ST-8 94 . . . ST-9 92 . .	Boring ID: RW-001-GB (page 2 of 2) Date/Time Completed : 1022/2015 - 15:00 (page 2 of 2) East Surface Elevation (f) Deph to Refusal (f) Total Deph (ft bgs) Differ Date/Time Completed : 1022/2015 - 15:00 Unged By East ENV Differ East Surface Elevation (f) Deph to Refusal (f) Total Deph (ft bgs) Differ Date/Time Completed : 1022/2015 - 15:00 Unged By East EnvironAnalytics Group Signarous Point (ft bgs) East Surface Elevation (f) Deph to Refusal (f) Total Deph (ft bgs) Viel Location : Parcel A3 er : Clear, 65 F Image 1 Image 1

02-05-2016 P:\EnviroAnalytics Group\150298M EAG_Sparrows Point Area A\Documents\Parcel A3 (RVMM)\Boring Logs\PNV_Field Logs\RW-001-GB.bor

	Boring	g ID: F		0 02-GB (page 1 of 2)	Date/Time Started : 10/23/2015 - 10:45 Northing (Date/ Time Completed : 10/26/2015 Easting (L Logged By : PNV Surface E Checked By : ESM Depth to F	S ft) evation (ft)	: 572,053.70 : 1,456,037.53 : 10.17 : NA
ARM F Client Site	t Name Project No. ble Locatic er	. :1 :E :S	50298 InviroA	nalytics Group vs Point - Area \3	Driller: Mike Waller - AlliedTotal DeptDrill Rig Type/Method: Dietrich B-120Depth to WBit/Auger Size: 8" (4.25" ID) HSA		: 30
Depth (ft.)	Sample No:	Recovery (%)	PID (PPM):	Blow Count	DESCRIPTION	USCS	REMARKS
0-	SS-1	60	0.1	36-18-8-5	0-6' SAND and GRAVEL, dark gray to black, fine to medium grained sand (slag fill)		SS-1 @ 0.5-2.5'
4-	SS-2	40	2.9	3-6-6-2		SW-GW	SS-2 @ 3-5'
6-	SS-3	40	0.3	1-2-2-2	6-8' SAND, tan, fine grained	SP	
8- - - - 10-	SS-4	70	0.1	4-7-8-4	8-12' CLAY, lean, brown to gray	CL	SS-4 @ 8-10' ST-1 @ 10-12.5'
12-	ST-1	92	-	-	12-24' CLAY, lean with sand, gray, hard concretions at base		SS-5 @ 12.5-14.5'
14-	SS-5	-	0.1	4-6-8-10	of spoon sample		ST-2 @ 15-17'
16-	ST-2	92	-	-			SS-6 @ 17.5-19.5'
18-	SS-6	75	-	2-2-3-5		CL	ST-3 @ 20-20.5'
20-	ST-3	90	-	-			31-3 @ 20-20.3
24-	SS-7	65	-	1-3-4-7	24-30' SAND, tan, fine to coarse sand with rounded gravel		
26-	SS-8	75	-	6-12-18-18		SW	Attempt ST from 25-27.5'; advanced 1' with no recovery SS-8 @ 26-28'
28-	HSA	-	-	-			Attempt ST from 28-30'; advanced 0.8' with no recovery

02-05-2016 P:\EnviroAnalytics Group\150298M EAG_Sparrows Point Area A\Documents\Parcel A3 (R\WM)\Boring Logs\PNV_Field Logs\RW-002-GB.bor

Project ARM P Client Site	Name roject No. le Locatic	: S : 1 : E : S : S	(Sparrow: 50298M EnviroAr	1 nalytics Group s Point - Area 3	Date/ Time Completed : 10/26/2015 Ea Logged By : PNV Sa Checked By : ESM Da Driller : Mike Waller - Allied To Drill Rig Type/Method : Dietrich B-120 Da Bit/Auger Size : 8" (4.25" ID) HSA For the second s	lorthing (US ft) asting (US ft) surface Elevation bepth to Refusal (otal Depth (ft bgs bepth to Water (ft	(ft) : NA s) : 30
Depth (ft.)	Sample No:	Recovery (%)	PID (PPM):	Blow Count	DESCRIPTION	nscs	REMARKS
30— - -	SS-9	100	0.0	1-2-3-4	30-31.5' SAND, tan, fine to medium grained with trace clay and gravel, some iron concretions near bottom of sand lay	y ver SW	no recovery
32— -					31.5-33' Silty CLAY, gray, with trace sand at bottom of spo	oon ML/C	Took SS sample 30-32'
- - 34 — -					33-35.5' Clayey SAND, gray	sc	ST-4 @ 35-37.5'
36- - -	ST-4	100	-	-	35.5-39.5' Clayey SILT, gray, with some thin fine sand stringers		
- 38— -	SS-10	100	0.0	1-2-3-3		CL/N	AL SS-10 @ 37.5-39.5'
40- - - 42-	ST-5	100	-	-	39.5-42.5' Silty CLAY, gray	ML/C	ST-5 @ 40-42.5'
- - 44 —	SS-11	100	0.0	1-1-2-2	42.5-44' Clayey SILT, gray	CL/N	SS-11 @ 42.5-44.5
-					44-50' Silty CLAY, gray		ST-6 @ 45-47.5'
46 — - -	ST-6	92	-	-		ML/C	CL
48- - -	SS-12	100	_	1-1-2-2			Augers to 48' SS-12 @ 48-50'
- 50-					End of Boring at 50' bgs		
52							

E	Borinę	g ID: F		003-GB (page 1 of 2)	Date/ Time Completed : 10/28/2015 - 11:30 Logged By : PNV	Northing (US ft) Easting (US ft) Surface Elevation Depth to Refusion	on (ft)	: 571,852.74 : 1,456,029.15 : 10.16 : NA	
Client Site	roject No Ile Locatio	. :1 :E :S	50298l EnviroA	nalytics Group /s Point - Area \3	Driller: Mike Waller - AlliedDrill Rig Type/Method: Dietrich B-120Bit/Auger Size: 8" (4.25" ID) HSA	Total Depth (ft I	bgs)	: 69.5 : 13.5	
Depth (ft.)	Sample No:	Recovery (%)	PID (PPM):	Blow Count	DESCRIPTION		USCS	REMARKS	
0	SS-1	100	0.1	12-20-16-10	0-4' SAND, dark gray to black, fine to coarse grained with some gravel (slag fill)		SW	SS-1 @ 1-3'	
	SS-2	80	0.1	2-4-6-11	4-13' CLAY, lean, light gray with trace amounts of light brown Clayey SILT			SS-2 @ 5-7'	
8	SS-3	100	0.1	3-5-8-12			CL	SS-3 @ 10-12'	
	ST-1	90	-	-	13-19' CLAY, lean, gray to brown, with fine grained sand, trace clay, wet	,		ST-1 @ 12-14' ST-2 @15-16'	
16	ST-2 SS-4	100 87.5	- 0.2	- 2-3-4-3		CL	CL-SP	SS-4 @16-18'	
20-	ST-3	92	-	-	19-25' CLAY, lean, grayish brown		CL	ST-3 @ 20-22.5'	
24-	SS-5	80	0.1	2-3-4-10	25-26' Clayey SAND, dark brown, fine grained sand		SC	SS-5 @ 22.5-24.5' ST-4 at 25-27' (0.25" R)	
26-	ST-4	12.5	-	-	26-28' SAND with SILT, tan, well graded, fine to coarse grained, trace fine gravel and silt		V/SM	SS-6 @ 27-29'	
28-	SS-6	90	0.5	4-6-6-8	28-36.5' SAND, tan to light brown, fine to coarse grained, with some fine gravel and silt	,			
30- 	SS-7	100	0.4	6-10-40-30		S	SW	SS-7 @ 30-32'	
34-								SS-8 @ 35-37'	
36-	SS-8	85	0.0	3-5-9-13	36.5-37.5' Silty SAND, gray, fine grained, trace clay	ML	_/SW	· ·	
38-	SS-9	88	0.0	4-5-4-5	37.5-39' SAND, tan, fine to coarse grained with some fine gravel	e g	SW	SS-9 @ 37.5-39.5'	
40-					39-40' Clayey SILT, gray		_/ML		

Project	Name	: S	(Sparrow		Date/ Time Completed : 10/28/2015 - 11:30 Ea Logged By : PNV Su Checked By : ESM De Driller : Mike Waller - Allied To	orthing (US ft) asting (US ft) Irface Elevation (ft) apth to Refusal (ft) tal Depth (ft bgs)	: NA : 69.5
Client Site	roject No. Ie Locatic er	:E :S n :P		nalytics Group s Point - Area 3	Bit/Auger Size : 8" (4.25" ID) HSA	epth to Water (ft)	: 13.5
Depth (ft.)	Sample No:	Recovery (%)	PID (PPM):	Blow Count	DESCRIPTION	RSCS	REMARKS
40- 42-	SS-10	82	-	2-2-7-8	40-44' SAND, tan, fine to coarse grained with some fine gravel	SW	SS-10 @ 40-42'
44	SS-11	80	-	2-4-7-12	44-45' Silty SAND, gray, fine grained 45-46' SAND, tan, fine to medium grained	SM SP	SS-11 @ 43-45'
46	SS-12	40	0.0	2-1-1-1	46-47.5' Sandy SILT, gray, fine grained sand with trace clay 47.5-49' Sandy SILT, fine to coarse grained, gray	y ML ML	SS-13 @ 48-50'
50- 52-	SS-13 ST-5	75 92	0.0	4-6-4-2 -	49-50' Clayey SAND, gray, fine grained 50-51 SAND, gray, fine grained 51-59.5' Clayey SAND, gray, fine grained	SC SP	ST-5 @ 50-52.5
54	SS-14	65	0.0	4-4-6-6			SS-14 @ 52.5-54.5' ST-6 @ 55-57.5'
56	ST-6	92	-	-		SC	SS-15 @ 57.5-59.5'
58 - 60 -	SS-15	-	0.0	4-4-4-4	59.5-63.5' Clayey SAND, gray		_
62	SS-16	90	0.0	4-5-4-5		SC	SS-16 @ 62.5-64.5'
64 – 66 –	ST-7	92	-	_	63.5-69.5' Sandy SILT, gray	SW/ML	ST-7 @ 65-67.5'
68	SS-17	90	0.0	4-4-4-5			SS-17 @ 67.5-69.5'
70- 					End of Boring at 69.5' bgs		
74-							
76- - 78-							
- 80-							

E	Boring	g ID: F		004-GB (page 1 of 2)			: 571,654.30 : 1,456,051.90 : 10.06 : NA	
Client Site	roject No. le Locatic	: 1 : E : S	50298I InviroA	nalytics Group /s Point - Area	Driller: Mike Waller - AlliedTotalDrill Rig Type/Method: Dietrich B-120DepthBit/Auger Size: 8" (4.25" ID) HSA	Depth (ft bgs) to Water (ft)	: 52.5 : -	
Depth (ft.)	Sample No:	Recovery (%)	PID (PPM):	Blow Count	DESCRIPTION	nscs	REMARKS	
0-					0-2' Gravelly SAND, dark brown to black, trace clay	GW-SW	SS-1 @ 1-3'	
2-	SS-1	100	0.1	42-25-18-20				
- - 4- -					2-5' Clayey SAND, light gray	SC		
6-	SS-2	100	0.2	4-6-6-7	5-11' Clayey SILT, light gray to brown with some mottling		- SS-2 @ 5-7'	
8-						CL/ML	SS-3 @ 8-10'	
- - 10-	SS-3	100	0.3	2-6-7-7			ST-1 @10-12.3'	
-	ST-1	92	-	-	11-15' CLAY, light gray		-	
12	SS-4	100	0.4	2-2-2-2		CL	SS-4 @ 12.5-14.5'	
14-							ST-2 @ 15-16.5'	
- 16-	ST-2	100	-	-	15-16.5' SAND with SILT, poorly graded	SP/SM		
-	SS-5	80	5.9	2-2-4-5	16.5-17' SAND, light brown, fine grained 17-19' SAND, light gray, fine grained	SP	SS-5 @ 16.5-18.5'	
18-			0.0		איז איזער איזער, איזער איזער איזער איזער איזער איזער איזער איז איזער איז איז איזער איז איזער איז איז איז איזער	SP		
20-					19-21' Clayey SAND, dark gray, fine grained	SC	ST-3 @ 20-22.3'	
22-	ST-3	92	-	-	21-25' Clayey SAND, brown to dark gray			
24-	SS-6	100	0.2	2-5-6-5		SC	SS-6 @ 22.5-24.5'	
- - 26-	ST-4	80	-	-	25-26.5' SILT, dark brown, with sand	ML	ST-4 @ 25-26.5'	
	SS-7	75	0.6	4-4-9-6	26.5-30' SAND, tan to gray, fine grained		SS-7 @ 26.5-28.5'	
28-			5.5			SP		
30-							ST-5 @ 30-31.3'	

Project ARM P Client Site	Name roject No. le Locatio	: S : 1 : E : S	Sparrow 50298I EnviroA	nalytics Group /s Point - Area	Date/ Time Completed : 10/29/2015 - 15:00 Ea Logged By : PNV Si Checked By : ESM Di Driller : Mike Waller - Allied To Drill Rig Type/Method : Dietrich B-120 Di Bit/Auger Size : 8" (4.25" ID) HSA	orthing (ft) asting (ft) urface Elevation (ft) epth to Refusal (ft) otal Depth (ft bgs) epth to Water (ft)	: 571,654.30 : 1,456,051.90 : 10.06 : NA : 52.5 : -
Depth (ft.)	Sample No:	Recovery (%)	PID (PPM):	Blow Count	DESCRIPTION	NSCS	REMARKS
30-	ST-5	24	-	-	30-32.5' Clayey SAND, gray, with some fine sand		ST-5 @ 30-31.3'
32-						SC	- SS-8 @ 32.5-34.5'
-	SS-8	70	0.3	4-4-4-4	32.5-33.5' SAND, fine to coarse grained, trace fine gravel 33.5-36' Clayey SAND, gray, with some fine sand	SW	00-0 ₩ 02.0-04.5
34					33.5-36 Clayey SAND, gray, with some line sand	SC	ST-6 @ 35-36.1'
36-	ST-6	86	-	-	36-39' SAND, light gray, fine grained		SS-9 @ 36.1-38.1'
-	SS-9	100	0.8	7-10-10-12		SP	
38- - -					39-42.5' Clayey SAND, gray		-
40-	ST-7	100	_		So 42.6 Olayey On ND, gray	SC	ST-7 @ 40-41.5'
- 42-	51-7	100	_	-			SS-10 @ 41.5-43.5'
-	SS-10	100	0.0	3-4-5-6	42.5-44.5' Silty CLAY, gray	ML/CL	-
44					44.5-45' SAND, gray, fine grained	SP	
46-	ST-8	100	-	-	45-51' Sandy CLAY, lean, gray		- ST-8 @ 45-46.8'
-							SS-11 @ 46.8-48.8'
48-	SS-11	50	-	3-6-9-5		CL	
- - 50-							ST-9 @ 50-52.5'
-	ST-9	100	-	-	51-52.5' CLAY, lean, dark gray		-
52-					End of boring at 52.5' bgs	CL	
- 54-							
-							
56							
58-							
-							
60-							

02-05-2016 P:\EnviroAnalytics Group\150298M EAG_Sparrows Point Area A\Documents\Parcel A3 (RVMM)\Boring Logs\PNV_Field Logs\RW-004-GB.bor

E	Boring	Eartl	M Group h Resource En and Consultar RW-057-S (page 1	gineers ats B	Proje Site ARM Cheo Drillin Drillie	Project No.: 150298M-11-3Weather: Raict Description: Sparrows Point - Parcel A3	/1/2015 niny 2,115.07 456,436.55	
Depth (ft.)	% Recovery	PID Reading (PPM)	Sample No/Interval	XRF - Zn (PPM)	XRF - Cd (PPM)	DESCRIPTION	USCS	REMARKS
0	80	-	RW-057-SB-1	55,100 80,204 57,886	725 1.990 2,767	(0-3') Slag, clayey to gravel sized, dark brown, moist, loose, no plasticity	GM	
-	80	-	KW-057-5B-5	13,847	123	(3-4') Sandy SILT, dark tan, moist, firm, no cohesion, no plasticity	SM	
5-		-		4,452	181	(4-10') SAND, orangish tan, moist, no cohesion, no plasticity		
		-	RW-057-SB-6	2,845	ND<57			
_		-		2,397	ND<55		SM-	
-	70	-		814	ND<54		SW	
-		-		212 596	ND<53 ND<54			
10-		-		202	ND<51	(10-13') SAND, beige, wet, soft, no cohesion, no plasticity	_	Wet at 10' bgs
-		-		163	ND<51		SM	
	100	-		166	ND<51			
1		-		382	ND<51	(13-17') Sandy CLAY, gray to dark gray, moist to wet, firm, high		
15-		-	RW-057-SB-15	1,019	262	cohesion, high plasticity	sc	
		-	RW-057-SB-16	791	399			
		-		292	901			
	100	-		315	132	(17-20') SAND, medium to coarse grained, dark gray, wet, very		
		-		502	ND<51	soft, no cohesion, no plasticity	SM	
20-		-		901	ND<53		_	
-		-		1,737	ND<60	(20-24.5') CLAY, brown, wet, soft, high cohesion, high plasticity		
-	100	-	RW-057-SB-23	1,539 1,707	ND<55 108		СН	
-	100	-	201-00-20	1,307	82			
		-		1,310	67		CN/	
25-		-		52	ND<55	(24.5-25') SAND, brown, wet, soft, no cohesion, no plasticity	SM	
1		-		64	ND<55	(25-30') Gravelly SAND, light tan, wet, loose, no plasticity		
1	100	-		69	ND<54		SW	
]		-	RW-057-SB-29	131	ND<43			
30-		-		63	ND<54			
		-		1,024	168	(30-33') Sandy CLAY, gray, wet, firm, high cohesion, medium plasticity		
		-	RW-057-SB-32	1,235	196	producty	SC	
	100	-		584	88	(22.251) OLAV dod. group firm high astronomic tick starts '	_	Boring
		-		580 218	67 67	(33-35') CLAY, dark gray, firm, high cohesion, high plasticity	СН	terminated at 35' bgs
35-		-		210	07			

Total Borehole Depth: 35' bgs.

E	Boring	Eartl	M Group h Resource En and Consultan RW-058-S (page 1 d	gineers tts B	A F S A C C	Client RM Project No. Project Description Site Location RM Representativ Checked by Drilling Company Driller Drilling Equipment	: Sparrows Point, MD	Date : 10/5/2015 Weather : Sunny Northing (US ft) : 572,177.57 Easting (US ft) : 1,456,500.09			
Depth (ft.)	% Recovery	PID Reading (PPM)	Sample No/Interval	XRF Zn (PPM)		XRF Cd (PPM)	DE	ESCRIPTION	USCS		
0-		-	RW-058-SB-1	12192 ± 1	13	378 ± 20	(0-3') Slag, sand sized, black,	moist, loose, no plasticity			
		-	RW-058-SB-2	1747 ± 2	25	95 ± 16			SM		
-	60	0.0		1289 ± 1		107 ± 15					
-		0.0 0.0		416 ± 10 NA	0	ND <41 NA	(3-4') Sandy CLAY, orangish t ∖plasticity	tan, moist, soft, low cohesion, medium	sc		
5-		0.0		47 ± 4		ND <38		wet, soft, no cohesion, no plasticity,	_ sw		
-		0.0		62 ± 4		ND <39	wet at 5' bgs				
	100	0.0	RW-058-SB-8	576 ± 12	2	56 ± 14	(7-8') CLAY, light gray, wet, hi	igh cohesion, medium plasticity	CL		
		0.0		351 ± 9)	47 ± 14	(8-9.3') SAND, orange, wet, so	oft, no cohesion, no plasticity	SW		
10-		0.0		461 ± 11	1	71 ± 14	(9.3-10') Sandy CLAY, orange	e, wet, firm, medium cohesion, low	SC		
-		-		268 ± 8		54 ± 13		· · · · · · · · · · · · · · · · · · ·	_/ sм		
-	100	-		267 ± 7		52 ± 13	(10-12) SAND, fine to mediun	dium grained with trace clay, orange, wet, ticity			
-	100	-		194 ± 7 221 ± 7		61 ± 14 ND <38	(12-15') SAND, fine to mediun	AND, fine to medium grained, orange, wet, soft, no			
-			RW-058-SB-15	324 ± 8		61 ± 13	cohesion, no plasticity		SW		
15-		-		124 ± 6		ND <43	(15-18.7') SAND, fine to media	um grained, orange, wet, slightly firm, no			
-		-		83 ± 5		41 ± 13	cohesion, no plasticity		sw		
-	90	-		121 ± 5	5	ND <38			1500		
-		-		251 ± 8	3	ND <42					
20		-		1118 ± 1	6	59 ± 14	(18.7-21') CLAY, grayish beige plasticity	e, wet, very soft, high cohesion, high	Сн		
20-		-		288 ± 8	8	ND <41					
]		-	RW-058-SB-22	478 ± 11	1	ND <43		n grained, orange, wet, soft, no	sw		
	60	-		133 ± 5		55 ± 13	cohesion, no plasticity				
-		-		59 ± 4		ND <39		e grained with gravels, finer grained vet, soft, no cohesion, no plasticity			
25-		-		NA		NA	and light orange with depth, w	et, son, no conesion, no plasticity			
		-		36 ± 3		38 ± 12					
-	00	-		82 ± 5	2	ND <43			SW		
-	80	-	RW-058-SB-28	661 ± 13 555 ± 12		90 ± 15 56 ± 14					
-		-		555 ± 12 NA	۲	56 ± 14 NA					
30-		-		193 ± 7		ND <42	(30-35') CLAY, brown, firm, hi	gh cohesion, very high plasticity			
-		-	RW-058-SB-32	258 ± 8		ND <41	· · · · · · · · · · · · · · · · · · ·	J			
-	100	-		163 ± 7		ND <44			Сн		
1		-		105 ± 6		ND <49					
		-		98 ± 5		ND <42					
35-		epth: 35'									

Total Borehole Depth: 35' bgs.

80 117.5 RW-059-SB-3 >10% ± 0% 987 5- 0 1.1 7824 ± 85 <60 (359 ± 46		Boring	Eartl	M Group h Resource En and Consultar RW-059-SI (page 1 d	gineers ats	AI Pr Si AI CI DI DI	lient RM Project No. roject Description ite Location RM Representative hecked by rilling Company riller rilling Equipment	: EnviroAnalytics Group : 150298M-11-3 : Sparrows Point - Parcel A3 : Sparrows Point, MD : L. Perrin : W. Mader P.G., CPSS : Green Services, Inc : Don Marchese : Geoprobe 7822DT	Date : 10/1/2015 Weather : Rainy Northing (US ft) : 572,159.86 Easting (US ft) : 1,456,362.07			
0.3 RW-059-SB-1 8005 98 (0-3.5) Slag, coarse grained to gravel sized, black, loose, no cohesion, no plasticity GM 5- 0 117.5 RW-059-SB-3 >10% ± 0% 987 (3.5-4.5) SAND, orange, wet, soft, no cohesion, no plasticity GM 5- 0 11 7824 ± 85 < 60	Depth (ft.)	% Recovery	PID Reading (PPM)	Sample No/Interval	XRF Zn (PPM)		ZRF Cd (PPM)	D	ESCRIPTION	nscs		
5 0 3599 ± 46 70 ± 19 (3.5-4.5) SAND, with rece clay, brownish red, moist, soft, no SM 80 - 507 ± 15 ND <56	0	80	9.7		13221	%	128		gravel sized, black, loose, no	GM		
80 - 507 ± 15 404 ± 13 188 ± 9 ND <54 ND <54 188 ± 9 no plasticity SW 10 - RW-059-SB-11 236 ± 10 ND <53 121 ± 7 ND <53 121 ± 7 ND <53 121 ± 7 ND <54 1171 ± 22 ND <55 133 ± 12 ND <54 1171 ± 22 (13.5-15') CLAY, reddish brown, high cohesion, high plasticity CH 100 - - 889 ± 15 1171 ± 22 ND <55 133 ± 12 (13.5-15') CLAY, reddish brown, high cohesion, high plasticity CH 100 - - 889 ± 15 1177 ± 15 81 ± 14 1802 ± 21 (17.5-20') SAND, fine to medium grained, beige, wet, soft, no cohesion, no plasticity SW 20 - RW-059-SB-20 955 ± 15 108 ± 14 (17.5-20') SAND, fine to medium grained, gray, wet, soft, no cohesion, no plasticity SM 20 - RW-059-SB-20 955 ± 15 108 ± 14 107 ± 13 (20-22') SINS AND, gray, wet, soft, no cohesion, no plasticity SM 20 - RW-059-SB-23 2490 ± 30 60 ± 16 (22-25') CLAY, brown, wet, sticky, soft, high cohesion, high plasticity CH 25 - - RW-059-SB-26 1064 ± 18 ND <45	5-			RW-059-SB-6	3599 ± 4	6	70 ± 19	cohesion, no plasticity	· · · · ·	SM SW		
10 . RW-059-SB-11 502 ± 14 ND <53	-	80	- -		507 ± 15 404 ± 13	5 3	ND <56 ND <54		gish brown, wet, soft, no cohesion,	SW		
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	-	100		RW-059-SB-11	502 ± 14 236 ± 10	1)	ND <53 ND <53			300		
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	- - 15-		- -		333 ± 12	2	ND <54			СН		
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	· -	100	-		797 ± 15	5	79 ± 15	cohesion, no plasticity (17.5-20') SAND, fine to medium		SW		
90 - RW-059-SB-23 2490 ± 30 60 ± 16 (22-25') CLAY, brown, wet, sticky, soft, high cohesion, high plasticity CH 25 - RW-059-SB-26 1105 ± 17 ND <42			-	RW-059-SB-20	955 ± 15 1802 ± 2	5 1	108 ± 14 107 ± 13	· · · ·	soft, no cohesion, no plasticity	SM SM		
- 813 ± 14 ND <41		90	-	RW-059-SB-23	2490 ± 3 1692 ± 2	0 0	60 ± 16 78 ± 13	(22-25') CLAY, brown, wet, stick	xy, soft, high cohesion, high plasticity	СН		
- 813 ± 14 ND <41	25-		-	RW-059-SB-26	1105 ± 1	7	ND <42	(25-27.2') CLAY, dark gray, wet	, firm, high cohesion, high plasticity	СН		
- 813 ± 14 ND <41	30-	90			167 ± 6 326 ± 9 132 ± 6		ND <40 ND <41 ND <42			SW		
- 813 ± 14 ND <41		100	-				1 1					
			-	RW-059-SB-34				(33-35') CLAY, gray, wet, hard,	high cohesion, high plasticity	СН		

Total Borehole Depth: 35' bgs.

	P	Earth	A Group h Resource Eng and Consultan	gineers	AF Pr Sit AF	ient RM Project No. oject Description te Location RM Representative	: EnviroAnalytics Group : 150298M-11-3 : Sparrows Point - Parcel A3 : Sparrows Point, MD e : L. Perrin : W. Mader P.G., CPSS	Date : 10/5/2015 Weather : 60s F, sunny	
E	Boring	g ID: I	RW-060-S (page 1 d		Dr Dr	necked by illing Company iller illing Equipment	Northing (US ft) : 572,070.27 Easting (US ft) : 1,456,510.50		
Depth (ft.)	% Recovery	PID Reading (PPM)	Sample No/Interval	XRF Zn (PPM)		XRF Cd (PPM)	DE	ESCRIPTION	USCS
0-		-	RW-060-SB-1	1092 ± 2	0		(0-0.5') Topsoil, with organic r moist, soft, slight cohesion, no	natter and trace clay, dark brown, plasticity	ML
		0.0		888 ± 14 619 ± 12 1204 ± 18			(0.5-2.5') Silty SAND, light bei plasticity	ge, slightly firm, no cohesion, no	_ SM
	76	0.1				ND <40 -	(2.5-4.3') SAND, light beige, s	lightly firm, no cohesion, no plasticity	
		0.0	RW-060-SB-4			ND <44			sw
5-		0.0		496 ± 11	I	ND <44	(4.3-5') Sandy SILT, beige, dr	y, hard, no cohesion, no plasticity	SM
		0.0		1203 ± 1	9		(5-10') CLAY, brown with red a high plasticity	streaks, dry, very firm, high cohesion,	
		0.0	RW-060-SB-7	1464 ± 2	2	ND <47			
	100	0.0		1129 ± 1	7	46 ± 14			СН
		0.0		898 ± 15	5	ND <42			
		0.0		877 ± 14	1	ND <41			
10-		0.0		771 ± 14	1		(10-14.3') CLAY, grayish brow plasticity, wet at 14.2' bgs	n, moist, firm, high cohesion, high	
1		0.0	RW-060-SB-12	777 ± 14	1	66 ± 14			
]	100	0.0		488 ± 11	I	60 ± 14			СН
]		0.0		397 ± 9		71 ± 13			
15		0.0		276 ± 8				clay, orange, wet, soft, no cohesion,	
15—		-		133 ± 6		ND <39	no plasticity		SM
-		-		160 ± 6		ND <41	(15.8-19') SAND, orange, wet	, soft, no cohesion, no plasticity	
1	83	-		347 ± 9		ND <41			sw
-		-		1613 ± 2	0	ND <41			
20-		-	RW-060-SB-20	3763 ± 3	6		(19-20') CLAY, with trace clay high plasticity	, dark gray, wet, firm, high cohesion,	СН

E	Boring	Eart	M Group h Resource En and Consultar RW-060-S (page 2 d	gineers ats B	AI Pr Si AI CI DI DI	lient RM Project No. roject Description ite Location RM Representative hecked by rilling Company riller rilling Equipment	: EnviroAnalytics Group : 150298M-11-3 : Sparrows Point - Parcel A3 : Sparrows Point, MD : L. Perrin : W. Mader P.G., CPSS : Green Services, Inc : Kevin Pumphrey : Geoprobe 7822DT	Weather : 60 Northing (US ft) : 57	0/5/2015 Ds F, sunny 72,070.27 456,510.50	
Depth (ft.)	% Recovery	PID Reading (PPM)	Sample No/Interval	XRF Zn (PPM)		XRF Cd (PPM)	DE	ESCRIPTION		USCS
20-		-		1667 ± 2	1		(20-24.9') CLAY, gray, wet, sc 24.5'	ft, high cohesion, high pla	asticity, firm at	
-		-	RW-060-SB-22	2110 ± 2	4	61 ±14				
-	93	-		2596 ± 2	9	ND <43				с⊦
		-		1291 ± 2	3	ND <54				
		-		294 ± 9		ND <44				
25-		- 897 ± 15	5	ND <42	(24.9-26') SAND, gray, wet, soft, no cohesion, no plasticity					
	-		86 ± 5			(26-27') SAND, fine to coarse no cohesion, no plasticity	grained, well graded, gra	y, wet, soft,	sw	
	80	-		140 ± 6			(27-29.5') SAND, fine to coars soft, no cohesion, no plasticity		orange, wet,	
		-		59 ± 4		ND <40				SW
30-		-		114 ± 5			(29.5-31.3') SAND, poorly gra	ded, orange with reddish	tint, no	
		-		304 ± 8		44 ± 13	cohesion, no plasticity			SP
		-		499 ± 10)	89 ± 13	(31.3-32.8') SAND, fine to coa soft, no cohesion, no plasticity	rse grained with some gra		sw
	73	-		773 ± 14	1	181 ± 15	(32.8-35') CLAY, gray, wet, ha	ard, high cohesion, high p		
-		-	RW-059-SB-34	485 ± 11	I	153 ± 14	(,g,g p		с⊦
35-		-		181 ± 7		75 ± 14	End of Boring			
- - - 40-										

	Boring	Eartl	M Group h Resource Eng and Consultan RW-061-S (page 1 d	gineers tts B	AF Pr Si AF Cf Dr Dr	ient RM Project No. roject Description te Location RM Representativ necked by rilling Company riller rilling Equipment	: EnviroAnalytics Group : 150298M-11-3 : Sparrows Point - Parcel A3 : Sparrows Point, MD e : L. Perrin : W. Mader P.G., CPSS : Green Services, Inc : Kevin Pumphrey : Geoprobe 7822DT	Date : 10/5/2015 Weather : 60s F, sunny Northing (US ft) : 572,054.65 Easting (US ft) : 1,456,375.09	
Depth (ft.)	% Recovery	PID Reading (PPM)	Sample No/Interval	XRF Zn (PPM)		XRF Cd (PPM)	DES	SCRIPTION	USCS
0-		0.5	RW-061-SB-1	1026 ± 2	1	ND <56	(0-1') Slag, coarse grained, bla	ack. drv. loose. no plasticity	SM/GN
-		17.5	RW-061-SB-2	>10% ± 1			(1-1.5') SILT, with very fine sa		ML
-	100	1.7		6834 ± 5		59 ± 14	cohesion, no plasticity		
-		35.2		794 ± 14	1			th trace silt, black, oily, moist to very	SM
_		8.7		100 ± 5		58 ± 14	moist, plasticity increasing with	n deptil, petibledin odol	
5-		-		796 ± 12	2	120 ± 13	(5-7') SAND, light brown, wet,	loose, soft, no plasticity	0.4/
-		-	RW-061-SB-7	1410 ± 1	9	ND < 42			SW
	90	-		944 ± 16	5			wn, dry, firm, low cohesion, low	SC
_		0.0		261 ± 8		IND <44	plasticity		
10-		0.0		71 ± 5			plasticity	moist, high cohesion, medium	CL
-		-	RW-061-SB-11	1725 ± 2	2	12.14	· · ·	nd, light grayish brown, moist, firm,	
-		-		793 ± 14		ND < 42	high cohesion, high plasticity		СН
-	90	-		267 ± 7		46 ± 13			
-		-		213 ± 7			(13-15) SAND, beige, wet at a	13' bgs, slightly firm, no cohesion, no	SW
15—		-		246 ± 7 474 ± 1(ND <40		grained, orangish brown, wet,	
-		-		474 ± 10 638 ± 12			loose, soft, no plasticity	grained, orangish brown, wet,	SW
-	80			2045 ± 2			(17-18') Sandy CLAY, orangis	h brown moist soft medium	SC
-	00	-	RW-061-SB-19	2279 ± 2			cohesion, high plasticity		
-		-		1832 ± 2		ND -12		sticky, soft, high cohesion, high	СН
20-		-	RW-061-SB-21	718 ± 15		ND <45	plasticity	coarse grained, orange, wet, firm,	sw
-		-		179 ± 7		ND <41	no cohesion, no plasticity	source grained, orange, wet, iiiii,	
-	80	-		292 ± 9		ND <42	(21.5-23.5') CLAY, gray, wet,	hard, high cohesion, high plasticity	СН
-		-		47 ± 4		ND <46	(23 5-28 8') SAND modium to	coarse grained with gravels, with	
25-		-		89 ± 4			trace clay, beige, wet, soft, no		
20-		-		78 ± 4		41 ± 13			SM
-		-		188 ± 7		ND <42			SIVI
-	80	-		334 ± 9		ND <41			
-		-	RW-061-SB-29	1217 ± 1		ND <46	(28 8-35') CLAV arow wat he	ard, high cohesion, high plasticity	
30 —		-		917 ± 15			120.0 00 / OLAT, ylay, Wel, He	and, myn concolor, myn plasticity	
-		-		190 ± 7		ND <42			
-	100	-		172 ± 7 308 ± 9		70 ± 14 ND <44			СН
-	100		RW-061-SB-34	308 ± 9 521 ± 12		ND <44 ND <44			
-		_	1.10-001-00-04	338 ± 9		ND <44 ND <43			
35 —		_		000 ± 9					

E	Boring	Eartl	M Group h Resource Eng and Consultan RW-062-S (page 1 c	gineers ts B	A F S A C C	Client ARM Project No. Project Description Site Location ARM Representativ Checked by Drilling Company Driller Drilling Equipment	: EnviroAnalytics Group : 150298M-11-3 : Sparrows Point - Parcel A3 : Sparrows Point, MD // L. Perrin : W. Mader P.G., CPSS : Green Services, Inc : Kevin Pumphrey : Geoprobe 7822DT	Date : 10/5/2015 Weather : 60s F, sunny Northing (US ft) : 571,999.96 Easting (US ft) : 1,456,334.98	
Depth (ft.)	% Recovery	PID Reading (PPM)	Sample No/Interval	XRF Zn (PPM)		XRF Cd (PPM)	DE	ESCRIPTION	USCS
0-		6.8	RW-062-SB-1	871 ± 25	5	ND < 72	(0-1.5') Slag, sand sized, dark	brown, moist, loose, no plasticity	SW
		0.0		702 ± 15	5	ND < 48	(1.5-2.2') SAND, with silt, grav	/ to brown, moist, firm, loose, no	SM
-	80	0.0 0.0	RW-062-SB-3	1762 ± 2 477 ± 11		ND <45 ND <42	cohesion, no plasticity		
		0.0		477 ± 11 123 ± 6		ND <42	cohesion, no plasticity	rown, mottled, dry, very firm, no	SM
5-		0.1		32 ± 4		ND <44	(5-7') Clayey SILT, beige, dry,	hard, low cohesion, low plasticity	CL
-		0.1		48 ± 4		ND <42			
-	100	0.1		30 ± 4		ND < 44	(7-10') Silty CLAY, dark beige cohesion, low plasticity	, gray streaked, dry, hard, high	
-		0.0 0.0	RW-062-SB-10	48 ± 5 43 ± 4		ND <46 54 ± 15	·····, ···· p·····,		CL
10-		0.0	1002-00-10	43 ± 4 33 ± 4		ND <44	(10-14.3') CLAY, gray, orange	e streaked, dry, firm, medium cohesion,	
-		0.0		44 ± 4		ND <41	medium plasticity		
	100	0.0		45 ± 4		ND <41			CL
		0.0		196 ± 7	•	ND <42			
15—		0.1	RW-062-SB-15	364 ± 9)	ND <41	(14.3-15') Clayey SAND, dark	gray, wet	SC
-		-		85 ± 5		ND <41		t 15' bgs, soft, no cohesion, no	-
-		-		84 ± 4		39 ± 13	plasticity		SM
-	100	-		149 ± 6		ND <37			
-		-	RW-062-SB-20	436 ± 8 1107 ± 1		ND <39 85 ± 14			
20-		-	11002-30-20	1107 ± 1 313 ± 8		85 ± 14 ND <39	(19.3-20.3') Clayey SAND, da	rk gray, wet, low cohesion, low	sc
		-	RW-062-SB-22	816 ± 13		ND <40	<u>v</u> ,	y, wet, soft, high cohesion, high	-/ сн
	95	-		484 ± 11		ND <41	plasticity		-
		-		59 ± 4		ND <41	(22.3-24.5') CLAY, dark gray, plasticity	wet, sticky, high cohesion, high	СН
25-		-		82 ± 5		ND <45	(24-26') SAND, gray, wet, soft	, no cohesion, no plasticity	SМ
20		-		22 ± 3		ND <40		· · · · · ·	
]		-		13 ± 3		43 ± 13		coarse grained, beige, wet, soft, no	0.47
	80	-		30 ± 3		ND <39	cohesion, no plasticity		SW
-		-		42 ± 6		ND <40		coarse grained, beige with red staining,	sw
30-		-	RW-062-SB-30	198 ± 7 309 ± 8		ND <44 ND <41	loose, no cohesion, no plastic		
-		-	RW-062-SB-32	309 ± 8 937 ± 15		50 ±14	(30-32) SAND, fine to mediun cohesion, no plasticity	n grained, grayish beige, wet, soft, no	SW
-	80	-		792 ± 15		ND <45		, very hard, high cohesion, high	
		-		351 ± 9		ND <42	plasticity		СН
		-		50 ± 5		ND <50			
35-		epth: 35'							

E	Boring	Eart	M Group h Resource En and Consultan RW-063-S (page 1 d	gineers tts B	AF Pr Si AF Cł Dr	ient RM Project No. roject Description te Location RM Representative hecked by rilling Company riller rilling Equipment	: EnviroAnalytics Group : 150298M-10-3 : Sparrows Point - Parcel A3 : Sparrows Point, MD : L. Perrin : W. Mader P.G., CPSS : Green Services, Inc : Don Marchese : Geoprobe 7822DT	Date : 10/6/2015 Weather : 70s F, sunny Northing (US ft) : 572,430.34 Easting (US ft) : 1,456,824.20		
Depth (ft.)	% Recovery	PID Reading (PPM)	Sample No/Interval	XRF Zn (PPM)		ZRF Cd (PPM)	DE	ESCRIPTION	USCS	
0-		_	RW-063-SB-1	2352 ± 3	0	1 133±16 1	(0-0.25') Topsoil, with clay and		<u>IML</u>	
-							(0.25-2.75') Clayey SAND, brown, dry, firm, no cohesion, no plasticit			
-		0.0		1052 ± 1	8	ND <45			SM/ SC	
	90	1.2		1599 ± 2	6	120 ± 17	(2,75-5') Sandy CLAY, black.	dry, firm, low cohesion, low plasticity,	<u> </u>	
	5.5 4748 ±						petroleum odor	,,,,,,, ,	CL	
		10.3	RW-063-SB-5	5251 ± 5	5	155 ± 18				
5-	10.3 RW-063-SB-5 5251 :						NA (5-6.5') CLAY, with trace sand, black, dry, firm, medium cohesion, medium plasticity			
		-		3626 ± 3	8	846 ± 19 (6.5-8') CLAY, with trace sand, black, moist, very soft, medium				
-	60	0.1	RW-063-SB-8	8240 ± 6	7		cohesion, high plasticity, wet a		Сн	
-		-		3059 ± 3	3	127 ± 15	(8-10') SAND, beige, wet, soft	, no cohesion, no plasticity		
-									SM	
10-		-		1562 ± 2	1	ND <41				
		-		1890 ± 2	7	ND <49	olasticity	y streaked, wet, soft, no cohesion, no	SW CL	
		-		986 ± 17	7	ND <46	blasticity	soft, medium cohesion, medium		
	100	-	RW-063-SB-13	1940 ± 2	5		(11.2-14') Sandy CLAY, gray v cohesion, low plasticity	with orange streaks, wet, soft, low	CL	
]		-		1351 ± 2	0	62 ± 15				
		-		732 ± 15	5		(14-15') SAND, fine to mediun cohesion, no plasticity	n grained, orange, wet, soft, no	sw	
15-		-		NA		NA	(15-16') CLAY, light gray, mois	st, soft, high cohesion, high plasticity	СН	
		-		NA		NA	(16-20') SILT, beige, with iron	staining, soft, no cohesion, no plasticity		
	40	-		NA		NA				
		-	RW-063-SB-19	864 ± 17	7	ND <48			ML	
1		-		304 ± 9)	ND <44				
20 –		1	ı						J	

20 . NA NA NA S4 ± 15 (20-23') CLAY, light brownish red, wet, very sticky, soft, high CI 60 . 319 ± 9 54 ± 15 (23-23.5') SAND, fine to medium grained, gray, wet, soft, no SV 25 . RW-063-SB-25 729 ± 13 55 ± 13 (23-23.5') SAND, fine to medium grained, gray, wet, soft, no SV 25 . RW-063-SB-25 729 ± 13 55 ± 13 (23-5-30') CLAY, gray, wet, soft, sticky, high cohesion, high plasticity SV 40 . NA NA NA (23-5-30') CLAY, gray, wet, soft, sticky, high cohesion, high plasticity (23-5-30') CLAY, gray, wet, soft, sticky, high cohesion, high plasticity 30 . RW-063-SB-30 861 ± 17 58 ± 16 (30-34.5') Clayey SAND, light gray, wet, soft, slight cohesion, no 30 100 100 		Boring	Eart	M Group h Resource En and Consultar RW-063-S (page 2	gineers ats B	AF Pro Sit AF Ch Dri Dri	ient RM Project No. roject Description te Location RM Representativ hecked by rilling Company riller rilling Equipment	: EnviroAnalytics Group : 150298M-10-3 : Sparrows Point - Parcel A3 : Sparrows Point, MD e : L. Perrin : W. Mader P.G., CPSS : Green Services, Inc : Don Marchese : Geoprobe 7822DT	Date Weather Northing (US ft) Easting (US ft)	: 10/6/2015 : 70s F, sunny : 572,430.34 : 1,456,824.20	
- NA NA NA (20-23) CLAY, light brownish red, wet, very sticky, soft, high 60 - 326 ± 9 53 ± 15 (23-23.5) SAND, fine to medium grained, gray, wet, soft, no Sticky, high cohesion, high plasticity 25 - RW-063-SB-25 729 ± 13 55 ± 13 (23-530) CLAY, gray, wet, soft, sticky, high cohesion, high plasticity Sticky, high cohesion, high plasticity 40 - NA NA NA CLAY, gray, wet, soft, sticky, high cohesion, high plasticity CL 30 - RW-063-SB-30 861 ± 17 58 ± 16 (30-34.5) Clayey SAND, light gray, wet, soft, slight cohesion, no CL 30 - RW-063-SB-34 2238 ± 27 49 ± 15 (30-34.5) Clayey SAND, light gray, wet, soft, slight cohesion, no Sticity, orange streaks at 32.5' 30 - 1121 ± 17 ND <44		% Recovery	PID Reading (PPM)	Sample No/Interval	XRF Zn (PPM)		ZRF Cd (PPM)	DE	ESCRIPTION		nscs
- - 319 ± 9 54 ± 15 - CI 60 - - 326 ± 9 53 ± 15 - C3-23.5') SAND, fine to medium grained, gray, wet, soft, no cohesion, no plasticity SN 25 - - RW-063-SB-25 729 ± 13 55 ± 13 (C3-23.5') SAND, fine to medium grained, gray, wet, soft, no cohesion, no plasticity SN 25 - - NA NA NA CI 40 - NA NA NA CI 40 - NA NA NA CI 30 - RW-063-SB-30 861 ± 17 58 ± 16 CI CI 30 - 1362 ± 20 71 ± 15 CI CI CI 100 - 1121 ± 17 ND <44	20-		-		NA		NA		red, wet, very sticky	, soft, high	
25 . . 242 ± 7 59 ± 13 (23-23.5) SAND, fine to medium grained, gray, wet, soft, no cohesion, no plasticity SV 25 . . RW-063-SB-25 729 ± 13 55 ± 13 . </td <td></td> <td></td> <td>-</td> <td></td> <td>319 ± 9</td> <td>9</td> <td>54 ± 15</td> <td></td> <td></td> <td></td> <td>СН</td>			-		319 ± 9	9	54 ± 15				СН
25 . RW-063-SB-26 729 ± 13 55 ± 13 (23.5-30') CLAY, gray, wet, soft, sticky, high cohesion, high plasticity 40 . NA NA NA 40 . NA NA 40 . . . 40 . . . 40 . . . 40 . . . 40 . . . 40 . . . 40 . . . 40 . . . 40 . . . 417 ± 11 . ND <46		60	-		326 ± 9	9	53 ± 15				
25 - RW-063-SB-25 729 ± 13 55 ± 13 - - CI 40 - NA NA NA - - CI 40 - NA NA NA - - CI 30 - 417 ± 11 ND <46			-		242 ± 7	,	59 ± 13	cohesion, no plasticity			SW
40 - NA NA NA A 40 - NA NA NA CI 40 - NA NA NA CI 40 - AIT ± 11 ND <46	25-		-	RW-063-SB-25	729 ± 13	3	55 ± 13	(23.5-30') CLAY, gray, wet, so	ft, sticky, high cohes	sion, high plasticity	
40 - NA NA NA 30 - RW-063-SB-30 861 ± 17 58 ± 16 - 1362 ± 20 71 ± 15 (30-34.5) Clayey SAND, light gray, wet, soft, slight cohesion, no 100 - 1794 ± 23 ND <44			-		NA		NA				
30 - 417 ± 11 ND <46			-		NA		NA				СН
30 - RW-063-SB-30 861 ± 17 58 ± 16 (30-34.5) Clayey SAND, light gray, wet, soft, slight cohesion, no - 1362 ± 20 71 ± 15 (30-34.5) Clayey SAND, light gray, wet, soft, slight cohesion, no plasticity, orange streaks at 32.5' 100 - 1121 ± 17 ND <44		40	-		NA		NA				
30 - 1362 ± 20 71 ± 15 (30-34.5') Clayey SAND, light gray, wet, soft, slight cohesion, no - 1794 ± 23 ND <44			-		417 ± 11	1	ND <46				
- - <td>30-</td> <td></td> <td>-</td> <td>RW-063-SB-30</td> <td>861 ± 17</td> <td>7</td> <td>-</td> <td>(30-34 5') Clavey SAND light</td> <td>aray wet soft sligh</td> <td>t cohesion no</td> <td></td>	30-		-	RW-063-SB-30	861 ± 17	7	-	(30-34 5') Clavey SAND light	aray wet soft sligh	t cohesion no	
100 - 1121 ± 17 ND <44			-								
100 - 1121±17 ND <44	-		-								SC
- 1708 ± 24 ND <47 35 - (34.5-35') Sandy CLAY, light gray, wet, soft, medium cohesion, low plasticity End of Borehole	-	100	-								
35 (34.5-35') Sandy CLAY, light gray, wet, soft, medium cohesion, low Classicity End of Borehole	-		-	RW-063-SB-34							
	35-		-		1708 ± 2	24	ND <47	plasticity	gray, wet, soft, medi	um cohesion, low	CL
								End of Borehole			
			ooth: OF!	hao							
	I otal Bo	orenole De	eptn: 35'	ogs.							

E	Boring	Eartl	M Group h Resource En and Consultar RW-064-S (page 1	gineers nts	A P S A C D D	lient RM Project No. roject Description ite Location RM Representation hecked by rilling Company riller rilling Equipment	: Sparrows Point, MD	Date : 10/6/2015 Weather : 70s F, sunny Northing (US ft) : 572,308.69 Easting (US ft) : 1,456,709.82	
Depth (ft.)	% Recovery	PID Reading (PPM)	Sample No/Interval	XRF Zn (PPM)	(XRF Cd (PPM)	DE	ESCRIPTION	nscs
0	80	- 1.3 0.8 0.8 2.2	RW-064-SB-1 RW-064-SB-5	NA 350 ± 22 128 ± 13 79 ± 7 775 ± 19	3	NA ND <103 ND <88 ND <57 ND <56		t, medium cohesion, medium plasticity ravel size with pieces of metal, black, ity, slight petroleum odor	CL GM
- - - - 10-	60	- 0.0 0.1 0.2	RW-064-SB-8	NA 1633 ± 2 15808 ± 1 2875 ± 6 1915 ± 2 23047 ± 2	97 2 6	NA ND <55 ND <74 ND <87 73 ± 16 529 ± 21	no cohesion, no plasticity	to gravel sized, black, moist, loose, hard, I sized, brown to black, moist, wet at	GM
- - - 15-	96	0.0 0.0 - -	RW-064-SB-12	23047 ± 21 55397 ± 52 49559 ± 42 55426 ± 52 41217 ± 32 2095 ± 22	534 1087 ± 28 434 882 ± 24 526 859 ± 26 327 845 ± 21		(11.2-15') CLAY, with trace sa very soft, medium cohesion, h	and and silt, black to dark brown, wet,	CH
	90	- - -		446 ± 10 131 ± 7 651 ± 14 2059 ± 3	0 4 :5	74 ± 13 113 ± 16 80 ± 16 88 ± 21	(18.5-19.5') Sandy CLAY, gra		SM CL CH
	100		RW-064-SB-21	9281 ± 9 9729 ± 8 9510 ± 7 7647 ± 7 6221 ± 5 NA 852 ± 15	2 8 3 9	482 ± 20 ND <48 83 ± 16 129 ± 17 55 ± 16 NA ND <44		soft, high cohesion, high plasticity d, high cohesion, high plasticity, soft at	СН
	60	-	RW-064-SB-29	852 ± 13 814 ± 15 1533 ± 1 812 ± 14 3717 ± 4	5 7 4	ND <44 ND <45 ND <41 ND <40 ND <48	cohesion, no plasticity (28.5-30') SAND, coarse to my soft	ined with some coarse, gray, wet, no edium grained with depth, beige, wet, ined, brown, wet, soft, no cohesion, no	SP SW SW
	100		RW-064-SB-32	5359 ± 5 4514 ± 4 3193 ± 3 3864 ± 4	2	ND <48 ND <43 47 ± 15 ND <47	plasticity	peige, wet, soft, medium cohesion,	

	Boring	Eart	M Group h Resource En and Consultar RW-065-S (page 1 d	gineers tts B	A P S A C C C	Client ARM Project No. Project Description Site Location ARM Representativ Checked by Drilling Company Driller Drilling Equipment	: Sparrows Point, MD ve : L. Perrin : W. Mader P.G., CPSS Northing (US ft) : 572,229.64 : Green Services, Inc Easting (US ft) : 1,456,574.89 : Kevin Pumphrey				
Depth (ft.)	% Recovery	PID Reading (PPM)	Sample No/Interval	XRF Zn (PPM)		XRF Cd (PPM)	DESCRIPTION				
0-		-	RW-065-SB-1	NA		NA	(0-3.9') Slag, silt to gravel size no plasticity, gray at 3.5'	ed, dark brown, dry, loose, no cohesion,			
_		-		NA		NA	····		GM		
-				131 ± 8	1	ND <58					
-		0.0		22 ± 4		ND <56					
		0.0	RW-065-SB-5	63 ± 5		ND <52	(3.9-6') Silty SAND, orange, m slight petroleum odor	noist, soft, low cohesion, no plasticity,			
5-	┥ │ ├───┤		NA		NA			SM			
-		-		NA	NA		(6-10') SAND, orangish beige,	, wet, loose, no cohesion, no plasticity			
_	40	-		NA		NA					
_		-	RW-065-SB-9	175 ± 8		ND <51			SP		
		-		122 ± 6	i	ND <45					
10-		-		NA		NA	(10-12') Silty SAND, orange, w plasticity	vet at 11' bgs, soft, no cohesion, no	0.14		
-		-		394 ± 12	2	ND <59			SM		
	80	-		716 ± 19	9	ND <66	(12-15') Silty CLAY, gray, with cohesion, medium plasticity	orange mottling, wet, hard, medium			
		-		937 ± 20	C	ND <62			CL		
45		-	RW-065-SB-15	1175 ± 2	3	ND <60					
15—		-		NA		NA	(15-17.5') Clayey SILT, orang plasticity	ish brown, wet, hard, low cohesion, no			
		-		716 ± 18	3	ND <62			ML		
	70	-		647 ± 16	6	ND <60		ish brown, wet, hard, medium	+		
		-	RW-065-SB-19	839 ± 19	9	ND <62	cohesion, medium plasticity		CL		
20-		-		452 ± 14	4	ND <62	(19.2-20') SAND, coarse grair plasticity	ned, orange, wet, soft, no cohesion, no	SP		
									-		

	Boring	Eart	M Group h Resource En and Consultar RW-065-S (page 2	gineers ats B	AF Pro Sit AF Ch Dri Dri	ent RM Project No. oject Description te Location RM Representative necked by illing Company iller illing Equipment	: EnviroAnalytics Group : 150298M-11-3 : Sparrows Point - Parcel A3 : Sparrows Point, MD : L. Perrin : W. Mader P.G., CPSS : Green Services, Inc : Kevin Pumphrey : Geoprobe 7822DT	Date : 10/8/2015 Weather : 70s F, sunny Northing (US ft) : 572,229.64 Easting (US ft) : 1,456,574.89			
Depth (ft.)	% Recovery	PID Reading (PPM)	Sample No/Interval	XRF Zn (PPM)		XRF Cd (PPM)	DE	ESCRIPTION	USCS		
20-		-		644 ± 15	5		(20-22') SAND, medium to coarse grained, orange, wet, loose, no cohesion, no plasticity				
		-		607 ± 15	5	ND <58					
	100	-		2338 ± 3	4		(22-22.7') SAND, coarse grain plasticity	ned, gray, wet, loose, no cohesion, no	SP		
_		-	RW-065-SB-24	6834 ± 74			(22.7-26.3') CLAY, dark gray t high plasticity	to gray, wet, sticky, firm, high cohesion	,		
- 25—	- 5872 ±					ND <67			СН		
20	- RW-065-SB-26 2929 ±				9	ND <59					
		-		1439 ± 2	4		(26.3-27.2') SAND, coarse grained, dark gray, wet, loose, no cohesion, no plasticity				
_	93	-		818 ± 19	9	ND <60	(27.2-28.5') CLAY, dark gray,	wet, firm, high cohesion, high plasticity	′ Сн		
		-		312 ± 12	2	ND <62	(28.5-33.5') SAND, orange, m	edium to very coarse grained, wet, sof	t,		
		-		366 ± 13	3	ND <61	no cohesion, no plasticity				
30 –		-		NA		NA					
		-		509 ± 14	4	ND <60			SW		
	80	-		239 ± 8		ND <51					
-		-		387 ± 13	3	ND <61	(33,5-35') SILT, with trace clay	y, gray, wet, hard, no cohesion, no			
-		-	RW-065-SB-35	1295 ± 2	4		blasticity	,,,, oonoolon, no	ML		
35 —			1			<u> </u>	End of Boring		I		
-											
-											
-											
-											
40 —											
Total Bo	orehole D	epth: 35'	bgs.								

$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	E	ar I	Eartl	M Group h Resource En and Consultan RW-066-S (page 1	gineers tts B	AR Pro Sit AR Ch Dri Dri	ent RM Project No. oject Description e Location RM Representative ecked by illing Company iller illing Equipment	ription : Sparrows Point - Parcel A3 : Sparrows Point, MD sentative : L. Perrin : W. Mader P.G., CPSS Northing (US ft) : 572,128.13 pany : Green Services, Inc : Don Marchese Easting (US ft) : 1,456,718.15				
- RW-066-SB-1 63791 ± 562 632 ± 24 (0-2) SAND, organic material is time to medium grained with silt and clay, wark form, moist SM 5 - 80 0.0 1894 ± 28 ND -51 (2-2) SAND, organic material is time to medium grained with silt and clay, wark form, moist SM 5 - RW-066-SB-5 212 ± 26 95 ± 16 (2-2) SAND, organic material is time to medium grained with silt and clay, wark form, medium cohesion, no plasticity SF 5 - RW-066-SB-5 212 ± 28 95 ± 16 (2-3) SAND, organic material is time to medium grained with silt and clay, wark form, medium cohesion, no plasticity CL 60 0.0 92 ± 18 ND -48 (7.5 - 17) Sandy CLAY, organy cnist, slightly firm, medium cohesion, nigh plasticity CL 100 . RW-066-SB-11 166 ± 4 ND -43 (10-14.5) CLAY, gray, moist, slightly firm, high cohesion, nigh plasticity SW 100 100 	Depth (ft.)	% Recovery	PID Reading (PPM)				XRF Cd (PPM)	DESCRIPTION				
80 0.0 155 ± 7 ND 246 169, Jatk Drivin, India 5 109, Jatk Drivin, India 169, Jatk Drivin, India 54 109, Jatk Drivin, India 55 60 0.0 155 ± 7 ND 248 95 ± 16 66 ± 17 124 ± 28 ND 248 127 ± 258 95 ± 16 124 ± 28 ND 248 125 ± 76 72 ± 78 72 ± 72 72 ± 78 72 ± 72 72 ± 78 72 ± 72 72 ± 72 72 ± 72 72 ± 72 72 ± 72 72 ± 72 72 ± 72 72 ± 72 72 ± 72 72 ± 72 75 ± 75 75 ±	0		-	RW-066-SB-1	63791 ± 5	62			is fine to medium grained with silt and	SM		
0.1 6912 ± 66 95 ± 16 44.5.5 Sandy CLAY, orange, moist, firm, medium cohesion, medium SH 5 0.0 RW-066-SB-5 992 ± 18 ND <48	-							•				
5 0.0 RW-066-SB-6 2126 ± 29 60 ± 17 [4-5.5] Sandy CLAY, ight gray, moist, soft, high cohesion, medium CL 80 0.0 1337 ± 20 ND <48	-	80				-		2-4') SAND, orange, moist, fil	rm, no conesion, no plasticity	SP		
5 . RW-066-SB-6 8937 ± 78 972 ± 17 [plasticity] [cs.75,75] Sandy CLAY, light gray, moist, soft, high cohesion, high plasticity Ch 10 0.0 53 ± 4 NO < 48				RW-066-SB-5				4-5.5') Sandy CLAY, orange,	moist, firm, medium cohesion, medium			
80 0.0 132 ± 10 180 × 45 plasticity plasticity plasticity c c c 10 0.0 100 × 45 66 ± 6 ND <45	5-		-	RW-066-SB-6	8937 ± 7	8		,		_		
10 0.0 53 ± 4 ND <45	_						ND <40		ray, moist, soft, high conesion, high	СН		
10 0.0 66 ± 6 ND <55 Intecluin plasticity CL 10 . RW-066-SB-11 16544 ± 133 99 ± 17 (10-14,5') CLAY, gray, moist, slightly firm, high cohesion, high plasticity CH 100 0.0 151 ± 7 ND <44	-	80				0	(7.5-10') CLAY, gray to light g	ray, moist, very firm, medium cohesion,			
10 . RW-066-SB-11 16544 ± 133 99 ± 17 (10-14.5) CLAY, gray, moist, slightly firm, high cohesion, high plasticity CH 10 0.0 . 15 ± 7 ND <44	-						1	nedium plasticity		CL		
100 0.0 1284 ± 20 47 ± 15 plasticity CH 15 100 0.0 151 ± 7 ND < 44	10-			RW-066-SB-11		33		10-14.5') CLAY, grav, moist,	slightly firm, high cohesion, high			
100 0.0 311 ± 9 52 ± 15 15 150 ± 7 57 ± 15 168 ± 6 ND <42	-		0.0				, in the second s					
15 0.0 150 ± 7 57 ± 15 (14.5-15') SAND, orange, moist, loose, no cohesion, no plasticity SF 100 - 150 ± 6 ND <43	1	100	0.0		151 ± 7		ND <44			СН		
15 - 168 ± 6 ND <42			0.0		311 ± 9		52 ± 15					
20 - 168 ± 6 ND <42	15-		0.0				L (14.5-15') SAND, orange, moi	st, loose, no cohesion, no plasticity	SP		
100 - 53 ± 4 ND <43	-		-				ND <42 (15-18') SAND, fine to mediun	n grained, orangish beige to beige, wet			
20 - 374 ± 10 ND <44	-	100					c	at 15' bgs, soft, no cohesion, r	no plasticity	1300		
20 - RW-066-SB-20 512 ± 11 57 ± 15 cohesion, no plasticity SW 20 - 1862 ± 25 ND <46			-)	_	18-20') SAND, fine to coarse	grained, dark gray, wet, soft, no			
100 - 1862 ± 25 ND <46	20		-	RW-066-SB-20								
100 - 2015 ± 28 ND < 50	207		-		1862 ± 2	5	<u> </u>	, , ,				
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	4		-	RW-066-SB-22					sand, dark gray, wet, firm, high			
$25 - \begin{bmatrix} - & & & & & & & & & & & & & & & & &$	-	100	-				ND <50	onosion, myn plastiolly				
25 - 977 ± 17 70 ± 15 - RW-066-SB-27 3605 ± 40 61 ± 16 80 - 1642 ± 26 ND <41	-		-							СН		
30 - RW-066-SB-27 3605 ± 40 61 ± 16 Image: constraint of the state o	25 -		-									
$30 - \begin{bmatrix} - & 1070 \pm 18 & 92 \pm 16 \\ - & 96 \pm 5 & ND < 45 \\ - & 232 \pm 8 & 80 \pm 15 \\ - & 284 \pm 8 & 63 \pm 14 \\ - & 8W-066-SB-35 & 977 \pm 17 & 70 \pm 15 \end{bmatrix}$ $(27.8-30') SAND, fine to coarse grained, beige, with gray streaks, wet, loose, no cohesion, no plasticity (30-35') SAND, fine to coarse grained, beige, wet, soft, no cohesion, no plasticity (30-35') SAND, fine to coarse grained, beige, wet, soft, no cohesion, no plasticity (30-35') SAND, fine to coarse grained, beige, wet, soft, no cohesion, no plasticity (30-35') SAND, fine to coarse grained, beige, wet, soft, no cohesion, no plasticity (30-35') SAND, fine to coarse grained, beige, wet, soft, no cohesion, no plasticity (30-35') SAND, fine to coarse grained, beige, wet, soft, no cohesion, no plasticity (30-35') SAND, fine to coarse grained, beige, wet, soft, no cohesion, no plasticity (30-35') SAND, fine to coarse grained, beige, wet, soft, no cohesion, no plasticity (30-35') SAND, fine to coarse grained, beige, wet, soft, no cohesion, no plasticity (30-35') SAND, fine to coarse grained, beige, wet, soft, no cohesion, no plasticity (30-35') SAND, fine to coarse grained, beige, wet, soft, no cohesion, no plasticity (30-35') SAND, fine to coarse grained, beige, wet, soft, no cohesion, no plasticity (30-35') SAND, fine to coarse grained, beige, wet, soft, no cohesion, no plasticity (30-35') SAND, fine to coarse grained, beige, wet, soft, no cohesion, no plasticity (30-35') SAND, fine to coarse grained, beige, wet, soft, no cohesion, no plasticity (30-35') SAND, fine to coarse grained, beige, wet, soft, no cohesion, no plasticity (30-35') SAND, fine to coarse grained, beige, wet, soft, no cohesion, no plasticity (30-35') SAND, fine to coarse grained, beige, wet, soft, no cohesion, no plasticity (30-35') SAND, fine to coarse grained, beige, wet, soft, no cohesion, no plasticity (30-35') SAND, fine to coarse grained, beige, wet, soft, no cohesion, no plasticity (30-35') SAND, fine to coarse grained, beige, wet, soft, no cohesion, no plasticity (30-35') SAND, fine to coars$	-		-	RW-066-SB-27								
$30 - \begin{bmatrix} - & 0 & 0 & 1 & 0 & 0 & 1 & 0 & 0 & 1 & 0 & 0$]	80	-		1642 ± 2	6						
30 - 96 ± 5 ND <45]		-		1070 ± 1	8	02 110			sw		
35	30-		-				ND <45	-	-			
60 - 480 ± 10 ND <41	4		-				, in the second s		grained, beige, wet, soft, no cohesion,			
- - 934 ± 16 ND <45	-	60	-				05 ±14			SW		
35 - RW-066-SB-35 977 ± 17 70 ± 15 End of Borehole	-		-									
End of Borehole			-	RW-066-SB-35								
Total Borehole Depth: 35' bgs.	35					l	E	End of Borehole				
i otal Borenole Depth: 35' bgs.				h								
	i otal Bo	orenole De	eptn: 35'	bgs.								

H	Boring	Eartl	M Group h Resource En and Consultar RW-067-S (page 1 d	gineers tts B	Al Pi Si Al Ci Di	lient RM Project No. roject Description ite Location RM Representative hecked by rilling Company riller riller rilling Equipment	: EnviroAnalytics Group : 150298M-11-3 : Sparrows Point - Parcel A3 : Sparrows Point, MD e : L. Perrin : W. Mader P.G., CPSS : Green Services, Inc : Don Marchese : Geoprobe 7822DT	Date : 10/7/2015 Weather : Cloudy Northing (US ft) : 572,220.49 Easting (US ft) : 1,456,678.83	
Depth (ft.)	% Recovery	PID Reading (PPM)	Sample No/Interval	XRF Zn (PPM)		XRF Cd (PPM)	DE	ESCRIPTION	
0	80	- 0.1 0.0 0.0 0.1 -	RW-067-SB-1 RW-067-SB-2	>10% ± 0 14570 ± 1 12964 ± 1 1687 ± 2 236 ± 8 NA 356 ± 10	21 07 3	146 ± 17 ND <49 ND <46 64 ± 15	plasticity (0.3-2.3') Slag, medium sand no cohesion, no plasticity (2.3-3.3') Clayey SAND, brow	noist, soft, medium cohesion, medium to gravel sized, dark brown, dry, loose, n, dry, soft, no cohesion, no plasticity own, moist, soft, high cohesion, high	С Сн
- - 10-	- 356 ± 100 - RW-067-SB-8 303 ± - 237 ± - 290 ±		303 ± 9 237 ± 8 290 ± 9 1859 ± 2		57 ± 15 ND <42 ND <45		, loose, no cohesion, no plasticity d, high cohesion, medium plasticity	SP	
- - - 15—	100	- - -	RW-067-SB-12	2383 ± 3 1996 ± 2 987 ± 17 120 ± 6	6 7	ND <44	cohesion, medium plasticity	and gray, mottled, wet, soft, medium	
-	90		RW-067-SB-19	1542 ± 2 111 ± 6 1064 ± 2 4484 ± 4 3975 ± 4	1	ND <43 ND <43 78 ± 18 49 ± 16	plasticity	, slightly firm, high cohesion, high	SP CH
20	100	-		3373 ± 4 2844 ± 32 2465 ± 3 2263 ± 3 3014 ± 32	3 1 1	ND <47 62 ± 16 ND <49	plasticity (22-22.5') SAND, gray, wet, so	ay, wet, hard, high cohesion, high oft, no cohesion, no plasticity et, sticky, stiff to soft, high cohesion,	CH
- 25 — -	00	- - -	RW-067-SB-25 RW-067-SB-26	2901 ± 3 2585 ± 2 1858 ± 2	4 9	72 ± 16 44 ± 15 54 ± 17	high plasticity		CH/ CL
- - 30-	80	-		98 ± 6 88 ± 6 189 ± 7 367 ± 10		ND <48 ND <41	cohesion, no plasticity	arse grained, beige, wet, loose, no	SW
-	100	- -		2016 ± 2 2332 ± 2 2522 ± 3	7 0	47 ± 15 ND <46	(31.3-34') Sandy CLAY, dark l cohesion, medium plasticity		CL
35—		-	RW-067-SB-35	2545 ± 2	9	53 ± 15	(34-35') CLAY, gray, wet, soft	, high cohesion, high plasticity	СН

E	Boring	Eartl	M Group h Resource En and Consultar RW-068-S (page 1	gineers ats B	A P S A C D D	lient RM Project No. roject Description ite Location RM Representation hecked by rilling Company riller rilling Equipment	: EnviroAnalytics Group : 150298M-11-3 : Sparrows Point - Parcel A3 : Sparrows Point, MD /e : L. Perrin : W. Mader P.G., CPSS : Green Services, Inc : Don Marchese : Geoprobe 7822DT	Date : 10/7/2015 Weather : Cloudy Northing (US ft) : 572,004.42 Easting (US ft) : 1,456,961.18	
Depth (ft.)	% Recovery	PID Reading (PPM)	Sample No:	XRF Zn (PPM)		XRF Cd (PPM)	DE	ESCRIPTION	nscs
0-		-	RW-068-SB-1	NA		NA		l bark, brown, moist, soft, loose, no	/ ML
	00	-		838 ± 34		ND <97	cohesion, no plasticity (0.3-3') Slag, coarse grained t	o gravel sized, dark brown, loose, no	—/GM/ GW
-	60	46.9 0.2		217 ± 10 148 ± 7		66 ± 20 63 ± 17	cohesion, no plasticity		
5-		0.2	RW-068-SB-5	6771 ± 6		127 ± 16	plasticity, petroleum odor, wet	ist, soft, sticky, high cohesion, high t at 5' bgs	СН
		-		NA		NA			
-	00	-	RW-068-SB-7	38406 ± 2		753 ± 21	(5-7') Slag, coarse grained to cohesion, no plasticity	gravel sized, black, wet, loose, no	GM/
-	80	-		2826 ± 3 3095 ± 3		135 ± 16 106 ± 14	(7-10') CLAY, with trace clay,	brown, wet, soft, medium cohesion,	
-		-		11883 ± 9		119 ± 15	medium plasticity		
10-		-		5382 ± 5	5	ND <50		n grained, brown, wet, no cohesion, no	SM
		-	RW-068-SB-17	4064 ± 3		98 ± 14	plasticity	rained brownish arey wat ast no	
-	86	-		2094 ± 2 2093 ± 2		57 ± 14	cohesion, no plasticity	rained, brownish gray, wet, soft, no	SP
-		-		2093 ± 2 3352 ± 3		68 ± 14 43 ± 14	(12.8-15') CLAY, with trace sa medium plasticity	and, gray, wet, soft, medium cohesion,	CL
15—		-		4576 ± 3		ND <31		et, firm, medium cohesion, high	
-		-		4900 ± 3	6	ND <32	plasticity		
-	100	-		3972 ± 3	4	53 ± 12			СН
		-		2814 ± 2	5	61 ± 12			
20-		-		3007 ± 3	0	45 ± 14			
		-		1904 ± 2	4	ND <44	(20-24') CLAY, light gray, wet,	, soft, high cohesion, high plasticity,	
		-	RW-068-SB-26	1776 ± 2	4	49 ± 15	with trace sand at 23'		СН
	100	-		1838 ± 2		ND <44			
		-		977 ± 17		69 ± 15			
25-		-		1712 ± 2		ND <44	(24-25') CLAY, light grayish bi ∖plasticity	rown, wet, soft, high cohesion, high	СН
-		-		466 ± 11	1	51 ± 15	<u>,</u>	, soft, high cohesion, high plasticity	/
-	100	-		75±6		ND <49			СН
-	100			68 ± 5 60 ± 5		62 ± 15 57 ± 14			
-		-		60 ± 3 42 ± 4		57 ± 14 57 ± 14			
30-		-		421 ± 11		ND <45	(30-31') SAND, gray, wet, loos	se, no cohesion, no plasticity	SP
		-	RW-068-SB-32	1060 ± 1		ND <49		, soft, sticky, high cohesion, high	
	100	-		252 ± 9)	ND <49	plasticity		
1		-		73 ± 6		ND <57			СН
35		-		63 ± 5		64 ± 16			
		epth: 35'							

E	Boring	Eartl	M Group h Resource En and Consultar RW-069-S (page 1	gineers ats B		Client ARM Project No. Project Description Site Location ARM Representativ Checked by Drilling Company Driller Drilling Equipment	: EnviroAnalytics Group : 150298M-11-3 : Sparrows Point - Parcel A3 : Sparrows Point, MD e : L. Perrin : W. Mader P.G., CPSS : Green Services, Inc : Don Marchese : Geoprobe 7822DT	Date : 10/7/2015 Weather : 70s F, cloudy Northing (US ft) : 572,031.30 Easting (US ft) : 1,456,874.17	
Depth (ft.)	% Recovery	PID Reading (PPM)	Sample No/Interval	XRF Zn (PPM)		XRF Cd (PPM)	DE	ESCRIPTION	USCS
0-		7.5	RW-069-SB-1	3986 ± 6	65	ND <90	(0-0.4') Topsoil, brown, with ro	oots and some fines and gravel slag,	ML
-		5.5		4609 ± 5	52	73 ± 18		sized with trace clay/silt, dark brown,	
-	100	0.2	RW-069-SB-3	>10% ± 1	%	2553 ± 69	•	n, low cohesion, slight plasticity, wet at	_
-		0.0		7410 ± 7	0	271 ± 18	3.5' bgs - perched		SC
-		0.0		781 ± 15	5	ND <46	(3.7-8') Sandy CLAY, light bro cohesion, medium plasticity	own to beige, wet, soft, medium	
5-		-		NA		NA			
-		-		647 ± 14	4	ND <47			CL
-	80	-		431 ± 11		ND <45			
-	00	_		329 ± 9		54 ± 14		peige, wet, soft, no cohesion, no	SM
-		-					plasticity (9-10.5') Sandy CLAY, gray, w	vet, firm, high cohesion, high plasticity	
10-		-	RW-069-SB-10	743 ± 15		62 ± 16			СН
-		-		833 ± 16		ND <47	(10.5-11.8') CLAY, light gray,	dry, soft, high cohesion, high plasticity	СН
-		-	RW-069-SB-12	1015 ± 1	8	ND <48	(11.8-16') Silty CLAY, light gra	ay, dry, firm, medium cohesion, low	+
	90	-		638 ± 14	4	ND <46	plasticity, wet at 15' bgs		
		-		120 ± 6	6	ND <44			CL
15—		-		201 ± 8	3	ND <47			
		-		220 ± 9)	ND <50			
]		-		285 ± 8	3	ND <40	(16-18.7') SAND, orange, wet	, loose, no cohesion, no plasticity	
]	80	-		476 ± 12	2	ND <46			SP
		-		408 ± 10	0	ND <44			
1		-	RW-069-SB-20	867 ± 16	6	ND <45	(18.7-20) SAND, gray, wet, lo	ose, no cohesion, no plasticity	SP
20-	orehole D	opth: 35'	has			· L			

	Boring	Earth	M Group h Resource En and Consultar RW-069-S (page 2	gineers ats B	A P S A C C	Client ARM Project No. Project Description Site Location ARM Representative Checked by Drilling Company Driller Drilling Equipment	: EnviroAnalytics Group : 150298M-11-3 : Sparrows Point - Parcel A3 : Sparrows Point, MD e : L. Perrin : W. Mader P.G., CPSS : Green Services, Inc : Don Marchese : Geoprobe 7822DT	Weather : 70 Northing (US ft) : 57	/7/2015 s F, cloudy 2,031.30 456,874.17		
Depth (ft.)	% Recovery	PID Reading (PPM)	Sample No/Interval	XRF Zn (PPM)		XRF Cd (PPM)	DE	ESCRIPTION		USCS	
20-		-		1925 ± 2 2553 ± 2			(20-22') Sandy CLAY, gray, wet, slightly firm, high cohesion, high plasticity				
-	90 - RW-069-SB-23 3157 - 2235					-46 ± 15	(22-25') CLAY, gray, wet, firm, high cohesion, high plasticity		icity	СН	
-	- 842 ±					49 ± 15 ND <51					
25-					9	ND <42	 (25-26') SAND, with trace clay, grayish brown, wet, loose, no cohesion, no plasticity (26-29.5') CLAY, gray, wet, firm, high cohesion, high plasticity 				
-	100	-	RW-069-SB-28	2458 ± 3 2696 ± 3		49 ± 16 69 ± 16	(20-29.5) CLAY, gray, wet, fir	m, nign conesion, nign pla	ISTICITY		
-		-		1501 ± 2	25	ND <53				СН	
30-		-		771 ± 17			(29.5-30') SAND, medium gra plasticity	ined, gray, wet, soft, no co	bhesion, no	SP	
_		-		345 ± 9 1178 ± 1		ND <40	(30-34.5') SAND, medium to c no cohesion, no plasticity	oarse grained, beige to gr	ay, wet, soft,		
_	80	-		1117 ± 1	7	ND <42				SW	
-		-		2695 ± 3		ND <46					
35—		-	RW-069-SB-35	6150 ± 6	50		(34.5-35') Sandy CLAY, gray, End of Boring	wet, soft, low cohesion, lo	w plasticity	CL	
- - 40 Total Bo	prehole D	epth: 35'	bgs.								

	ARM Group Inc. Earth Resource Engineers and Consultants Boring ID: RW-006-SB RW-070-SB (page 1 of 2)		ARM Group Inc. Earth Resource Engineers and Consultants ARM I Project Site Li ARM I Check Drillen Drillen Drillen Drillen Drillen		Client ARM Project I Project Descri Site Location ARM Represe Checked by Drilling Compa Driller Drilling Equipr	iption : Sparrows Point - Parcel A3 : Sparrows Point, MD entative : L. Perrin : W. Mader P.G., CPSS Northing (US ft) : 572,073.37; 572,0' any : Green Services, Inc : Kevin Pumphrey		
Depth (ft.)	% Recovery	PID Reading (PPM)	Sample No/Interval	XRF Zn (PPM)	XRF Cd (PPM)	DESCRIPTION	nscs	
0-		-	RW-070-SB-1	8775 ± 119	ND <75	(0-0.7') Topsoil, brown, with plant detritis, dry, loose, soft, no cohesion, no plasticity, few slag gravels at 0.33'	ML	
-		16.3		68 ± 6	ND <55	(0.7-2.16') Slag, coarse grained to gravel sized, brown, dry, loose, no cohesion, no plasticity	GW	
_	100	10.2	RW-070-SB-3	1198 ± 37	ND <91	(2.16-2.66') Slag, coarse grained to gravel sized, light gray, dry, loose, no cohesion, no plasticity	GM SM	
		4.9		50 ± 5	ND <49	(2.66-3.66') SAND, fine grained with silt, brown, dry, soft, loose, no cohesion, no plasticity		
5-		5.8		691 ± 17	ND <55	(3.66-5') CLAY with wood debris brown moist soft high cohesion		
		-		1423 ± 20	100 ± 15	(5-7.5') Sandy CLAY, gravish brown, wet, firm, high cohesion, high		
_		-	RW-070-SB-7	8228 ± 59	158 ± 13		СН	
_	90	-		1491 ± 20	65 ± 14	(7.5-11') CLAY, with trace sand, light gray, wet, soft, medium		
_		-		1950 ± 23	ND <42	cohesion, medium plasticity		
10-		-		1537 ± 21	ND <44		CL-CH	
_		-		421 ± 11	ND <46			
_		-		374 ± 10	ND <42	(11-14.16') CLAY, with trace sand, light gray, wet, firm, high cohesion, high plasticity, less firm at 13.16'		
-	80	-		1085 ± 16	58 ± 13		СН	
_		-		553 ± 13	ND <47			
15-		-	RW-070-SB-15	1423 ± 20	100 ± 15	(14.16-17') SAND, coarse grained, light gray, soft, wet, no cohesion, no plasticity		
-		-		71 ± 5	ND <41		SW	
-		-		61 ± 4	62 ± 14			
_	83	-		66 ± 4	ND <39	(17-20') SAND, medium to coarse grained, orange, wet, soft, no cohesion, no plasticity		
_		-		231 ± 8	ND <42		SW	
20-		-	RW-070-SB-20	291 ± 9	ND <44			
	l orehole D	epth: 35'	bgs					

0-10ft. - based on RW-006-SB drilling

10-25ft. - based on RW-070-SB drilling

ARM Group Inc. Earth Resource Engineers and Consultants Boring ID: RW-006-SB RW-070-SB		ARM Project No.: 150298M-10-3Project Description: Sparrows Point - Parcel A3Site Location: Sparrows Point, MDARM Representative: L. PerrinChecked by: W. Mader P.G., CPSS		Date Weather Northing (US ft) Easting (US ft)	: 10/8/2015 : Sunny, 70s F : 572,073.37; 572,0 : 1,457,082.23; 1,45				
			(page 2	of 2)					1
Depth (ft.)	% Recovery	PID Reading (PPM)	Sample No/Interval	XRF Zn (PPM)	XRF Cd (PPM)	DESC	CRIPTION		NSCS
20-		-		1472 ± 20	ND <43	(20-25') CLAY, with trace sand, gr plasticity	ay, wet, soft, high col	hesion, high	
-		-	RW-070-SB-22	1497 ± 20	54 ± 14				
-	100	-		210 ± 8	57 ± 15				сн
-		-		100 ± 6	56 ± 15				
-		-		61 ± 6	61 ± 18				
25—		-		NA	NA	(25-28') CLAY, gray, wet, very sof	t, high cohesion, high	plasticity	
		-	RW-070-SB-27	180 ± 7	ND <41				СН
	60	-		64 ± 5	ND <44				
		-		48 ± 5	ND <48	(28-29') SAND, coarse grained, lig plasticity			SW
30-		-		131 ± 7	ND <47	(29-35') CLAY, gray, wet, soft, hig	h cohesion, high plas	ticity	
		-		106 ± 5	ND <42				
-		-	RW-070-SB-32	104 ± 6	74 ± 15				СН
-	100	-		73 ± 5	ND <46				
-		-		74 ± 5	62 ± 16				
35-		-		52 ± 5	64 ± 16	End of Boring			
- - - 40-						-			
-	orehole De	epth: 35'	bgs						
	0-10ft based on RW-006-SB drilling 10-25ft based on RW-070-SB drilling								

APPENDIX C



NG, INC. P P P P P P P P P P P P P P P P P TRIAD Listens, Designs & Delivers

December 4, 2015

Mr. James Calenda EnviroAnalytis Group, LLC 1650 Des Peres Road, Suite 303 St. Louis, MO 63131

Re: Sparrows Point Piezometer Survey Sparrows Point, MD Triad Engineering Job No. 03-15-0343

Mr. Calenda:

Below are the specified surveyed piezometers, date of last field work completed on November 24, 2015. The coordinate values shown were derived from G.P.S. observations based on National Geodetic Surveys stations "GIS 1", PID AC7684 and "GIS 2", PID AC7685 which purport to be on NAD83(2011) Maryland Grid coordinate system and NAVD88 elevations.

DESCRIPTION	NORTHING	EASTING	TOP CASING ELEVATION	GROUND AT PIEZOMETER ELEVATION
A2-013-PZ	574018.74	1463788.08	16.17	12.38
A2-022-PZ	572911.38	1463476.53	12.58	9.68
A2-025-PZ	573614.75	1464570.56	11.23	8.51
A2-031-PZ	574485.04	1464939.09	22.88	20.78
A4-001-PZ	571114.57	1458067.91	14.71	12.71
A4-005-PZ	571746.11	1458066.66	15.95	12.94
A4-005a-PZ	571748.15	1458062.51	15.55	12.99
A4-007-PZ	572370.58	1457965.85	15.41	12.88
A4-010-PZ	572631.43	1458703.03	14.67	12.79
A4-012-PZ	570367.73	1458232.61	15.90	12.24
A4-013-PZ	570657.51	1458543.60	12.00	9.76
A4-014-PZ	571109.86	1459218.50	15.39	11.49
A4-019-PZ	571962.55	1458881.91	16.34	12.65
A8-002-PZ	573593.69	1461765.45	16.14	13.21
A8-004-PZ	573652.14	1462090.63	16.73	12.85
A8-007-PZ	573458.80	1462039.43	15.86	12.60
A8-009-PZ	573912.57	1461846.67	16.73	12.81
A8-013-PZ	574444.07	1462162.14	20.01	16.10
A8-015-PZ	574293.04	1461458.35	16.18	11.91
A8-017-PZ	572956.53	1461959.46	16.59	13.26
A8-017a-PZ	572957.82	1461960.12	15.44	13.26



FFF FFF FFF FFF FFF FFF FF FF

April 1, 2016

Mr. James Calenda EnviroAnalytis Group, LLC 1650 Des Peres Road, Suite 303 St. Louis, MO 63131

Re: Sparrows Point Well Survey Sparrows Point, MD Triad Engineering Job No. 03-15-0343

Mr. Calenda:

Below are the specified surveyed wells, date of last field work completed on March 31, 2016. The coordinate values shown were derived from G.P.S. observations based on National Geodetic Surveys stations "GIS 1", PID AC7684 and "GIS 2", PID AC7685 which purport to be on NAD83(2011) Maryland Grid coordinate system with NAVD88 (AMSL) elevations.

DESCRIPTION	NORTHING	EASTING	TOP CASING ELEVATION	GROUND AT WELL ELEVATION
RW01-PZM020	572285.02	1456497.40	12.72	10.15
RW02-PZM000	572167.62	1456601.84	12.39	10.05
RW02-PZM020	572158.64	1456606.28	13.02	10.27
RW03-PZM003	572259.59	1456590.24	10.87	10.31
RW04-PZM003	572273.38	1456415.50	11.11	10.27
RW05-PZP001	572192.49	1456509.88	13.03	10.76
RW06-PZM001	572173.11	1456427.80	12.17	10.20
RW07-PZM004	572145.46	1456308.46	13.70	10.61
RW07-PZM017	572137.29	1456311.82	12.94	10.71
RW08-PZM003	572100.62	1456449.49	11.38	10.76
RW09-PZM004	572065.65	1456324.72	13.67	10.76
RW10-PZM004	572028.98	1456365.53	10.92	11.22
RW10-PZM020	572016.81	1456385.68	11.86	11.47
RW10-PZM065	572031.12	1456376.20	10.75	10.98
RW11-PZM004	572016.05	1456486.05	13.79	11.11
RW12-PZM004	572051.83	1456593.90	13.88	11.16
RW13-PZM020	571971.43	1456592.59	13.05	11.17
RW14-PZM020	572204.47	1456202.53	13.60	11.24
RW15-PZM020	571989.55	1456088.94	12.17	11.84
RW16-PZM020	571861.44	1456127.25	13.89	11.65
RW17-PZM019	571801.70	1456321.19	13.73	11.43
RW18-PZM047	572418.32	1456080.56	15.69	13.70

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RW19-PZM020	571975.38	1455960.61	13.53	11.28
RW19-PZM050	571973.56	1455966.33	12.95	11.17
RW19-PZP003	571981.70	1455964.46	13.49	11.16
RW20-PZM020	571694.60	1456021.05	13.03	11.14
RW20-PZM050	571704.36	1456022.96	11.87	11.09
RW20-PZP000	571705.48	1456018.60	13.54	11.06
RW21-PZM023	571512.69	1456045.20	12.93	10.86
RW-RW89	572109.51	1456513.71	11.35	10.97
RW-RW90	572154.39	1456467.19	11.08	10.55
RW-RW93		N	OT INSTALLED	
RW-RW95	572243.17	1456479.97	12.62	10.81
RW-RW97	572070.55	1456523.86	13.08	10.93
RW-RWBW-20	WELL CASING I	DAMAGED, COULD NO	DT SURVEY (SEE FIGURE 1.0)	14.04
RW-RWBW-21	572425.20	1456092.04	15.11	14.75
SW03-PZM003	571205.39	1456735.24	14.54	10.93
SW03-PZM060	571201.38	1456738.70	14.93	10.92
TS04-PDM004	571781.18	1456010.86	13.69	11.10
TS04-PPM007	571713.99	1455885.63	10.20	10.24
TS04-PZM023	571723.19	1455884.69	10.05	10.30
SW-061-MWS	567005.21	1457693.91	15.83	13.65
SW-059-MWS	567199.64	1458459.63	15.99	13.64
SW-060-MWS	567889.61	1457693.79	14.12	12.20
SW-051-MWS	565671.75	1462655.02	13.40	10.99
SW-049-MWS	566666.92	1463263.78	11.55	11.89
SW-050-MWS	565719.62	1463489.52	10.62	8.04
SW-066-MWS	564235.89	1458826.45	13.02	10.77
SW-071-MWS	564957.19	1460809.42	16.63	14.25
SW-072-MWS	564563.01	1460661.22	14.60	12.02
SW-073-MWS	564422.72	1461025.48	14.76	12.43
SW-065-MWS	564008.99	1457839.54	12.27	12.57
SW-057-MWS	567666.75	1460456.19	12.31	12.62
SW-058-MWS	568148.01	1459749.57	11.45	11.75
SW-056-MWS	566048.47	1460677.32	11.52	8.72
SW-054-MWS	566520.20	1461893.20	13.35	10.89
SW-055-MWS	565946.68	1461317.07	11.87	9.28
SW-053-MWS	567410.98	1461986.20	13.84	14.06
SW-037-MWS	563571.81	1461007.95	13.28	10.96
SW-035-MWS	563772.91	1460297.91	13.43	11.06
SW-034-MWS	563668.32	1459941.32	12.62	10.16
SW-032-MWS	563537.58	1458639.17	12.64	10.49
SW-027-MWS	564973.53	1456177.11	16.98	14.33
SW-028-MWS	564518.61	1456324.45	15.59	13.20

	Г		T	
SW-021-MWS	568534.52	1457422.96	12.83	10.42
SW-022-MWS	568222.29	1457122.05	14.31	12.20
SW-023-MWS	568116.87	1456637.37	14.66	12.79
SW-024-MWS	568021.88	1456157.41	14.03	11.62
SW-025-MWS	566943.92	1456126.02	13.16	11.03
SW-026-MWS	566649.66	1455514.08	11.51	8.61
SW-040-MWS	564306.40	1463005.67	13.01	11.16
SW-041-MWS	564416.60	1463773.99	13.47	11.80
SW-042-MWS	564740.08	1464633.24	7.40	7.78
SW-043-MWS	565729.24	1464430.00	10.26	8.53
SW-044-MWS	566398.36	1464363.35	8.61	8.99
SW-048-MWS	568760.44	1463140.98	16.73	14.27
SW-046-MWS	569504.23	1464948.41	9.80	10.13
SW-047-MWS	570242.63	1464394.66	20.24	20.56
SW-038-MWS	563432.87	1461357.62	16.28	13.76
SW-039-MWS	563507.65	1462484.16	19.91	17.91
SW-031-MWS	563598.44	1458394.82	13.41	10.93
SW-070-MWS	565612.92	1459619.82	11.17	9.10
SW-052-MWS	565095.06	1462682.05	13.88	11.49
SW-045-MWS	568357.88	1463927.89	13.10	11.17
SW-043-MWI	565719.77	1464429.47	10.43	8.56
SW-045-MWI	568344.09	1463932.84	12.86	10.92
SW-074-MWI	567047.75	1464301.55	10.20	8.20
SW-036-MWS	563678.17	1460774.35	13.38	10.82
SW-033-MWS	563597.45	1459274.61	10.28	10.59
SW-030-MWS	563547.95	1458146.61	14.72	12.32
SW-074-MWS	567038.13	1464298.66	11.32	8.79
SW-062-MWS	567420.73	1456909.57	16.81	14.39
SW-063-MWS	565322.90	1456892.20	19.98	17.54
SW-067-MWS	564917.48	1458453.61	14.85	12.66
SW-068-MWS	565823.84	1458036.16	16.87	14.55
SW-069-MWS	566309.02	1458770.00	16.56	14.23
SW-029-MWS	563980.59	1456323.19	15.75	13.15
SW-064-MWS	564322.36	1457393.54	17.39	15.15
FM01-PZM003	568251.65	1460279.28	10.08	10.37
FM01-PZM041	568251.76	1460275.61	9.91	10.24
FM05-PZM004	568565.69	1462040.51	14.48	11.73
FM05-PZM024	568578.67	1462043.77	14.47	12.04
SG07-PZM007			IOT INSTALLED	1
SW06-PZM001	569184.69	1463625.88	17.29	14.92
SW06-PZM053	569188.45	1463637.32	16.75	14.59
SW07-PZM004	567658.52	1456050.21	14.52	12.02

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SW07-PZM108	567665.11	1456048.67	15.76	11.56
SW08-PZM003	568091.75	1458990.33	11.75	9.37
SW08-PZM053	568090.03	1458982.75	12.02	9.67
SW09-PZM004	566974.91	1460293.50	13.16	10.34
SW09-PZM028	566965.08	1460295.30	12.70	10.48
SW09-PZM068	566970.72	1460290.93	13.31	10.32
NO DESC.	566975.78	1460287.86	13.03	10.17
SW10-PZM012	567312.59	1463288.23	7.91	4.82
SW10-PZM085	567286.63	1463311.33	7.83	4.88
SW11-PZM005	565794.79	1456073.98	13.54	11.35
SW12-PZP001	565989.17	1457438.18	17.66	15.57
SW13-PZM003	563493.91	1456407.34	16.26	14.01
SW13-PZM025	563498.66	1456410.45	15.59	13.56
SW13-PZM111	563502.75	1456409.98	15.37	13.66
SW14-PZM004	563392.23	1457680.38	15.85	13.80
SW15-PZM005	564367.29	1459534.16	14.83	12.17
SW15-PZM031	564371.72	1459531.84	14.90	12.02
SW15-PZM085	564367.22	1459539.25	14.23	12.15
NO DESC.	564374.63	1459537.53	14.50	12.19
SW16-PZM003	564524.42	1462434.76	14.94	12.80
SW16-PZM067	564528.56	1462441.95	15.33	13.06
TM03-PZM004	568852.92	1457628.81	12.66	10.34
TM03-PZM037	568849.30	1457622.17	12.08	10.38
TM05-PZM005	568837.40	1458595.64	12.76	10.62
TM05-PZM040	568830.24	1458596.23	12.83	10.70
TS10-PDM008	567529.89	1464010.26	6.74	3.88
SG07 PD	564025.39	1463980.66	17.93	15.19

Figure 1.0: RW-RWBW-20 Photographs



APPENDIX D

XRF CALIBRATION LOG											
PROJECT NAME: Area A Parcel A3 PDI SAMPLER NAME: N. Kurtz											
PROJECT NUMBER:	150298M-11-3				DATE: April	1, 2016	PAGE 1 of 1				
	NIST	2710a	NIST	2711a	Blank	x SiO2					
DATE/TIME	Zn	Cd	Zn	Cd	Zn	Cd	COMMENTS				
Certified Value (mg/kg)	0.418±0.015	12.3±0.3	414±11	54.1±0.5	±	±	-				
10/1/2015 0840	0.4084*	ND<74	NA	NA	ND	ND	-				
10/5/2015 0748	NA	NA	385±13	66±16	ND<11	ND<60	-				
10/5/2015 1003	NA	NA	357±11	60±16	ND<9	ND<50	-				
10/5/2015 1141	NA	NA	360±11	49±15	ND<9	ND<62	-				
10/5/2015 1600	NA	NA	361±12	47±16	ND<9	ND<50	-				
10/6/2015 0920	NA	NA	357±11	48±15	ND<9	ND<48	-				
10/6/2015 1145	NA	NA	361±11	36±16	ND<8	ND<52	-				
10/7/2015 0755	NA	NA	363±11	52±16	ND<10	ND<53	-				
10/7/2015 1000	NA	NA	357±11	77±16	ND<9	ND<57	-				
10/7/2015 1110	NA	NA	360±11	69±13	ND<10	ND<52	-				
10/7/2015 1335	NA	NA	354±11	59±16	ND<11	ND<59	-				
10/7/2015 1505	NA	NA	349±11	60±16	ND<9	ND<53	-				
10/8/2015 0805	NA	NA	363±11	67±16	ND<10	ND<53	-				
10/8/2015 1000	NA	NA	372±11	65±15	ND<10	ND<56	-				
10/8/2015 1205	NA	NA	405±11	60±14	ND<11	ND<60	-				

APPENDIX E

PID CALIBRATION LOG										
PROJECT NAME	E: Area A Parcel A3			SAMPLER NAME: N	. Kurtz, L. Perrin & P	. Vogel				
PROJECT NUME	BER: 150298M-10/11-	3		DATE: April 1, 2016	PAGE	E <u>1</u> of <u>1</u>				
				STANDARD						
DATE/TIME	PID SERIAL #	FRESH AIR CAL	STANDARD	CONCENTRATION	METER READING	COMMENTS				
9/21/2015	592-913262	*	Isobutylene	100 ppm	100.1	LLP				
9/22/2015	592-908581	*	Isobutylene	100 ppm	100.1	LLP				
9/23/2015	592-908581	*	Isobutylene	100 ppm	100.1	LLP				
9/24/2015	592-908581	*	Isobutylene	100 ppm	100.1	NSK				
9/25/2015	592-908581	*	Isobutylene	100 ppm	100.1	LLP				
9/28/2015	592-908581	*	Isobutylene	100 ppm	100.3	LLP				
9/29/2015	592-908608	*	Isobutylene	100 ppm	100.0	NSK				
9/30/2015	592-908608	*	Isobutylene	101 ppm	100.1	LLP				
10/1/2015	592-908608	*	Isobutylene	100 ppm	100.1	NSK				
10/5/2015	592-908608	0.0	Isobutylene	100 ppm	100.0	-				
10/6/2015	592-908608	0.0	Isobutylene	100 ppm	99.6	_				
10/7/2015	592-908608	0.0	Isobutylene	100 ppm	100.0	-				
10/8/2015	592-908608	0.0	Isobutylene	100 ppm	100.0	-				
10/21/2015	592-908608	0.0	Isobutylene	100 ppm	100.1	PV				
10/22/2015	592-908608	0.0	Isobutylene	100 ppm	100.1	PV				
10/23/2015	592-908608	0.0	Isobutylene	100 ppm	100.0	PV				
10/26/2015	592-908608	0.0	Isobutylene	100 ppm	100.0	PV				
10/27/2015	592-908608	0.0	Isobutylene	100 ppm	100.1	PV				
10/28/2015	592-908608	0.0	Isobutylene	100 ppm	100.1	PV				
10/29/2015	592-908608	0.0	Isobutylene	100 ppm	100.0	PV				
			Isobutylene	100 ppm						
			Isobutylene	100 ppm						
			Isobutylene	100 ppm						

* Fresh air calibrations were completed, but not recorded

APPENDIX F

	A	RM Group Inc.	LOG OF	TEMPORARY GR COLLECTION PO		
	e: Sparro Sj	EnviroAnalytics Group ws Point - Area A Parcel A3 parrows Point, MD oject No.: 150298M-10-3 Page 1 of 1	Date Installed Casing/Riser Type Borehole Diameter Drilling Method Driller	: 10-26-15 : PVC : 3.25" : 7822DT Geoprobe : Kevin Pumphrey	Drilling Company TOC Elevation 0-Hr DTW 24-Hr DTW ARM Representative	: Green Services, Inc : 13.14 : 14.53' TOC : 15.20' TOC : L. Perrin
Depth in Feet	Surf. Elev. 10.17	DESCRIF	ΫΤΙΟΝ	PZM Name: RW-05	;7-PZ	REMARKS
1— 2— 3—	- 8 - 7	Riser Type: PVC Riser Diameter: 1 inch Riser Stickup: 32.75"				
4— 5— 6— 7— 8—	- 5 - 4 - 3	Screen Type: PVC Screen Diameter: 1 inch Screen Amount: 5 feet Slot Size: 0.010"				
9	- 1 - 0 1	Filter Pack: Top: 20' bgs Bottom: 25' bgs Used filter pack		Bentonite	seal	
13— 14— 15— 16—	3 4 5	Bentonite Seal: Top: 0 (surface) Bottom: 25' bgs Grain Size: 3/8" chips/ granu	lar 30-50 mesh	1" PVC R	iser	
17— 18— 19— 20—	7 8 9 10					
21- 22- 23- 24-	12 13 14					
	16 17 18				sk	' pre-packed well screen
29 – 30 – Total De	19 epth: 30' t	End of Boring				

1		RM Group Inc.	LOG OF	TEMPORARY GROCULLECTION POI		
	e: Sparro Sj	EnviroAnalytics Group ws Point - Area A Parcel A3 parrows Point, MD oject No.: 150298M-10-3 Page 1 of 1	Date Installed Casing/Riser Type Borehole Diameter Drilling Method Driller	: 10-26-15 : PVC : 3.25" : 7822DT Geoprobe : Kevin Pumphrey	Drilling Company TOC Elevation 0-Hr DTW 24-Hr DTW ARM Representative	: Green Services, Inc : 14.19 : 13.52' TOC : 13.24' TOC : L. Perrin
Depth in Feet	Surf. Elev. 11.07	DESCRIF	PTION	PZM Name: RW-06	3-PZ	REMARKS
	- 8 - 7 - 6 - 5 - 4 - 3 - 2 - 1 - 0 1 2 3	Riser Type: PVC Riser Diameter: 1 inch Riser Stickup: 34.75" Screen Type: PVC Screen Diameter: 1 inch Screen Amount: 5 feet Slot Size: 0.010" Filter Pack: Top: 30' bgs Bottom: 35' bgs Used filter pack Bentonite Seal: Top: 0 (surface) Bottom: 30' bgs Grain Size: 3/8" chips/ granul	lar 30-50 mesh	Bentonite		
16	6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	End of Boring		-Sand Pack	5 K	' pre-packed well screen
Total De	epth: 35' t	_				

1	A	RM Group Inc.	LOG OF	TEMPORARY GR	OUNDWAT INT: RW-06	er Sample 7-Pz
Client: EnviroAnalytics Group Site: Sparrows Point - Area A Parcel A3 Sparrows Point, MD ARM Project No.: 150298M-10-3 Page 1 of 1			Date Installed: 10-26-15Drilling ComCasing/Riser Type: PVCTOC ElevatiBorehole Diameter: 3.25"0-Hr DTWDrilling Method: 7822DT Geoprobe24-Hr DTWDriller: Kevin PumphreyARM Represe			: Green Services, Inc : 13.37 : 15.17' TOC : 14.71' TOC re : L. Perrin
Depth in Feet	Surf. Elev. 10.68	DESCRIF	PTION	PZM Name: RW-06	7-PZ	REMARKS
0	- 10 - 9 - 8 - 7 - 6 - 5 - 4 - 3 - 2 - 1234567891011121314151617181920131415161718192021222324232424	Riser Type: PVC Riser Diameter: 1 inch Riser Stickup: 28.5" Screen Type: PVC Screen Amount: 5 feet Slot Size: 0.010" Filter Pack: Top: 27' bgs Bottom: 32' bgs Used filter pack Bentonite Seal: Top: 0 (surface) Bottom: 27' bgs Grain Size: 3/8" chips/ granu	lar 30-50 mesh		iser	5' pre-packed well screen

1	A	RM Group Inc.	LOG OF	TEMPORARY C		
	e: Sparro S	EnviroAnalytics Group ws Point - Area A Parcel A3 parrows Point, MD oject No.: 150298M-10-3 Page 1 of 1	Casing/Riser Type: PVCTOC ElevationBorehole Diameter: 3.25"0-Hr DTWDrilling Method: 7822DT Geoprobe24-Hr DTW			: Green Services, Inc : 14.14 : 10.60' TOC : 10.51' TOC e : L. Perrin
Depth in Feet	Surf. Elev. 10.84	DESCRIF	ντιον	PZM Name: R\ ∏	V-070-PZ	REMARKS
0 1 2 3	- 10 - 9 - 8	Riser Type: PVC Riser Diameter: 1 inch Riser Stickup: 37.25"				
4 5 6 7 8	- 7 - 6 - 5 - 4 - 3	Screen Type: PVC Screen Diameter: 1 inch Screen Amount: 5 feet Slot Size: 0.010"				
9- 10- 11- 12-	- 2 - 1 - 0	Filter Pack: Top: 25' bgs Bottom: 30' bgs Used filter pack		Bentc	nite seal	
13- 14- 15- 16-	4	Bentonite Seal: Top: 0 (surface) Bottom: 25' bgs Grain Size: 3/8" chips/ granu	lar 30-50 mesh	1" PV	'C Riser	
17- 18- 19- 20-	7 8 9					
22- 23- 24-	10 11 12 13					
26- 27- 28-	14 15 16 17					5' pre-packed well screen
30-	18 19 epth: 30' t	End of Boring				

ARM Group Inc. Earth Resource Engineers and Consultants Boring ID: RW22-PZM(I)				Resource Engi ad Consultants	ineers s	ARM Project No. : 150298M-10-3 W Project Description : Sparrows Point - Parcel A3 0 Site Location : Sparrows Point, MD 2 ARM Representative : P. Vogel 1 Checked by : E. Magdar N Drilling Company : Allied E Driller : Mike Waller D Drilling Equipment : Diedrich D 120			Date Started: 10/19/15 ~12:30Weather: Clear to P. Cloudy, 55 F0 Hr Depth to Water: NA24 Hr Depth to Water: NATOC Elevation:: 11.25' amslNorthing: 571963.73Easting: 1456061.85			
				(page 1 of	1)	Bit/Auger Size:	: 4.25" ID HSA			1		
Depth (ft.)	Sample No:	Recovery (%)	(MAA) DIA	Blow Count		DESC	RIPTION	Well IC	D: RW22-PZM(I) — Flush-mount	REMARKS		
0-	S1	50	0.5	13-13-6-38		avelly SAND, fine to c ark gray to black	oarse grained with some		1 1 1	Concrete		
	S2	70	0.1	7-5-6-5	-		nge brown to gray, wet at		Concrete	pad		
4-	S3	80	0.2	1-2-1-2	4 093							
-	S4	85	0.1	3-5-6-8		ayey SILT, gray and , moist throughout	tan to brown, some			bentonite		
8-	S5	80	0.2	7-5-6-7	linetanig	, molet in oughout				chips		
-	S6	85	0.2	6-7-8-8								
12-	S7	90	0.1	9-10-10-10					2" PVC Riser			
-	S8	65	0.1	4-8-7-8	SAND,	fine-grained, tan to g	ray, wet		Bentonite Seal			
16-	S9	75	0.1	5-6-6-6								
-	S10	75	0.1	7-8-8-6								
20-	S11	75	0.0	3-2-4-4	20-21.5 dark gra		e grained with fine gravel,					
-	S12	50	0.0	3-4-4-5	21.5-26	.5' CLAY, dark gray,	stiff, moist					
24-	S13	25	0.0	5-5-13-18					-			
- 28-	S14	100	0.2	8-14-16-19		' SAND, fine to coars brown and tan to gra	e grained with fine gravel,			#2 sand		
-	S15	100	0.2	25-33-40-50/5		2.5 m and tail to gra	,,		-Sand Pack	5' screen		
- 32-	S16	100	0.1	2-5-19-30					2" PVC Screen	29-34' bgs 0.020" slot		
-	S17	100	0.5	12-31-31-35								
- 36-	S18	100	0.1	2-3-4-6		' CLAY, light gray, sti			Bentonite Seal			
-	S19	85	0.1	7-7-7-14	36-37.5		ff, with 1/2" thick fine					
40-	S20	75	0.1	2-6-10-12	37.5-39	' Clayey SAND, dark Clayey SAND, light gr	gray		-Borehole Loss			
					100-40 (Jayey OAND, light gi	מץ, שכו	/				
Total Bo	orehole	Depth	: 40' bg	S.								

ARM Group Inc. Earth Resource Engineers and Consultants Boring ID: RW23-PZM(I) (page 1 of 1)					ineers s (I)	ARM Project No. : 150298M-10-3 V Project Description : Sparrows Point - Parcel A3 0 Site Location : Sparrows Point, MD 2 ARM Representative : P. Vogel T Checked by : E. Magdar N			Date Started: 10/16/1508:00Weather: Clear to P. Cloudy, 55 F0 Hr Depth to Water: NA24 Hr Depth to Water: NATOC Elevation:: 11.46' amslNorthing: 572002.55Easting: 1456257.38			
Depth (ft.)	Sample No:	Recovery (%)	(МАА) ОІА	Blow Count		DESCI	RIPTION	We		23-PZM(I) Ish-mount	REMARKS	
0-	S1	50	0.0	6-28-50/2		ND and GRAVEL, fin black, dry	e to coarse grained, dark				Concrete	
-	S2	75	0.0	13-12-11-12			prange to ten, wet at 6		- −Cc	ncrete	pad	
4-	S3	100	0.0	7-8-9-9	bgs	שמאס, inte grained, (brange to tan, wet at 6'	9797979 19	and a second sec			
-	S4	100	0.1	8-8-8-5							Bentonite	
8-	S5	75	0.0	1-5-4-5							chips	
-	S6	100	0.1	4-5-6-7	1				2"	PVC Riser		
12-	S7	85	0.0	1-2-3-3	11.8-16'	Sandy CLAY, gray		100 B	Ве	ntonite Seal		
-	S8	100	0.0	4-4-4-4	1							
16-	S9	25	0.0	1-7-4-6	16-31' S	AND, tan to orange	to gray, wet	2.62.62.62				
-	S10	100	0.0	4-7-7-7	1			2012 2012 2012 2012 2012 2012 2012 2012				
20-	S11	100	0.0	3-1-2-13								
-	S12	100	0.0	4-7-13-14	1							
24-	S13	100	0.0	3-1-2-13								
-	S14	100	0.0	22-18-3-4							#2 sand	
28-	S15	100	0.2	4-7-10-14	1				-Sa	nd Pack		
-	S16	100	0.0	14-22-17-25	31-35.5'	SAND, fine to coars	e grained, with trace fine		1 - Carl	PVC Screen	10' screen 26-36' bgs 0.020" slot	
32-	S17	100	0.0	3-5-10-17	gravel, ta						0.020 0.01	
-	S18	100	0.0	8-3-4-4								
36-	S19	50	0.0	4-12-32-14	35.5-38'	CLAY, with trace sil	t, gray, stiff			rehole Loss		
- - 40-					End of B	Boring						
Total Bo	orehole	Depth	38' bg	S.								

в	soring	E	arth l an	Group Resource Engine d Consultants V24-PZM((page 1 of	Project Description : Sparrows Point - Parcel A3 0 Hr Depth to Water : NA Site Location : Sparrows Point, MD 24 Hr Depth to Water : NA ARM Representative : P. Vogel TOC Elevation : 11.05' ams Checked by : E. Magdar Northing : 572055.46 Drilling Company : Allied Easting : 1456360.6 Drilling Equipment : Diedrich D 120 : Diedrich D 120 : 1456360.6	Cloudy, 55 F
Depth (ft.)	Sample No:	Recovery (%)	(MAG) OIG	Blow Count	DESCRIPTION	REMARKS
0-	S1	50	0.1	10-40-19-5	0-2' Silty SAND with gravel (slag), brown to Concrete	Concrete pad
4-	S2	75	0.2	8-9-5-5	2-3' Silty SAND, dark gray 3-4.5' Sandy CLAY, olive gray, wet at 4' bgs	
	S3	90	0.4	5-7-13-6	4.5-7' SAND, fine-grained, tan, wet	
8-	S4	95	0.1	9-15-16-9	7-10' SAND, fine-grained, light gray, trace clay at 8'	Bentonite chips
	S5	85	0.1	4-7-7-6	bgs	
12-	S6	80	0.1	2-2-3-7	10-12' Clayey SAND, fine-grained, gray to orange, wet — Bentonite Seal	
	S7	85	0.0	1-3-3-4	12-16' SAND, fine-grained, tan to orange, wet	
16-	S8	-	-	4-5-5-4		
-	S9	50	0.1	3-1-1-1	16-18' SAND, gray, wet	
20-	S10	100	0.0	1-2-3-2	18-22' CLAY, with trace fine sand, dark gray, stiff, moist	
-	S11	55	0.0	2-2-4-8		
24-	S12	60	0.0	4-6-9-11	22-28' SAND, fine to coarse grained with some fine gravel, tan to orange, wet	#2 sand
-	S13	100	0.0	4-5-8-16	Trace fine gravel and 1" Clayey SAND layer at 27' bgs 2" PVC Screen	5' screen 23-28' bgs
28-	S14	100	0.0	16-17-17-18		0.020" slot
	S15	-	-	1-4-4-4	28-36' CLAY, with trace sand, gray	
32-	S16	65	0.0	5-4-4-5	2" Gravelly medium grained SAND layer at 31' bgs 3" Clayey SAND medium/coarse grained layer at 33'	
-	S17	70	0.0	4-5-5-6	bgs Trace silt at 35' bgs	
- 36	S18	100	0.0	3-3-4-5		
-	S19	100	0.0	4-3-4-6	36-38' Silty CLAY, dark gray, moist	
40-	S20	100	0.0	2-2-4-5	38-48' Clayey SILT, very clayey, dark gray, moist Bentonite Seal	
-	S21	100	0.0	4-3-4-6		
- 44	S22	100	0.0	4-4-4-5		
	S23	100	0.0	4-6-9-5		
48-	S24	100	0.0	5-4-4-4		
	S25	100	0.0	3-4-4-4	48-50' Silty CLAY, dark gray, moist	
52-					End of Boring	
Total Bo	L orehole	Depth:	: 50' ba	S.		
			- 9			

CRRGPFKZ'I "

GROUNDWATER SAMPLI Sheet Number	
Job Name: Area A, Rwn PDI Job Loc Job Number: 150298m Phase: PDI Task: (Sample Location: RW-057-PZ-Name(s) of Sampler(s) Description of Sample: Water X	: Lisa Perrin, Nick Kurtz
PURGINGTime/Date Started: 12.50 / $11-9-15$ Air Temperature:	SAMPLING Time/Date Started: 1321/1-1-4-15 Air Temperature: 54 CPCO Weather Sunny Rain Conditions Overcast Other Depth to Water: ft Sampling Method: Bailer Submersible Pump Peristaltic Pump Peristaltic Pump Other Number of Bottles Filled: 5 Date Sent To Lab: 11-4-15 Laboratory Name: PACE Parameters to Analyze: See Coc Chain of Custody Number:

FIELD DATA

Time	1300	1306	1311	1316		Remarks:
Volume of water purged					gal	
pH	4.73	4.42	4.36	4.33	s.u.	
Conductance	2.638	2.591	2.574	2.576	ms/cm	
Temperature	the second second second	16.04			°C	
DO		0.43		0.21	mg/l	
Redox	-221	-40.4	47.4	-49:3	mV	
Turbidity	3117 AU	2644 AN	1958 AU	1559 AN	NTU	-
SpC		3126			us/cm	

Pipe Volume:

1" I.D. = 0.041 gal/ft 2" I.D. = 0.163 gal/ft 4" I.D. = 0.653 gal/ft 6" I.D. = 1.47 gal/ft

GROUNDWATER SAMPI Sheet Number	
Job Name:Area A, Rum PDIJob LocJob Number:150249mPhase:RDISample Location:Rw-063-PzName(s) of Sampler(s)Description of Sample:WaterX	s): Lisa Perrin Nick Kurtz
PURGINGTime/Date Started: $1 23 / 1 - 9 - 15$ Air Temperature: 50 (F)°C WeatherSunnyRainConditionsOvercast XOtherDepth to Water: $13 \cdot 30$ ftTotal Well Depth: $37 \cdot 36$ ftHeight of Water Column: $24 \cdot 06$ ftWell1-inch X4-inchDiameter:2-inch0.6 ft x 0.041 gal/ft = 0.486 galPurge Volume Calculation: $24 \cdot 06$ ft x 0.041 gal/ft =24 \cdot 06 ft x 0.041 gal/ft = 0.486 galPurge Volume = $3 \times 0.986 = 2.958$ galPurging Method:Pump X Bailed OtherGallons Removed: 4.25 galLength of Time Purged 30 minYield at End of Purging: 0.142 gpmHow was yield measured?Graduated BucketColor 0.142 gpmHow was yield measured?Yes_ No	SAMPLING Time/Date Started: 1158 / 11-9-15 Air Temperature: 50 0000 Weather Sunny Rain Conditions Overcast X Other Depth to Water: ft Sampling Method: Bailer Submersible Pump Peristaltic Pump Veristaltic Pump X Other Other Number of Bottles Filled: 6 Date Sent To Lab: Pace Parameters to Analyze: Set Coc Chain of Custody Number: Other: Other: Other

Time	1138	1143	1148	1153		Remarks:
Volume of water purged	3.00	3.60	3:75	4.25	gal	
pН	4.90	4.89	4.89	4.90	s.u.	
Conductance	2:790	2.768	2.781	2790	ms/cm	-
Temperature	14.37	14.40	1	14.41	°C	
DO 🔗	0116	0.31	0.29	0,18	mg/l	
Redox	-30.7	-46.8	-53.6	-59.4	mV	
Turbidity	1182 AU	183	696 AU	66244	NTU	
SpC	3497	3471	3484		us/cm	

Pipe Volume:

1" 1.D. = 0.041 gal/ft 2" 1.D. = 0.163 gal/ft

GROUNDWATER SAMPLIN Sheet Number	
Job Name: Area A Row Pot Job Locat Job Number: 150298m Phase: PDT Task: Task: Sample Location: Rwood 7 - PZ Name(s) of Sampler(s): Description of Sample: Water X Sample	tion: <u>SPT</u> <u>6w sampling</u> <u>Lisa Pervin and Nick Kurtz</u> Soil Other
PURGINGTime/Date Started: 1024 / $11-9-15$ Air Temperature: 45 $69^{\circ}C$ WeatherSunnyRainConditionsOvercast XOtherDepth to Water: 14.61 ftTotal Well Depth: 34.01 ftHeight of Water Column: 19.40 ftWell1-inch X4-inchDiameter:2-inch6-inchWell Volume Calculation: 19.40 ft x 0.041 gal/ft = 0.795 galPurge Volume = $3 \times 0.795 = 2.39$ galPurging Method:Pump X BailedOtherGallons Removed: 3.75 galLength of Time Purged 3.3 minYield at End of Purging: 0.114 gpmHow was yield measured?Graduated BucketColor 51.6000 NoneTurbidity 40.5000 NoneWas well cavitated?YesNo	SAMPLING Time/Date Started: 1102 / 11-9-15 Air Temperature: 45 @ff °C) Weather Sunny Rain Conditions Overcast X Other Depth to Water: ft Sampling Method: Bailer Submersible Pump Other Other Other

Time	1042	1047	1052	1057		Remarks:
Volume of water purged	2.75	3.00	3.50	3.75	gal	
pН	4.58			and the second se	s.u.	
Conductance	3.577			3.510	ms/cm	
Temperature	15.38	15.43	15.38		°C	
DO	8233	3.4	20:24	0.22	mg/l	
Redox	-0,7	-3.4	-6.1	-10.3	mV	
Turbidity	92.0	85.6	44.1	35.8	NTU	
SpC	4383	4246	4282		us/cm	

Pipe Volume:

1" I.D. = 0.041 gal/ft 2" I.D. = 0.163 gal/ft

GROUNDWATER SAMPL Sheet Number	
Job Name: A. Pacced A3, FDI Job Log Job Number: 15029800 Phase: Task: Sample Location: Rw-070-PZ Name(s) of Sampler(s Description of Sample: Water X): Lisa Perrin, Nick Kurtz
PURGINGTime/Date Started: $0 915 / 11 - 9 - 15$ Air Temperature: $34 - 66^{\circ}$ Air Temperature: $34 - 66^{\circ}$ WeatherSunnyRainConditionsOvercastXOtherDepth to Water: $0.55 - 6t$ Depth to Water: $0.55 - 6t$ Total Well Depth: $32.50 - 6t$ Height of Water Column: $22.05 - 6t$ Well1-inch 4 -inchDiameter:2-inch 2 -inch 6 -inchWell Volume Calculation: $22.05 - 6t \times 0.041 - 8al/et = 0.904 - 8al/et = 2.71 - 8alPurge Volume =3 \times 0.964 = 2.71 - 8alPurging Method:Pump \vee BailedOtherGallons Removed:3.75 - 8algalLength of Time Purged25 - 8pmHow was yield measured?Graduated BucketColorClearOdorNomeTurbidityWas well cavitated? YesWas well cavitated? YesNo$	SAMPLING Time/Date Started: 0945 / 11-9-15 Air Temperature: 34 _ CF*C) Weather Sunny _ Rain Conditions Overcast & Other Depth to Water: ft Sampling Method: Bailer Submersible Pump Peristaltic Pump X Other

Time	0925	0930	0935	0940		Remarks:
Volume of water purged	3.0	3.25	3.5	3.75	gal	
pH	6.35	5.41	5,19	5,10	s.u.	
Conductance			3792	3766	ms/cm	
Temperature	14.25	14.32	14.27	14,26	°C	
DO	0,85	0.37	0.031	0.041	mg/l	
Redox	1.8	-20.4	-26.6	-28.4	mV	
Turbidity	6.17	4.00		2.32	NTU	
SpC	3.088	3.047	3,013	2.993	us/cm	

Pipe Volume:

1" I.D. = 0.041 gal/ft 2" I.D. = 0.163 gal/ft

Job Name:Mathematical A farcel A3Job IJob Number:15029800Phase:MOTSample Location:RW10-P20020Name(s) of SamplerDescription of Sample:WaterX	(s): Lise Petru
PURGING Time/Date Started: 1203 / 11-12-15 Air Temperature: 01 FPCC) Weather Sunny Rain Conditions Overcast X Other Depth to Water: NA ft Total Well Depth: NA ft Height of Water Column: ft Well 1-inch 4-inch Diameter: 2-inch 6-inch Well Volume Calculation: ft x gal Purge Volume = x = gal Purging Method: Pump & Bailed Other Gallons Removed:	SAMPLING Time/Date Started:/

Time	1203		/	1	1			Remarks: Wellis
Volume of water purged	Ø		1	1	/		gal	from pump test.
pH ± 0.1	6.74	11					s.u.	has already been
Conductance	3.213			/		/ /	ms/cm	running
Temperature	17.20	1					°C	O
DO 1905 16/10 0.3	0.82	$\left(\right)$	/	/			mg/l	
Redox ± 10 mV	-85.3		//	1		11	mV	
Turbidity 75 10%	12,32	$\left[\right]$				11	NTU	
SpC 3 %	3777	(/		1	1	us/cm	

Pipe Volume:

1" I.D. = 0.041 gal/ft 2" I.D. = 0.163 gal/ft 4" I.D. = 0.653 gal/ft 6" I.D. = 1.47 gal/ft

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GROUNDWATER SAMPLI Sheet Number	
Job Name: Area A Parcel A'3 Job Loca Job Number: 150298m Phase: PDF Task: 0 Sample Location: Kula-Pzmozo Name(s) of Sampler(s): Description of Sample: Water X	<u>Lisa Perrin</u>
PURGINGTime/Date Started: 1330 / $1-12-15$ Air Temperature:	SAMPLING Time/Date Started: 1355 / 11-12-15 Air Temperature: 61 60°C) Weather Sunny Rain Conditions Overcast X Depth to Water: ft Depth to Water: ft Sampling Method: Bailer Submersible Pump X Peristaltic Pump Other Number of Bottles Filled: 16 Date Sent To Lab: 11-12-15 Laboratory Name: PHCE Parameters to Analyze: Sceecoc Chain of Custody Number:

Time	1330	1335	1340	1345		Remarks:
Volume of water purged	0.25	0.50	1,00	1.50	gal	
pH ± 0.1	5.84	5.70	5.68	5.65	s.u.	
Conductance	8.586	9.777	10.07	10.21	ms/cm	
Temperature Zills	16.92	17.20	17.39	17.34	°C	
DO toals ASIA 0.3	1.00	0.45	0.43	0.30	mg/l	
	-48.6	62.8	-66.9	-71.3	mV	
Turbidity 75 10%	67.4				NTU	
SpC 3 %	9896				us/cm	

Pipe Volume:

1" I.D. = 0.041 gal/ft 2" I.D. = 0.163 gal/ft 4" I.D. = 0.653 gal/ft 6" I.D. = 1.47 gal/ft 3 x purge volume was not completed b/c pername well

GROUNDWATER SAMPLI Sheet Number	
Job Name:AreaA Parcel A3Job LocJob Number: $150,240$ Phase: PDT Task:Sample Location: $Rw_{D,2}$ $PTm 020$ Name(s) of Sampler(s)Description of Sample:WaterX	: Lisa Perrin
PURGINGTime/Date Started: 1210 / $11-13-15$ Air Temperature: 59 $00^{\circ}/^{\circ}C$)WeatherSunny y RainConditionsOvercastOtherDepth to Water: 12.03 ftTotal Well Depth:ftHeight of Water Column:ftWell1-inch4-inchDiameter:2-inch6-inchWell Volume Calculation:ft xft xgal/ft =galPurge Volume =x=galPurging Method:Pump > BailedOtherGallons Removed:1.75galLength of Time Purged28minYield at End of Purging:0.0625gpmHow was yield measured? m minYield at End of Purging:0.0625gpmHow was yield measured? m minYield at End of Purging:0.0625gpmHow was yield measured? m minYield at End of Purging:0.0625gpmHow was yield measured? m minYield at End of Purging:0.0625gpmHow was yield measured? m minYield at End of Purging:NominYield at End Of Purging:Yield PurgingMinYield At End Of Purg	SAMPLING Time/Date Started: 1240 11-13-15 Air Temperature: 59 10°C° Weather Sunny Kain 10°C° Weather Sunny Kain 10°C° Weather Sunny Kain 10°C° Weather Sunny Kain 10°C° Onditions Overcast Other 10°C° Depth to Water: ft Sampling Method: Bailer 10°C° Submersible Pump X Other 10°C° 10°C° Number of Bottles Filled: 16°C 16°C 16°C 16°C Date Sent To Lab: 16°C 16°C 16°C 16°C 16°C Date Sent To Lab: 16°C 16°C

Time	1213	1208	1223	1228	1233	1238		Remarks: 🕺 3×
Volume of water purged	0.25	0.50	1,00	1.25	1.50	1.75	gal	volume was not
pH ± 0.1	4.91	4.49	4.40	4.25	4.19	4.17	s.u.	calculated 6/a
Conductance	2.822	3.263	3,369	3.292	3.224	3.134	ms/cm	permanent well.
	16.63							
DO tola Man 03							mg/l	
1	-108.8	1.00					mV	
	6.40	and the second					NTU	
	3352						us/cm	

Pipe Volume:

1" I.D. = 0.041 gal/ft 2" I.D. = 0.163 gal/ft

GROUNDWATER SAMPL Sheet Number	ING RECORD SHEET
Job Name: Arace Ar parcel Ar3 Job Loc Job Number: 150298m Phase: Point Task: Sample Location: Rw07-PZm017Name(s) of Sampler(s) Description of Sample: Water X): <u>Lisa Perrue</u>
PURGINGTime/Date Started: $0991 / 11 - 13 - 15$ Air Temperature: $55 - 66^{\circ}C$ WeatherSunnyXConditionsOvercastOtherDepth to Water: $11.91 - ft$ Total Well Depth: $56 - ft$ Height of Water Column:ftWell $1 - inch - 4 - inch - ft$ Diameter: $2 - inch - 4 - inch - ft$ Well Volume Calculation: $ft x _ gal/ft = _ gal$ Purge Volume = x = galPurging Method: $1.75 - gal$ Length of Time Purged $28 - min$ Yield at End of Purging: $0.0625 - gpm$ How was yield measured?ColorColor $46 - Clear - Odor - cone - Turbidity - lowWas well cavitated? Yes _ No$	SAMPLING Time/Date Started: 10.5 / 11-13-15- Air Temperature: 55 ©P°C) Weather Sunny X Rain Conditions Overcast Other Depth to Water:

Time	0944	0949	0954	0959	1004	1009		Remarks:
Volume of water purged	0,25	0.50	1.00	1.25	1.50	1.75	gal	
pH ± 0.1	5.24	4.49	4.30	4.19	4.14	4.10	s.u.	
Conductance	2.666	2.641	2.610	2.597	2.592	2.577	ms/cm	
Temperature	17.33	and the second second second	17.12	17.31	17.43	17.18	°C	
DO they woll 0.3	0.50	0.40	0.38	0.31	0.28	6.25	mg/l	
Redox ± 10 mV	-38.6	-44.1	-48.6		-60.9		mV	
Turbidity 75, 10%	1.73	1.47	1.82	0,61	0.83	0.68	NTU	
SpC 3%	3123	3096	3012					

Pipe Volume:

1" I.D. = 0.041 gal/ft 2" I.D. = 0.163 gal/ft

	Low Flow Sampling						ARM Group Inc. Earth Resource Engineers and Consultants						
	Project N	lame: Area	A Parce	1 +3	PDE	Project Nu	mber:	502980		-			
1.00	Well Nur	nber: Rw;	20 - PZI	mozo			-17-15			-			
(1)		meter (in):					Volume (gal)):					
	Total Dep	oth (ft):				CONTRACTOR DATA	roller Setting						
		Water (ft)	13.31				(mL/min)		0.0530				
		Water Colu					time Purged	and the second se	3				
		1			WELL PUR	GING RECC		()	2				
tait 758	Time	Volume Purged (gallons)	Temp (°C)	рН (s.u.)	Specific Conductance (Mater)	Dissolved Oxygen (mg/L)	ORP (mV)	Turbidity (NTU)	Comments				
	0801	0.25	16.67	3,25	2.460	0,50	-33.8	14.3	Clouder				
	0806	0.50	16.35	292	2414	0.35	-79.9	15.2	Cloudy No odor				
	0811	0.75	16.21	2.82	2374				no odor				
	0816	1.00	16.05	2.83		0.26	107.7	12.7					
	0821				2.346	0.23	-125.1	12,19					
		1.25	16.09	2,91	2.329	6.21	-147.9	11.07					
	0826	1.50		\$3.00	2.326	019	158.0	12.02	-	_			
	0831	1.75	16.30	3.06	2,323	0.18	167.7	10,94					
	Cam	ple ID	Time C		MONITORING		The second second			1925			
	Sam	ole ID	Time C	ollected	Param			tainer	Perservative	Y/N			
					TCL-V TCL-SV			nL VOA	HCL	4			
	2000-	Pzmaco	00 10	~	TAL-M			Amber nL Plastic	none	4			
	Thursday	1 211 Web	D8 3	S	Oil and O		1-2501		HN03-none	1 y			
					TPH-L			Amber	nono	N			
		1		1.14	TPH-C			nL VOA	none HCL	N			
				0	Hexavalent			nL Plastic	1	9			
					Cyan			nL Plastic	Nac H-Done	Y			
- 1	Ν	Aatrix Spike	e present?	N		220.84	2-16	III. I Idolle	NUC H HONC	-			
1		Duplicate a		M									
	Sampled	By: Lise	a ferru	Commen	ts:	Extra	frechesig	mpaira	moters tak	en			
		Casing	Volume: 1'	'I.D. = 0.041	gal/ft - 2" I.D. = 0 ft x	0.163 gal/ft - 4" gal/ft =		ul/ft - 6" I.D. =	1.47 gal/ft				

2-11 plastic unpreserved 1-500 a plastic sulfuric acid 2-40 ml VOAS sulfuric acid 1-500 ml plastic Nault + znacotate

Project Name	Parcel A3	Date	11/9/15	
Weather	Partly Cloudy 50s-60s			
Calibrated by	N. Kurtz & L. Perrin		Instrument	YSI Meter
Serial Number	NA			

Parameters	Morning Calibration	Morning Temperature	End of Day Calibration Check	End of Day Temperature
Specific Conductance Standard #1	1.412	40°F (est.)	NA^{2}	NA
Specific Conductance Standard #2	NA	NA	NA	NA
pH (7)	6.98	40 °F (est.)	NA^{Σ}	NA
pH (4)	3.97	40°F (est.)	NA [¥]	NA
pH(10)	9.96	40°F (est.)	NA [¥]	NA
ORP Zobel Solution	240.1	40°F (est.)	NA^{Ψ}	NA
Dissolved Oxygen 100% water saturated air mg/L	13.30	40°F (est.)	NA^{F}	NA
Dissolved Oxygen Zero Dissolved Oxygen Solution mg/L	NA	40°F (est.)	NA	NA
Barometric Pressure mm Hg	775.2	NA	NA	NA
Turbidity #1 (10 NTU)	9.24	NA	NA [¥]	NA
Turbidity #2 (0.0 NTU)	0.04	NA	NA^{Ψ}	NA
Turbidity Standard #3	NA	NA	NA	NA

^{*}The post-calibration check was not performed on this date. Values displayed on field purge logs may be inaccurate.

Project Name Parcel A3 Date 11/12/15 Weather Cloudy 50s Calibrated by N. Kurtz & L. Perrin Serial Number NA

Instrument YSI Meter

Parameters	Morning Calibration	Morning Temperature	End of Day Calibration Check	End of Day Temperature
Specific Conductance Standard #1	1.446	55 F (est.)	$1.078^{\text{¥}}$	60 F (est.)
Specific Conductance Standard #2	NA	NA	NA	NA
pH (7)	7.00	55°F (est.)	7.00	60°F (est.)
pH (4)	4.00	55 °F (est.)	3.87	60°F (est.)
pH(10)	10.00	55 °F (est.)	10.00	60 °F (est.)
ORP Zobel Solution	240	55 F (est.)	240	60°F (est.)
Dissolved Oxygen 100% water saturated air mg/L	99.9%	55 F (est.)	99.5%	60 F (est.)
Dissolved Oxygen Zero Dissolved Oxygen Solution mg/L	NA	55 F (est.)	NA	60 F (est.)
Barometric Pressure mm Hg	NA	NA	NA	NA
Turbidity #1 (10 NTU)	NA	NA	NA	NA
Turbidity #2 (0.0 NTU)	NA	NA	NA	NA
Turbidity Standard #3	NA	NA	NA	NA

[¥]Specific conductance is outside of the post-calibration acceptance criteria. Values displayed on field purge logs may be biased low.

Project Name Parcel A3 Date 11/13/15 _____ Weather Sunny 60s Calibrated by N. Kurtz & L. Perrin Serial Number NA

Instrument YSI Meter

Parameters	Morning Calibration	Morning Temperature	End of Day Calibration Check	End of Day Temperature
Specific Conductance Standard #1	1.410	55 F (est.)	$1.186^{\text{¥}}$	57°F (est.)
Specific Conductance Standard #2	NA	NA	NA	NA
pH (7)	7.00	55 °F (est.)	NA^{Σ}	57 °F (est.)
pH (4)	3.87	55 °F (est.)	NA [¥]	57 °F (est.)
pH(10)	10.00	55 °F (est.)	9.87	57 °F (est.)
ORP Zobel Solution	240.0	55 F (est.)	$NA^{\mathbb{Y}}$	57 °F (est.)
Dissolved Oxygen 100% water saturated air mg/L	99.5%	55 F (est.)	NA^{F}	57 F (est.)
Dissolved Oxygen Zero Dissolved Oxygen Solution mg/L	NA	55 F (est.)	NA	57 F (est.)
Barometric Pressure mm Hg	NA	NA	NA	NA
Turbidity #1 (10 NTU)	NA	NA	NA	NA
Turbidity #2 (0.0 NTU)	NA	NA	NA	NA
Turbidity Standard #3	NA	NA	NA	NA

[¥]Specific conductance is outside of the post-calibration acceptance criteria. Postcalibration checks were not performed for DO, ORP, or pH (4 & 7). Values displayed on field purge logs may be inaccurate.

Project NameParcel A3DWeatherSunny 40sCalibrated byN. Kurtz & L. PerrinSerial NumberNA

Date 11/17/15

Instrument YSI Meter

Parameters	Morning Calibration	Morning Temperature	End of Day Calibration Check	End of Day Temperature
Specific Conductance Standard #1	$0.985^{\text{¥}}$	52 F (est.)	1.005 [¥]	55 F (est.)
Specific Conductance Standard #2	NA	NA	NA	NA
pH (7)	6.99	52°F (est.)	5.27 [¥]	55 °F (est.)
pH (4)	3.58	52 °F (est.)	-0.67 [¥]	55 °F (est.)
pH(10)	10.08	52°F (est.)	10.17	55 F (est.)
ORP Zobel Solution	240.0	52 °F (est.)	235.4	55 °F (est.)
Dissolved Oxygen 100% water saturated air mg/L	99.9%	52 F (est.)	100.8%	55 F (est.)
Dissolved Oxygen Zero Dissolved Oxygen Solution mg/L	NA	52 F (est.)	NA	55 F (est.)
Barometric Pressure mm Hg	NA	NA	NA	NA
Turbidity #1 (10 NTU)	NA	NA	NA	NA
Turbidity #2 (0.0 NTU)	NA	NA	NA	NA
Turbidity Standard #3	NA	NA	NA	NA

[¥]Specific conductance and pH < 10 are outside of the post-calibration acceptance criteria. Values displayed on field purge logs may be biased low.

APPENDIX H



Parcel A3 - IDW Drum Log Pre-Design Investigation

Drum ID	Designation	Activity/Phase	Contents	Open Date
5-N. Acid-9/15/15-A	Non-haz.	Area A	Nitric Acid	9/15/2015
6-Hexane-9/15/15-A	Hazardous	Area A	Hexane	9/15/2015
18-Liners-9/29/15-A3 (RWM)	Non-haz.	Parcel A3	Liners	9/29/2015
19-Decon Water-9/29/15-A3 (RWM)	Non-haz.	Parcel A3	Decon water	9/29/2015
20-PPE-9/30/15-A3 (RWM)	Non-haz.	Parcel A3	PPE	9/30/2015
21-Soil-10/8/15-A3 (RWM)	Non-haz.	Parcel A3	Soil	10/8/2015
22-Liners-10/8/15-A3 (RWM)	Non-haz.	Parcel A3	Liners	10/8/2015
29-Soil-10/1/15-A3 (RWM)	Non-haz.	Parcel A3	Soil	10/1/2015
RW-24-PZM(I) Soil	Non-haz.	Parcel A3	Soil	10/15/2015
31 RW 24-PZM(I) Soil	Non-haz.	Parcel A3	Soil	10/15/2015
32 RW 24-PZM(I) Soil	Non-haz.	Parcel A3	Soil	10/15/2015
33 RW 23-PZM(I) Soil	Non-haz.	Parcel A3	Soil	10/16/2015
34 RW 23-PZM(I) Soil	Non-haz.	Parcel A3	Soil	10/16/2015
RW22-PZM(I) Soil	Non-haz.	Parcel A3	Soil	10/21/2015
RW22-PZM(I) Soil	Non-haz.	Parcel A3	Soil	10/20/2015
RW-01-GB	Non-haz.	Parcel A3	Soil	10/22/2015
RW-01-GB	Non-haz.	Parcel A3	Soil	10/22/2015
RW-(22,23,24) PZM(I)	Non-haz.	Parcel A3	Purge water	10/22/2015
RW-02-GB	Non-haz.	Parcel A3	Soil	10/23/2015
RW-02-GB	Non-haz.	Parcel A3	Soil	10/23/2015
RW-03-GB	Non-haz.	Parcel A3	Soil	10/27/2015
RW-03-GB	Non-haz.	Parcel A3	Soil	10/27/2015
RW-03-GB	Non-haz.	Parcel A3	Soil	10/27/2015
RW-04-GB	Non-haz.	Parcel A3	Soil	10/29/2015



Drum ID	Designation	Activity/Phase	Contents	Open Date
RW-04-GB	Non-haz.	Parcel A3	Soil	10/29/2015
RW-04-GB	Non-haz.	Parcel A3	Soil	10/29/2015
61-Purge Water-11/4/15-A3	Hazardous	Parcel A3	Purge water	11/4/2015
66-DW-10/29/15-A	Non-haz.	Parcel A3	IDW Decon	10/29/2015
67-DW-10/29/15-A	Non-haz.	Parcel A3	IDW Decon	10/29/2015
68-DW-10/29/15-A	Non-haz.	Parcel A3	IDW Decon	10/29/2015
78-Purge water-11/16/15-A3	Non-haz.	Parcel A3	Purge water	11/16/2015
91-PPE-11/11/15-A3	Non-haz.	Parcel A3	PPE	11/11/2015
93-Dec Water-11/11/15-A3	Non-haz.	Parcel A3	Decon water	11/11/2015



APPENDIX I

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(Electronic Attachment)

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CRRGP F KZ'L''

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*Grgevt qple'Cvcej o gpv+

CRRGP F KZ'M'

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*Grgevt qple'Cvcej o gpv+

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APPENDIX L

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(Electronic Attachment)

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APPENDIX M

Table M-1 EnviroAnalytics Group - Area A Parcel A3 ARM Project No: 150298-13-3 Aquifer Testing - Slug Tests

			Total		Screen			Recovery In		C	onductivity	(К)	
Well Name:	Field ID:	Zone	Depth (ft bgs)	Screened Interval (ft bgs)	length (ft)	Well Casing Diameter (in)	Borehole Diameter (in)	Screen Interval?	Falling Head (ft/sec)	Falling Head (ft/day)	Rising Head (ft/sec)	Rising Head (ft/day)	Average K (ft/day)
RW01-PZM020	RW-1	Intermediate	29.51	24.51-29.51	5	2	10.25	No	4.86E-05	4.20	6.97E-05	6.02	5.11
RW02-PZM000	RW-2S	Shallow	9.75	4.75-9.75	5	2	10.25	No	7.06E-05	6.10	4.19E-05	3.62	4.86
RW02-PZM020	RW-2D	Intermediate	29.93	24.93-29.93	5	2	10.25	No	3.63E-04	31.38	3.23E-04	27.89	29.64
RW03-PZM003	RW-3	Shallow	13.87	8.87-13.87	5	2	10.25	No	3.22E-06	0.28	1.11E-06	0.10	0.19
RW04-PZM003	RW-4	Shallow	13.98	8.98-13.98	5	2	10.25	No	6.56E-06	0.57	5.21E-06	0.45	0.51
RW05-PZP001	RW-5	Shallow	9.67	4.67-9.67	5	2	10.25	No	4.12E-05	3.56	4.14E-05	3.58	3.57
RW06-PZM001	RW-6	Shallow	8.32	3.32-8.32	5	2	10.25	No	1.38E-04	11.91	1.13E-04	9.78	10.84
RW07-PZM004	RW-7S	Shallow	13.66	3.66-13.66	10	2	10.25	YES	2.98E-05	2.58	1.61E-05	1.39	1.99
RW07-PZM017	RW-7D	Intermediate	29.87	24.87-29.87	5	2	10.25	No	2.65E-04	22.90	2.90E-04	25.03	23.97
RW08-PZM003	RW-8	Shallow	14.28	9.28-14.28	5	2	10.25	No	1.55E-07	0.01	1.53E-07	0.01	0.01
RW09-PZM004	RW-9	Shallow	12.29	2.29-12.29	10	2	10.25	YES	1.73E-04	14.96	1.53E-04	13.18	14.07
RW10-PZM004	RW-10S	Shallow	13.84	3.84-13.84	10	2	10.25	No	2.86E-05	2.47	1.96E-05	1.69	2.08
RW10-PZM020	RW-10I	Intermediate	30.57	20.57-30.57	10	4	10.25	NA	Соор	er- Jacob Str	aight Line M	ethod	12.1
RW10-PZM065	RW-10D	Deep	74.97	69.97-74.97	5	2	10.25	No	1.50E-04	12.97	1.66E-04	14.37	13.67
RW11-PZM004	RW-11	Shallow	13.72	3.75-13.72	10	2	10.25	YES	9.61E-05	8.30	6.44E-05	5.57	6.93
RW12-PZM004	RW-12	Shallow	13.57	3.57-13.57	10	2	10.25	YES	9.04E-05	7.81	5.52E-05	4.77	6.29
RW13-PZM020	RW-13	Intermediate	30.05	25.05-30.05	5	2	10.25	No	3.63E-04	31.33	3.10E-04	26.76	29.05
RW14-PZM020	RW-14	Intermediate	29.58	24.58-29.58	5	2	10.25	No	2.50E-04	21.57	1.78E-04	15.34	18.45
RW15-PZM020	RW-15	Intermediate	29.21	19.21-29.21	10	4	10.25	NA	Соор	er- Jacob Str	aight Line M	ethod	7.11
RW16-PZM020	RW-16	Intermediate	29.64	24.64-29.64	5	2	10.25	No	1.91E-04	16.49	1.42E-04	12.25	14.37
RW17-PZM019	RW-17	Intermediate	29.65	24.65-29.65	5	2	10.25	No	4.38E-04	37.84		-	37.84
RW18-PZM047	RW-18D	Deep	60.55	55.55-60.55	5	2	10.25	No	3.40E-08	0.003	1.97E-07	0.017	0.003
RW19-PZM020	RW-19I	Shallow	29.21	24.21-29.21	5	4	10.25	No	9.10E-04	78.64	7.66E-04	66.17	72.41
RW19-PZM050	RW-19D	Deep	59.33	54.33-59.33	5	2	10.25	No	5.49E-07	0.05	1.84E-07	0.02	0.05
RW19-PZP003	RW-19S	Shallow	9.56	4.56-9.56	5	2	10.25	YES	5.03E-04	43.49	5.29E-04	45.73	44.61
RW20-PZP000	RW-20S	Shallow	10.62	5.62-10.62	5	2	10.25	YES	5.46E-05	4.71	3.35E-05	2.90	3.81
RW20-PZM020	RW-201	Intermediate	32.86	22.86-32.86	10	2	10.25	No	1.31E-06	0.11	2.63E-06	0.23	0.17
RW20-PZM050	RW-20D	Deep	57.85	52.85-57.85	5	2	10.25	No	5.80E-06	0.50	1.35E-06	0.12	0.31
RW21-PZM023	RW-21	Intermediate	33.18	28.18-33.18	5	2	10.25	No	2.73E-05	2.36	1.02E-04	8.81	5.59
RW-22(I)	RW-22(I)	Intermediate	34.00	29.00-34.00	5	2	8.25	No	1.62E-04	14.04	2.6E-04	22.18	18.11
RW-22-PZM	RW-22-PZM	Shallow	19.50	9.50-19.50	10	2	8.25	NA		Not te	sted - LNAPL	in well	
RW-23(I)	RW-23(I)	Intermediate	36.00	26.00-36.00	10	2	8.25	No	1.93E-04	16.64	1.27E-04	10.94	13.79
RW23-PZM	RW23-PZM	Shallow	20.00	10.00-20.00	10	2	8.25	No	5.53E-05	4.78	5.59E-05	4.83	4.80
RW-24(I)	RW-24(I)	Intermediate	28.00	23.00-28.00	5	2	8.25	No	1.53E-04	13.22	1.26E-04	10.93	12.08
RW24-PZM	RW24-PZM	Shallow	20.00	10.00-20.00	10	2	8.25	No	1.28E-05	1.11	1.41E-05	1.22	1.16
RW-RW89	RW-RW89	Shallow	14.40	9.40-14.40	5	2	10.25	No	1.46E-06	0.13	1.90E-06	0.16	0.15
RW-RW90	RW-RW90	Shallow	13.80	8.80-13.80	5	2	10.25	No	1.28E-06	0.11	5.24E-06	0.45	0.28
RW-RW93	RW-RW93	Shallow	9.43	4.43-9.43	5	2	10.25	No	1.28E-05	1.10	1.78E-05	1.54	1.32
RW-RW95	RW-RW95	Shallow	9.95	4.95-9.95	5	2	10.25	No	3.03E-05	2.62	3.67E-05	3.17	2.89
RW-RW97	RW-RW97	Shallow	14.67	9.67-14.67	5	2	10.25	No	1.09E-07	0.01	5.56E-07	0.05	0.03
TS04-PDM004	TS-04	Shallow	15.31	5.31-15.31	10	2	10.25	YES	2.79E-06	0.01	8.39E-06	0.03	0.48
1304-10101004	13-04	Shanow	13.31	2.21-12.21	10	۷	10.25	I LJ	2.791-00	0.24	0.391-00	0.75	0.40

"*" Cooper-Jacob Straight Line Method from pumping tests data used to calculate K

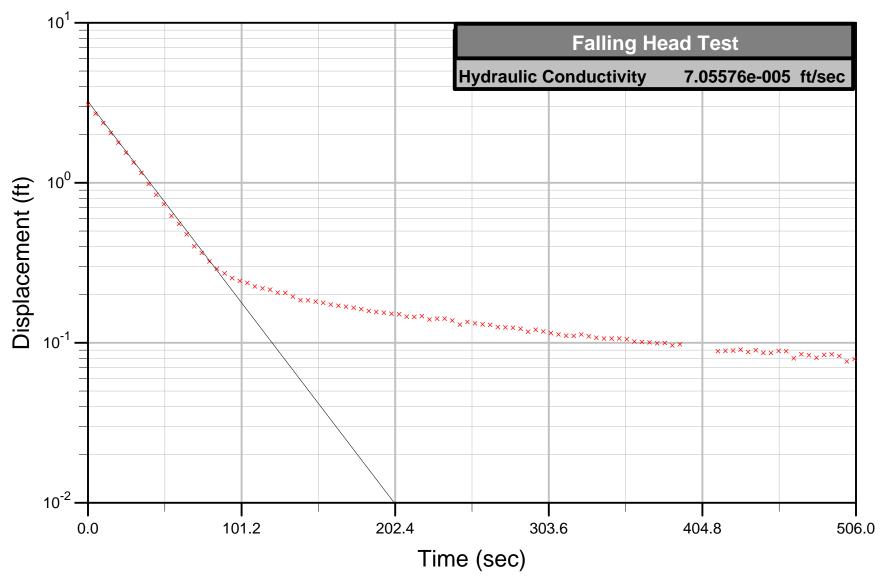
"-" data unusable - test proceeded too rapidly/turbulent

10.25" borehole diameter assumed - no well construction information available

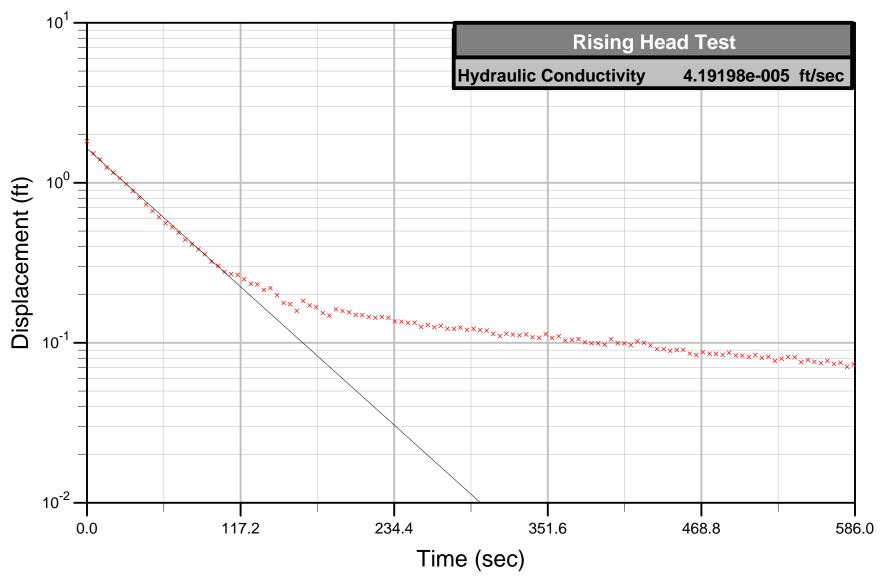
NA - not applicable

SHALLOW MONITORING WELLS

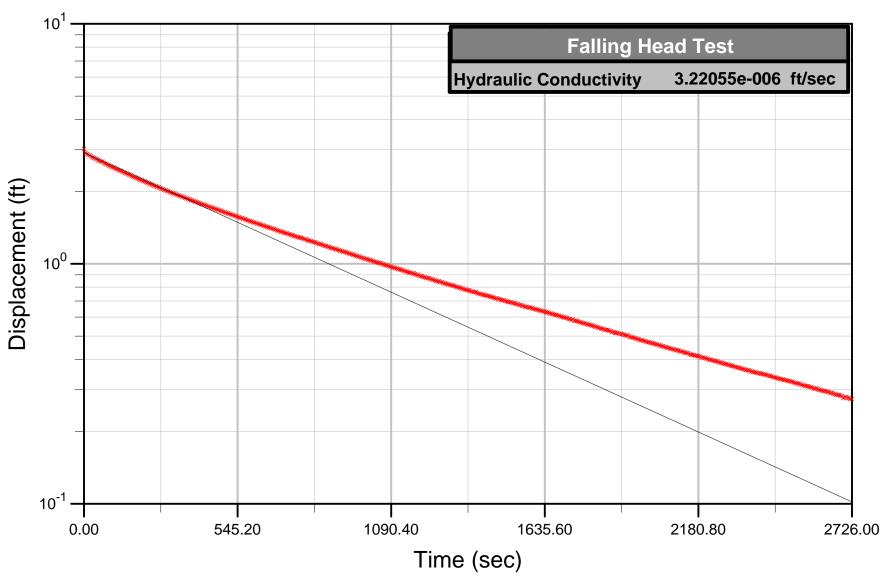
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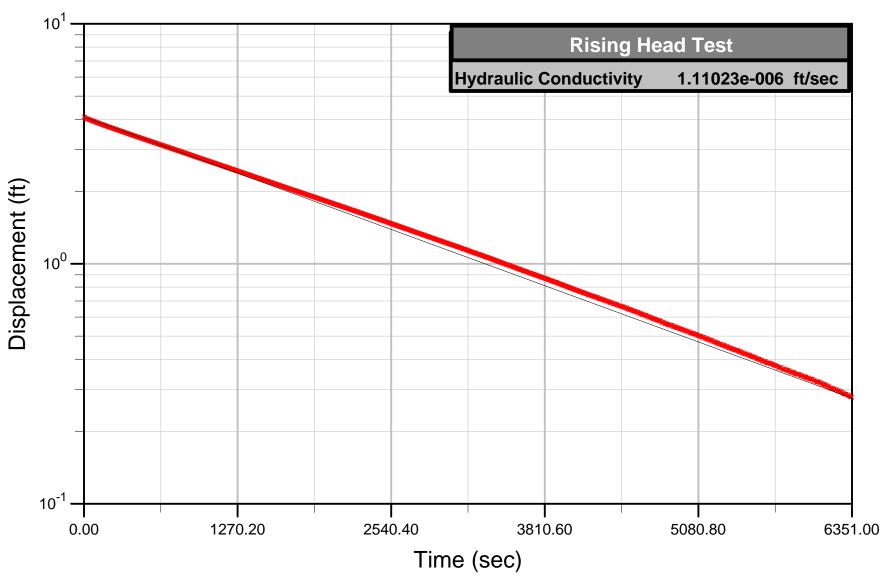
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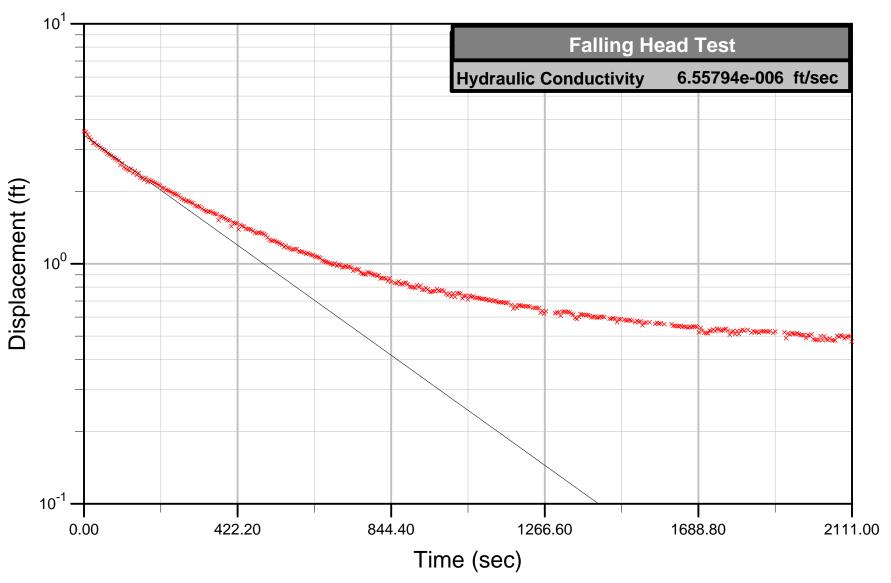
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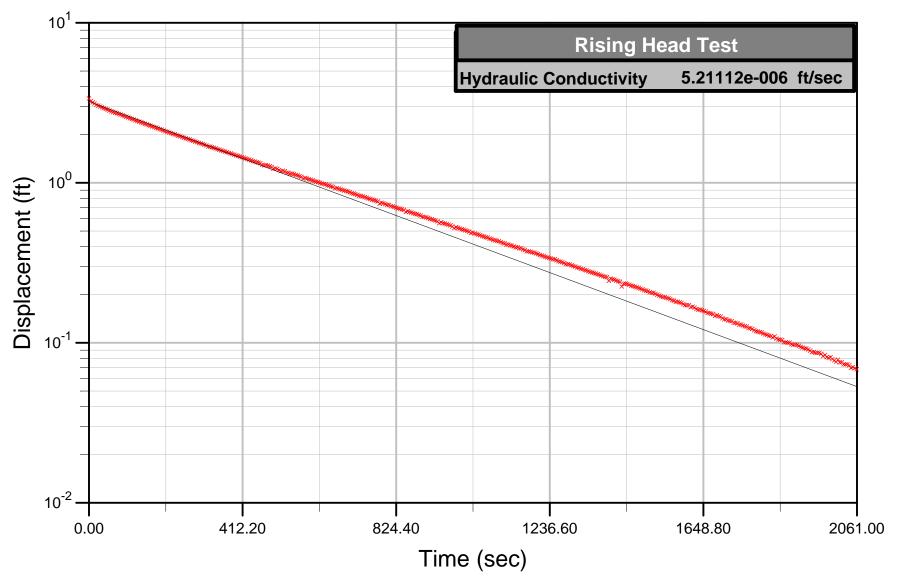
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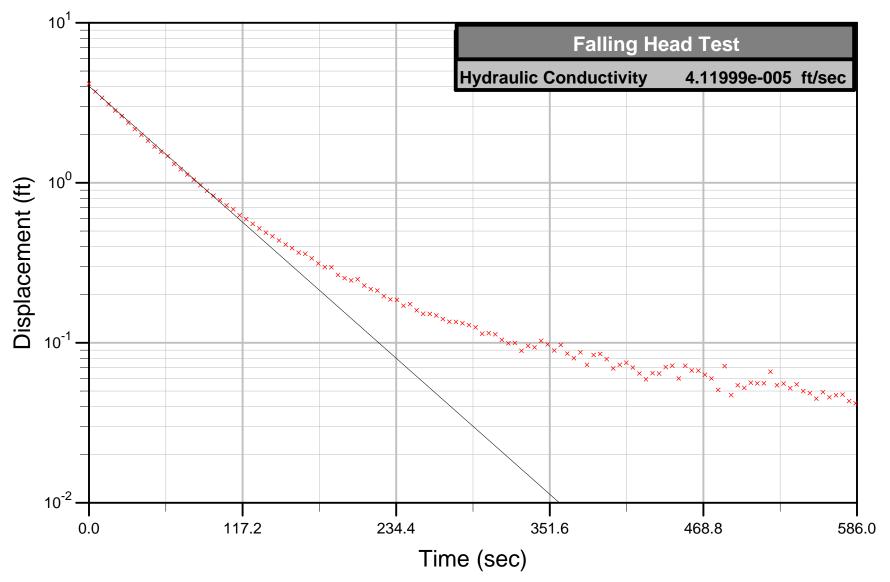
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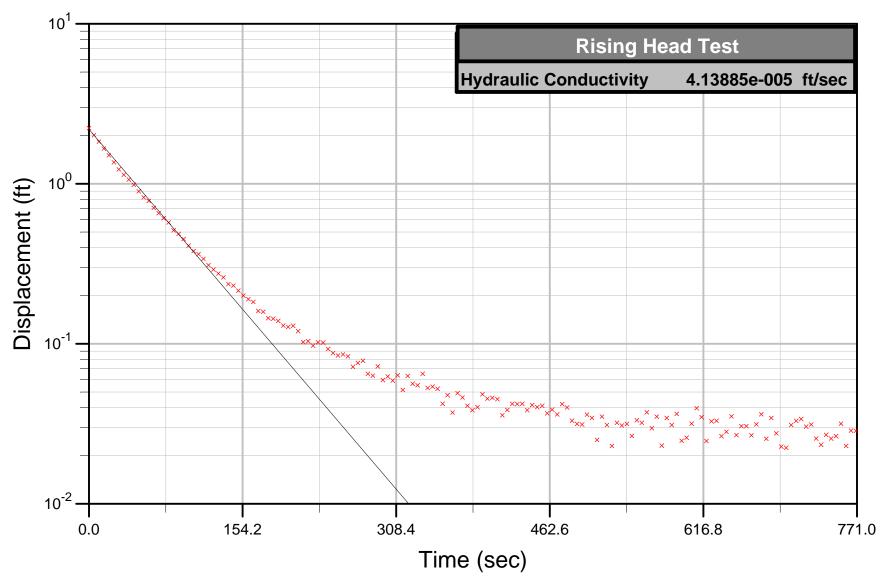
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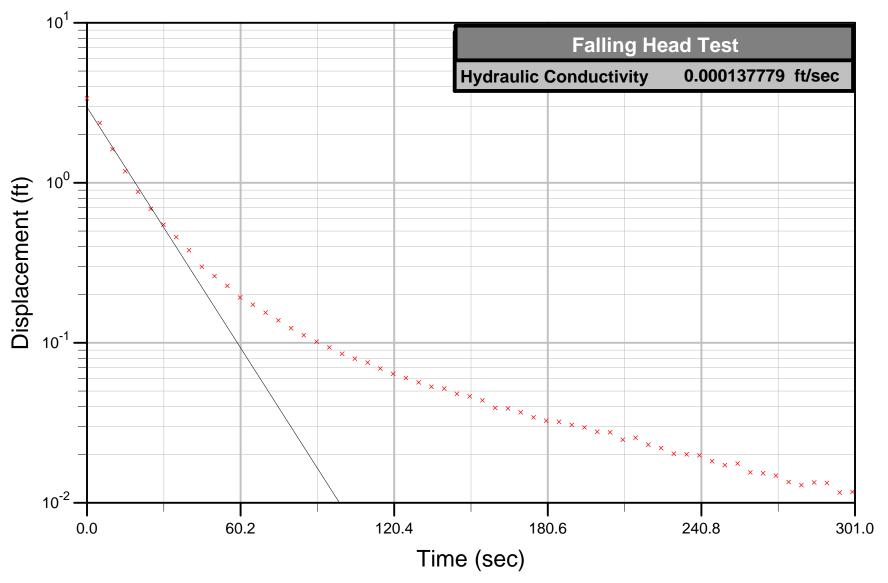
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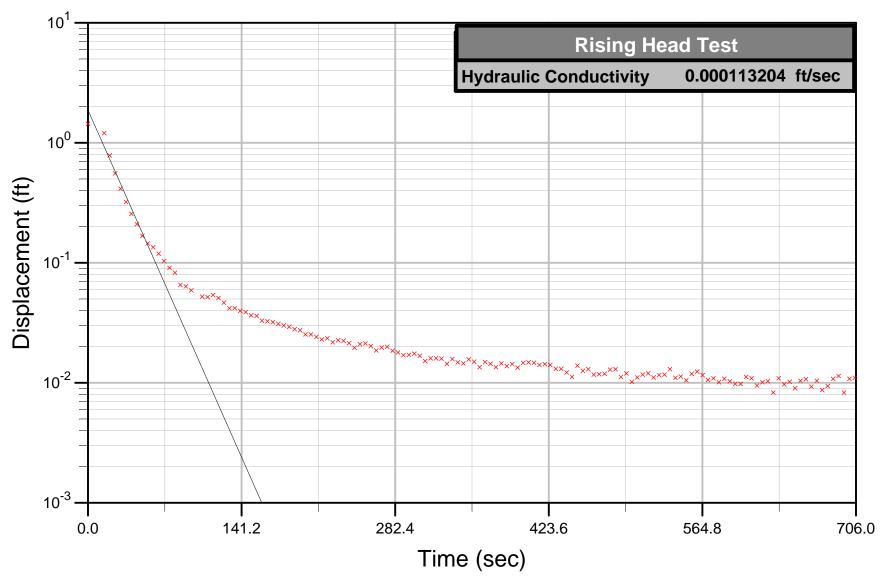
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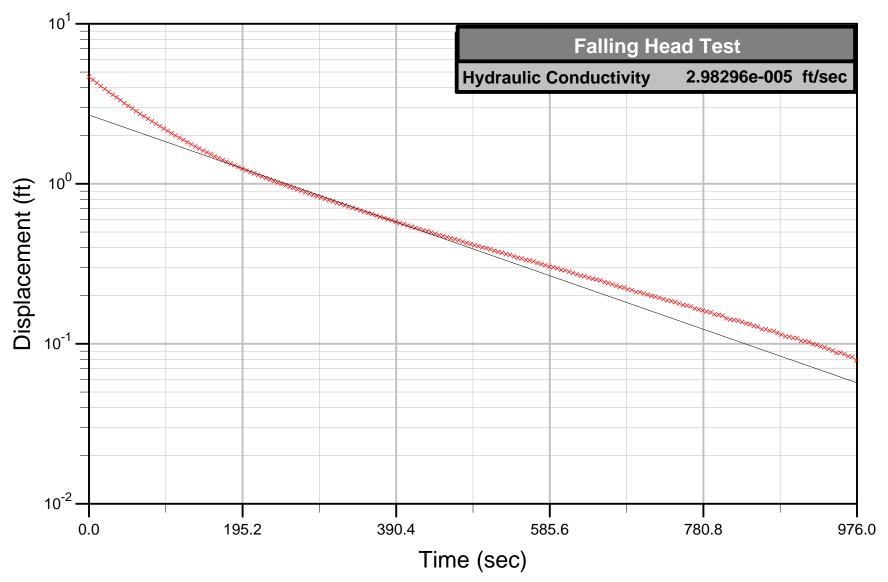
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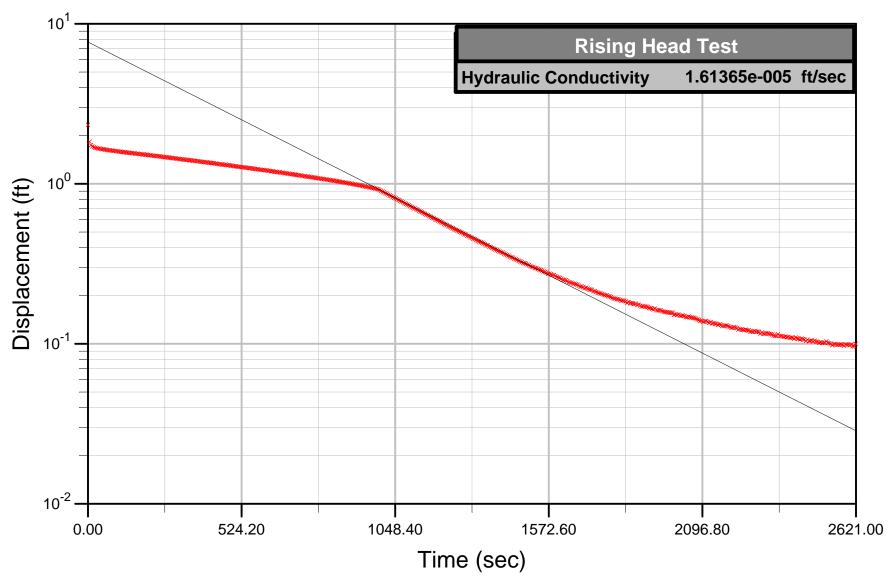
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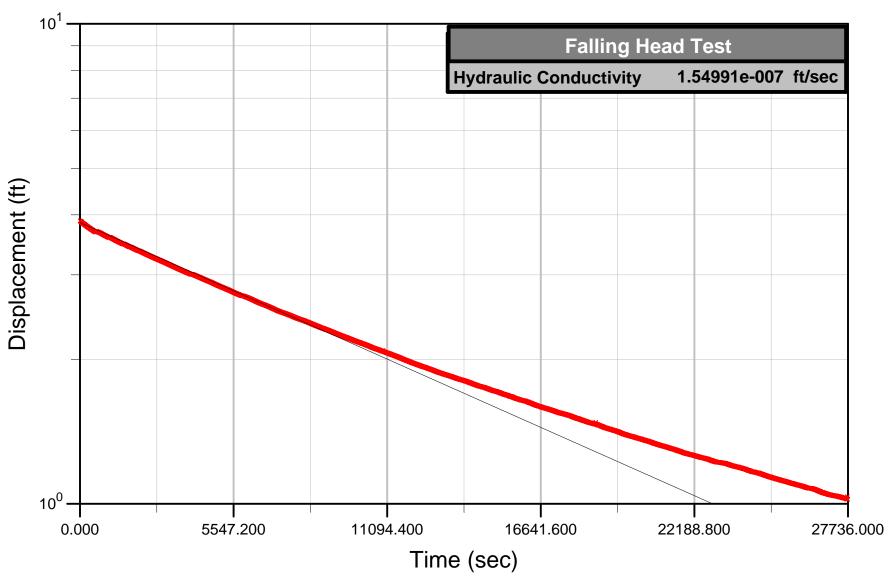
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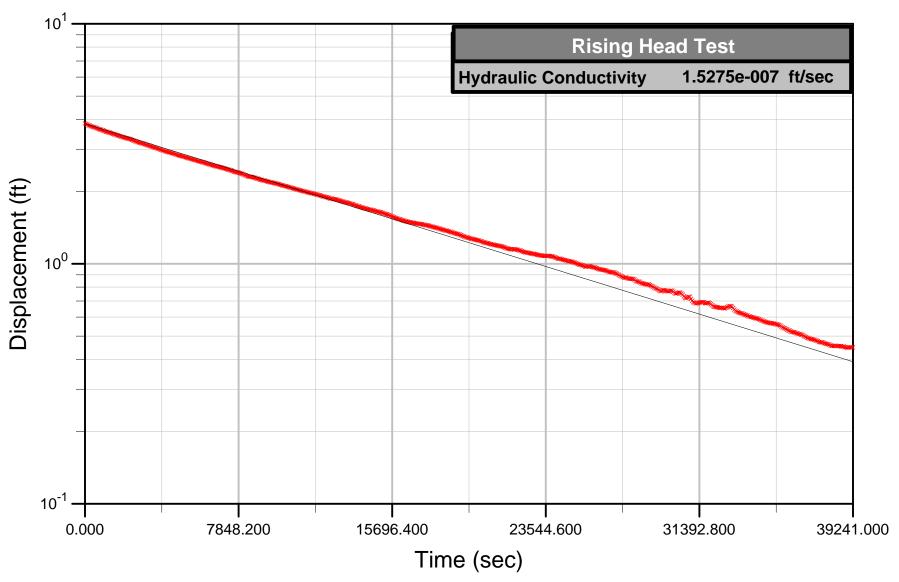
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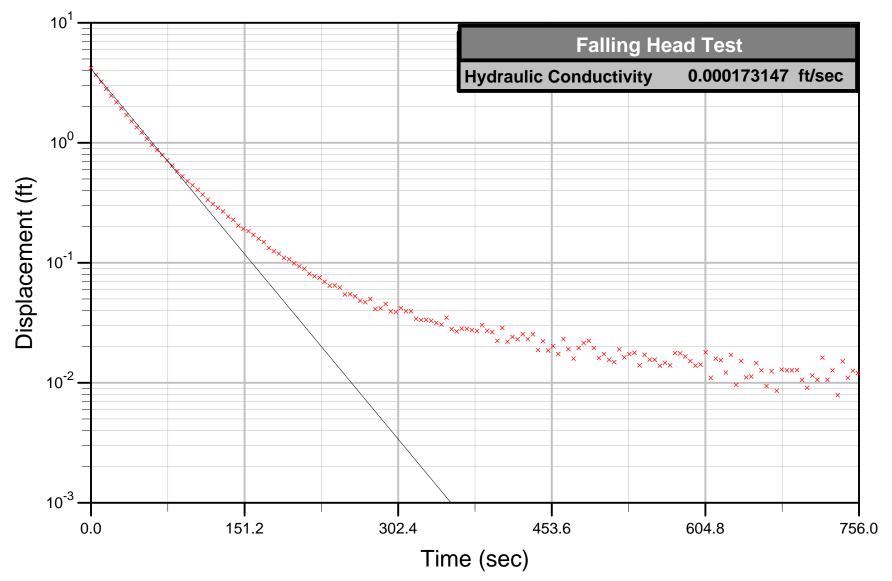
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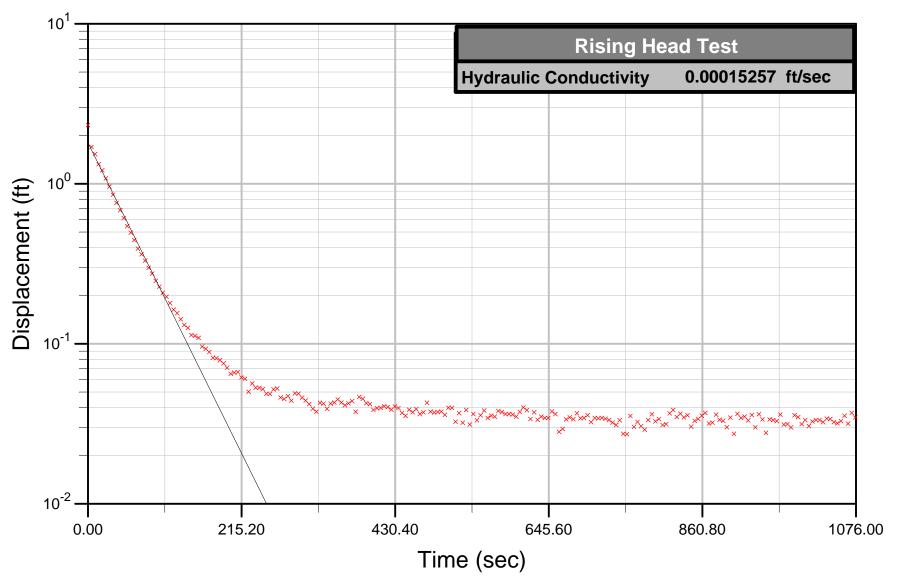
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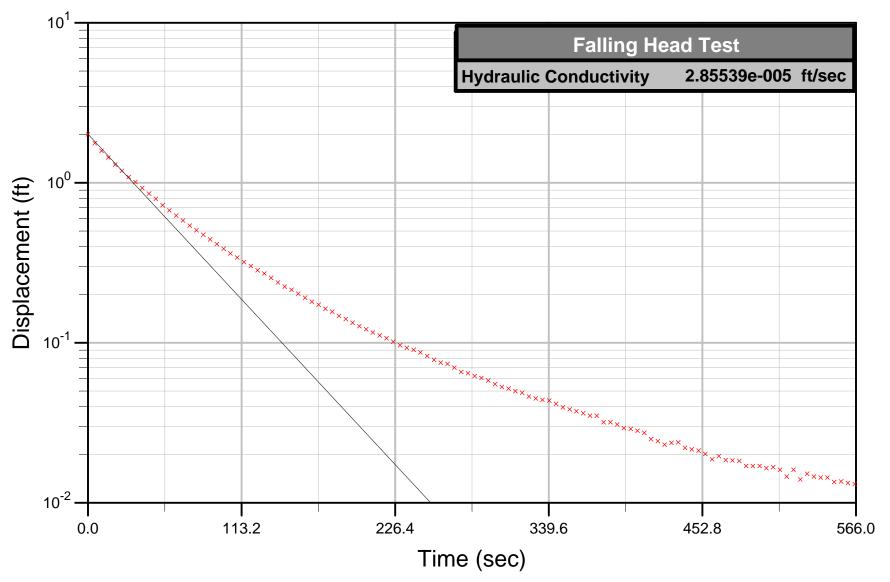
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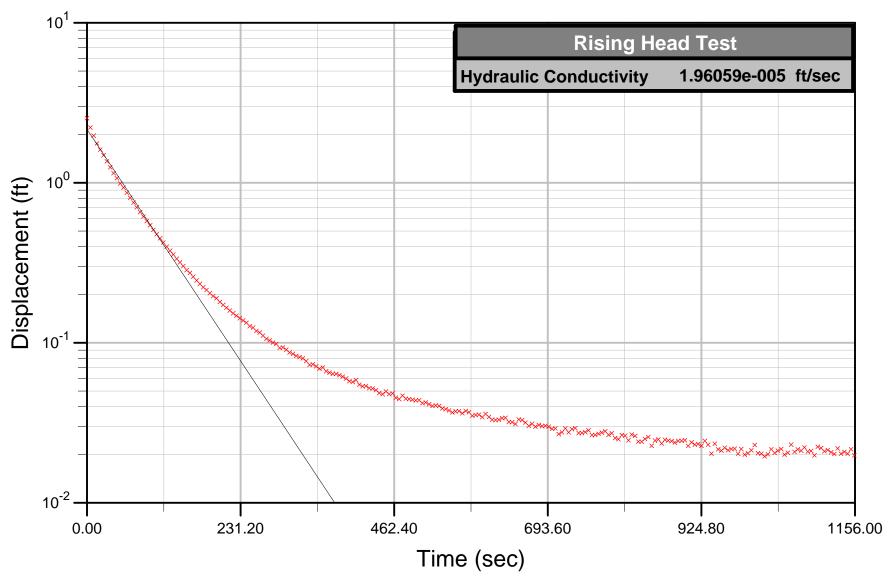
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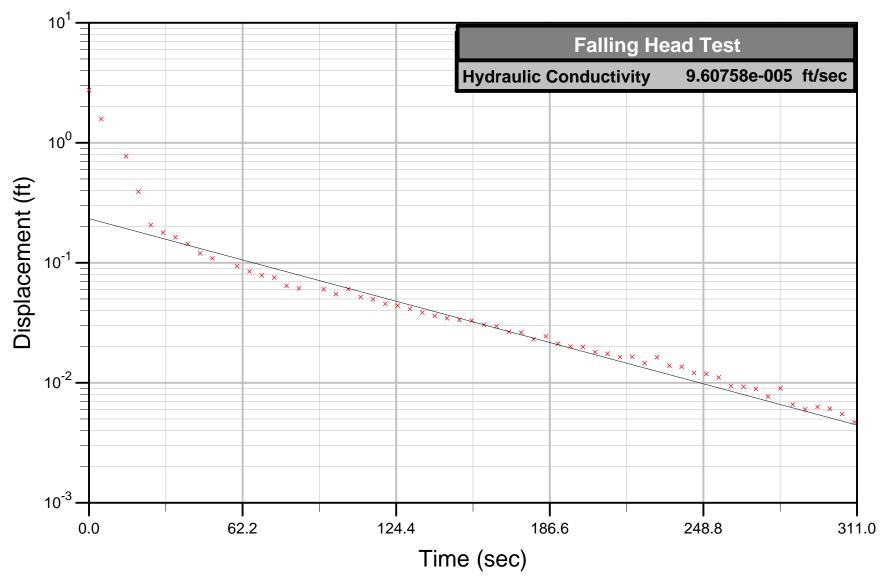
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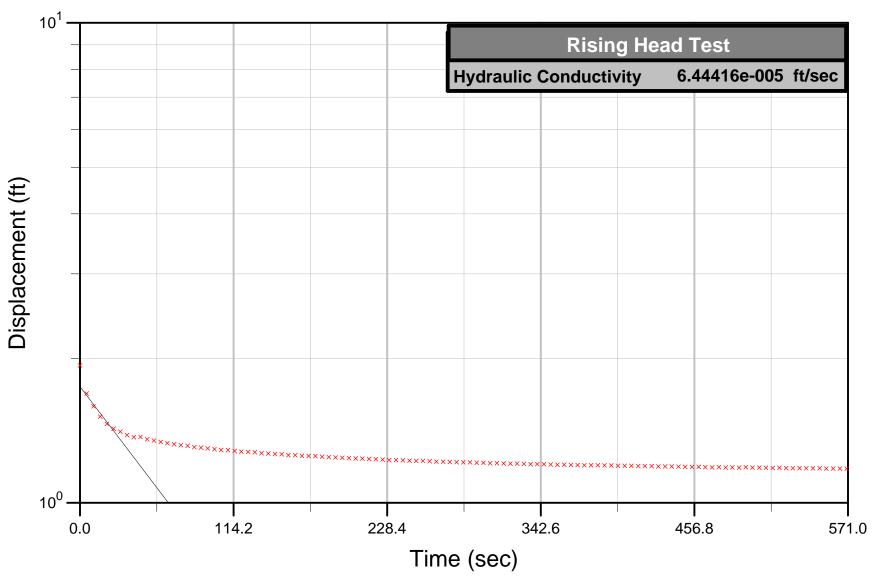
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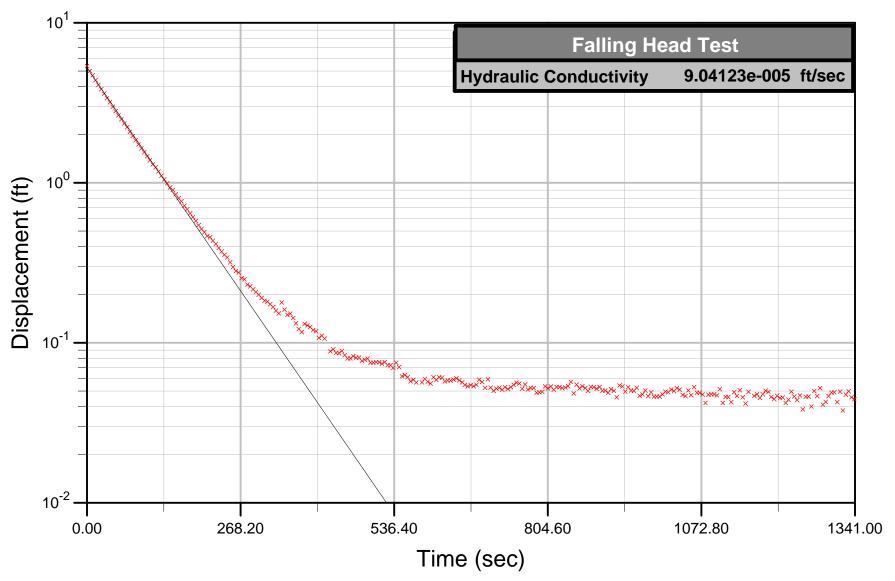
RW11-PZM004



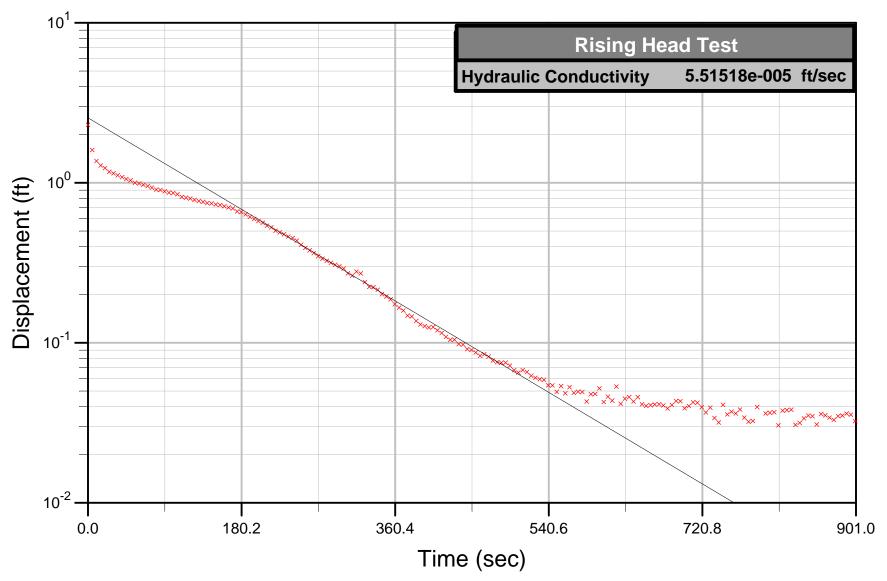
RW11-PZM004



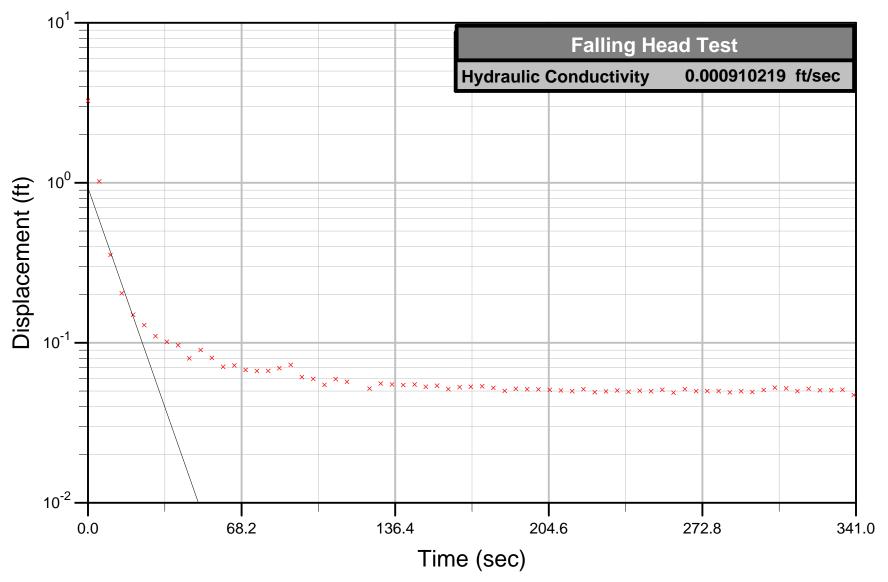
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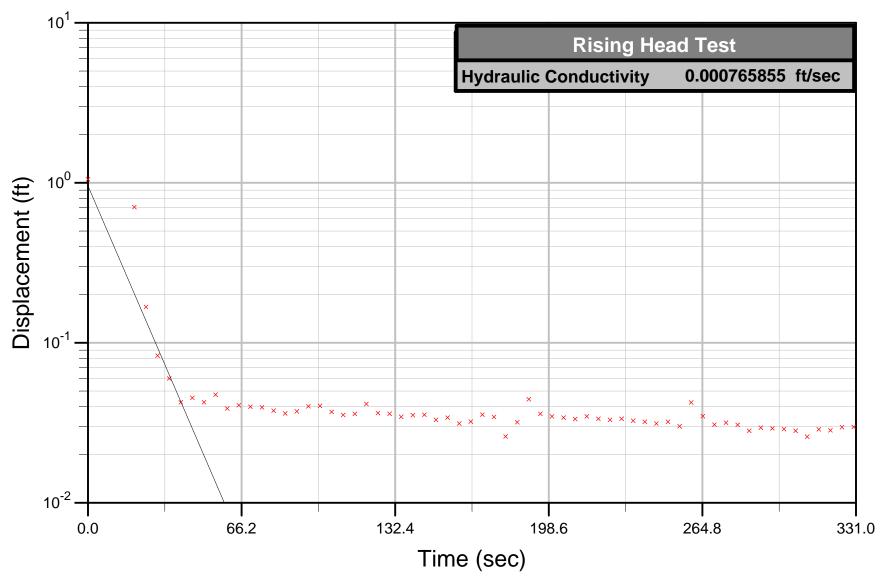
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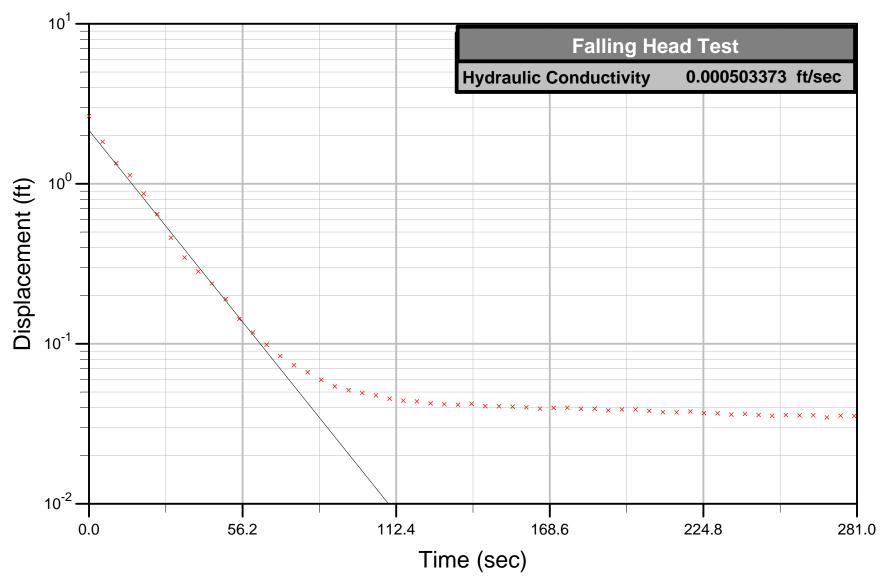
RW19-PZM020



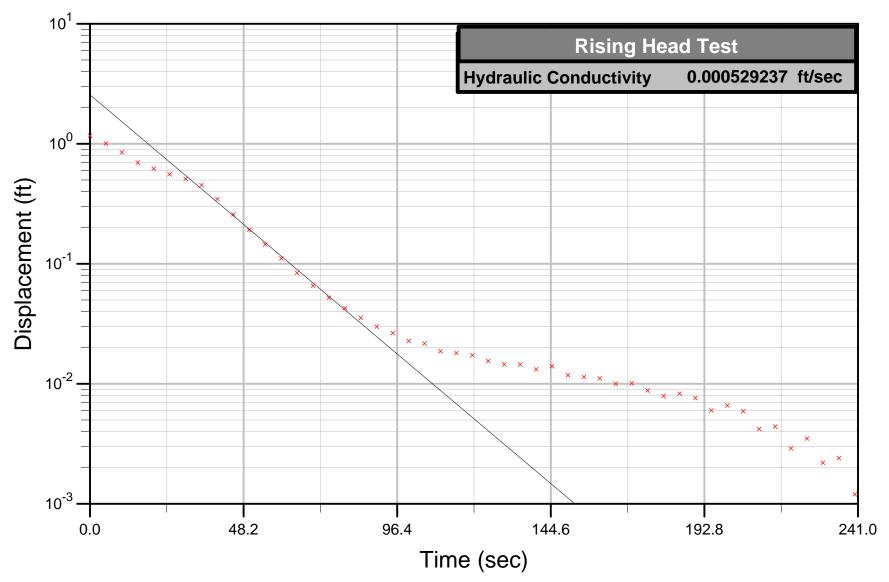
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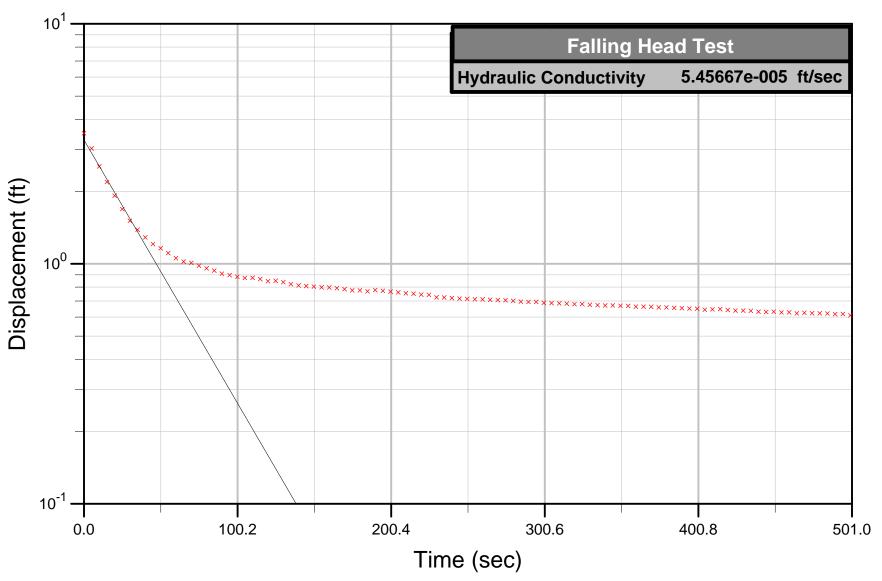
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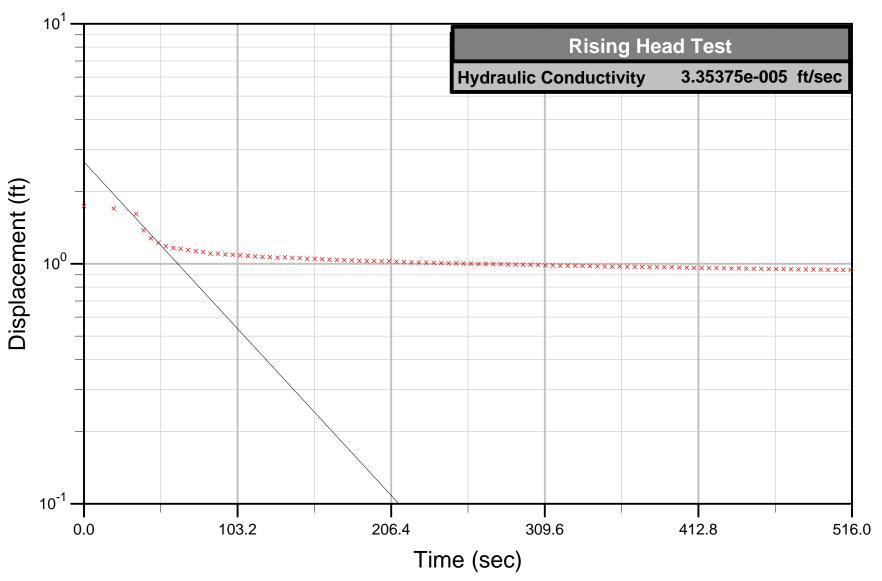
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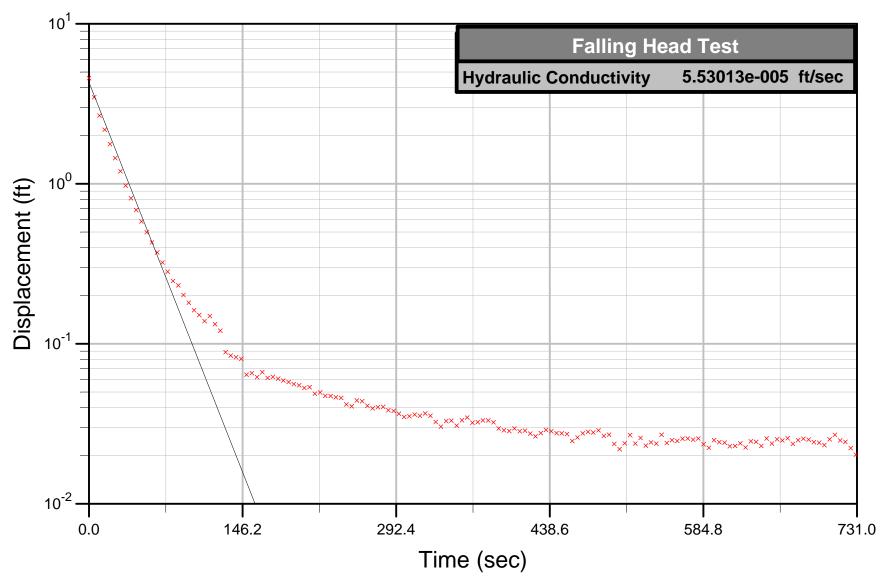
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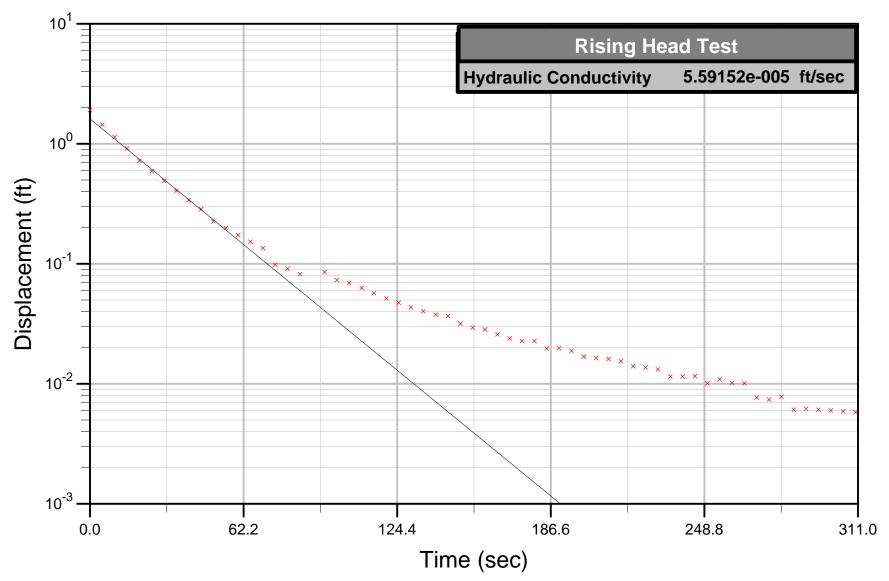
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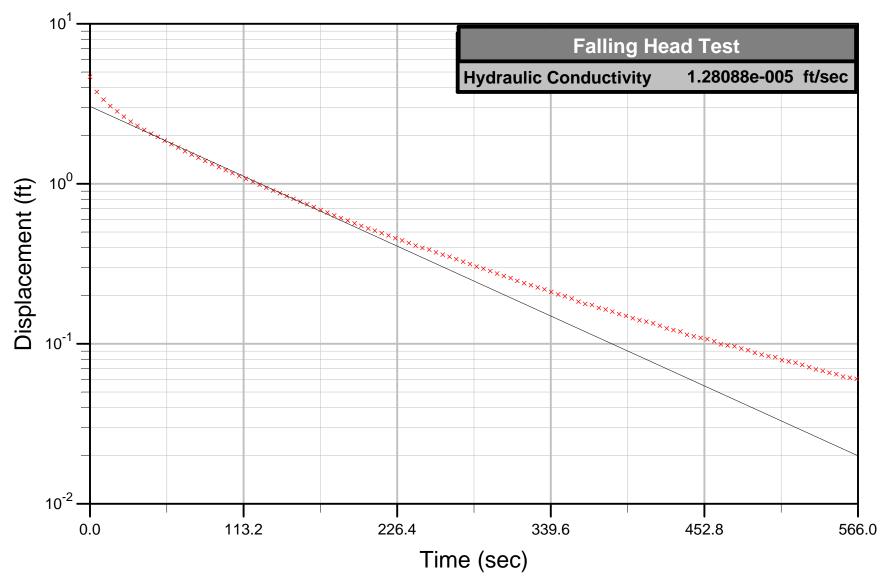
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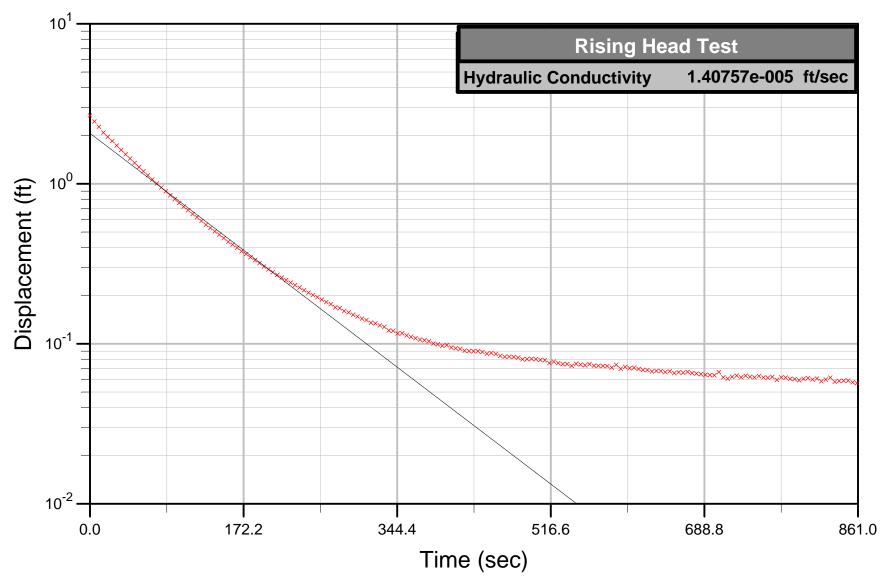
RW23-PZM

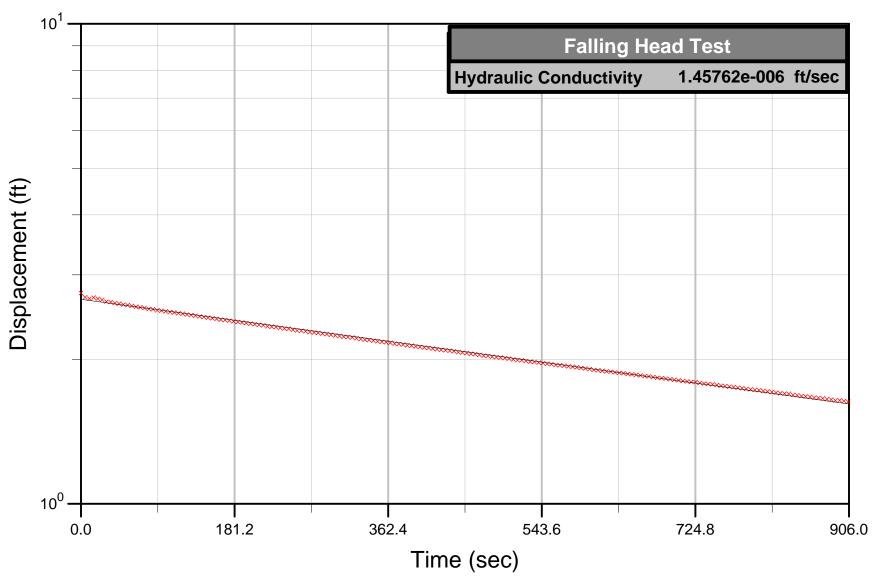


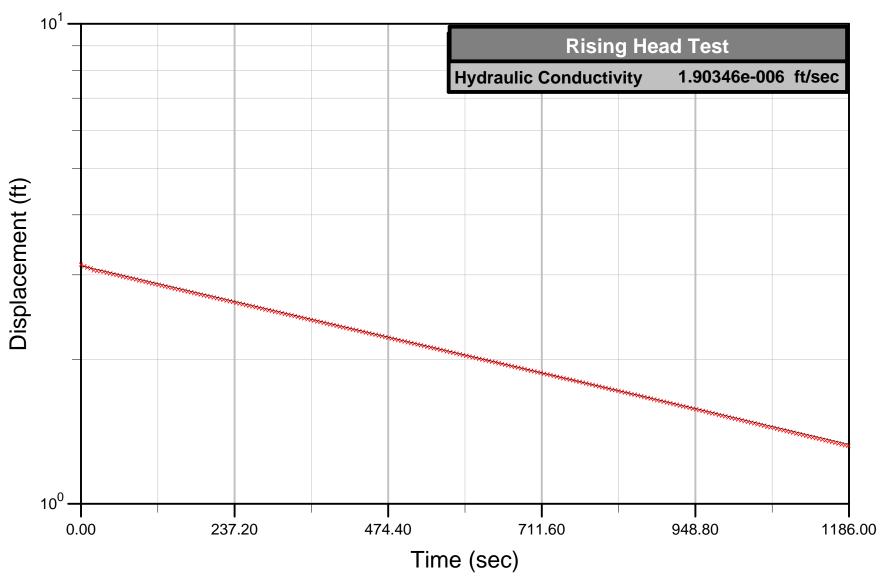
RW24-PZM

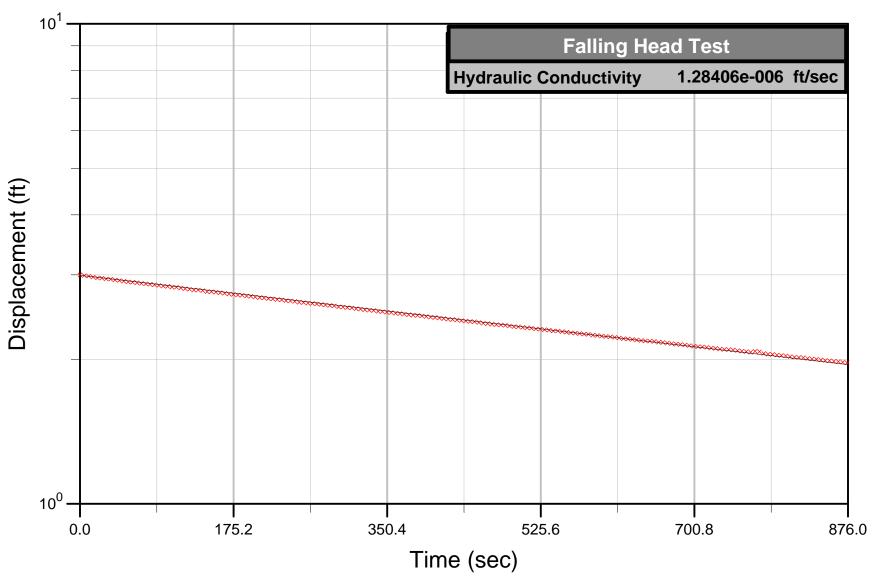


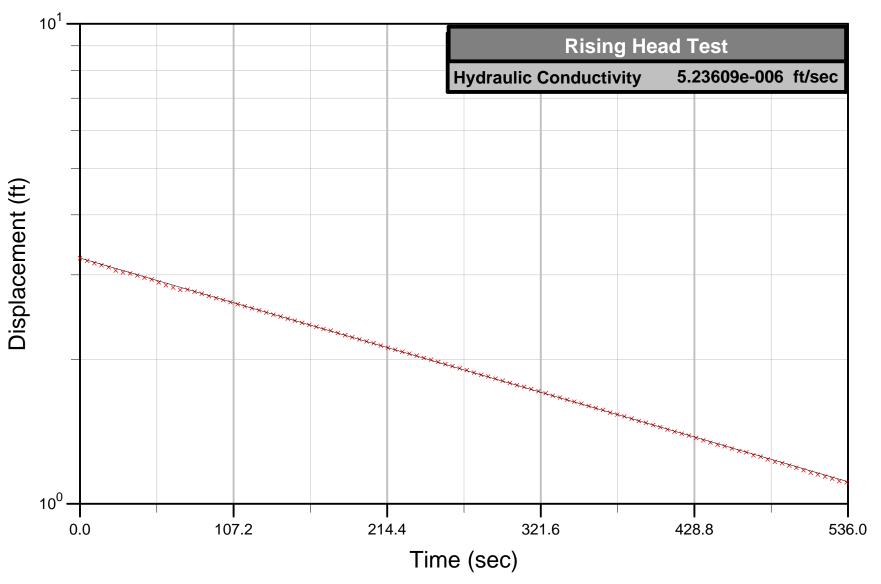
RW24-PZM

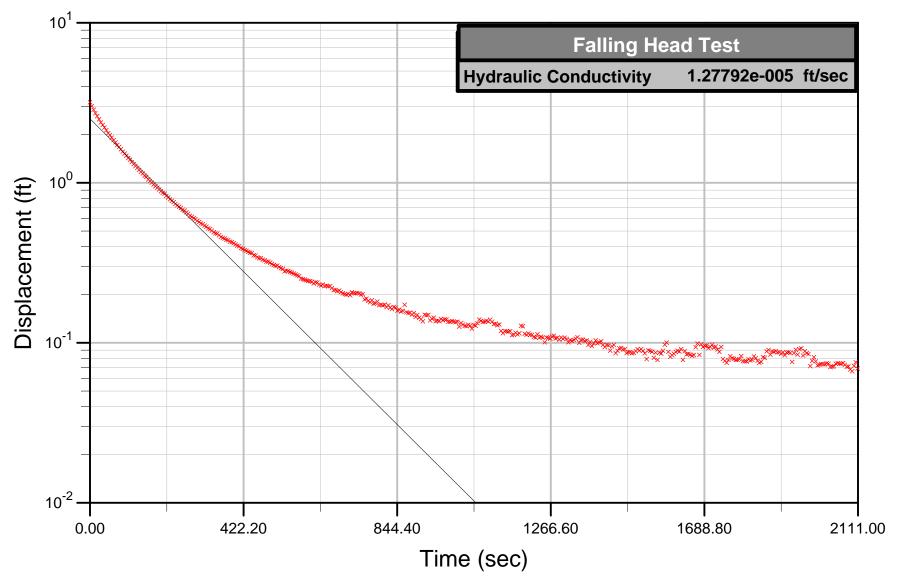


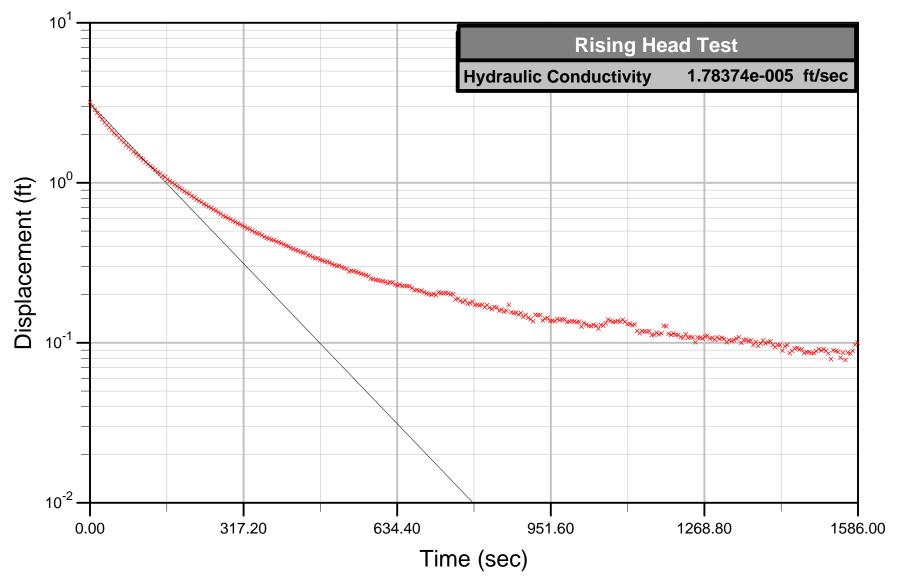


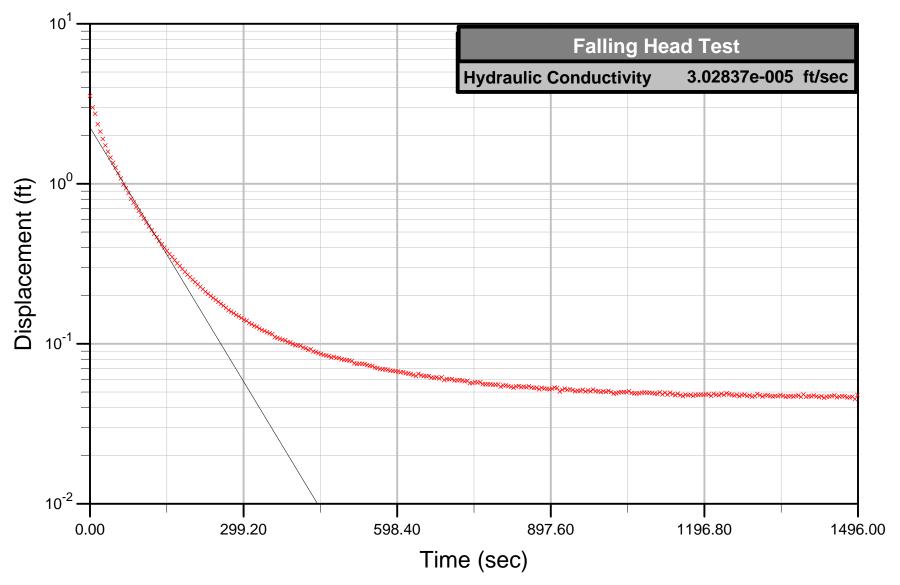


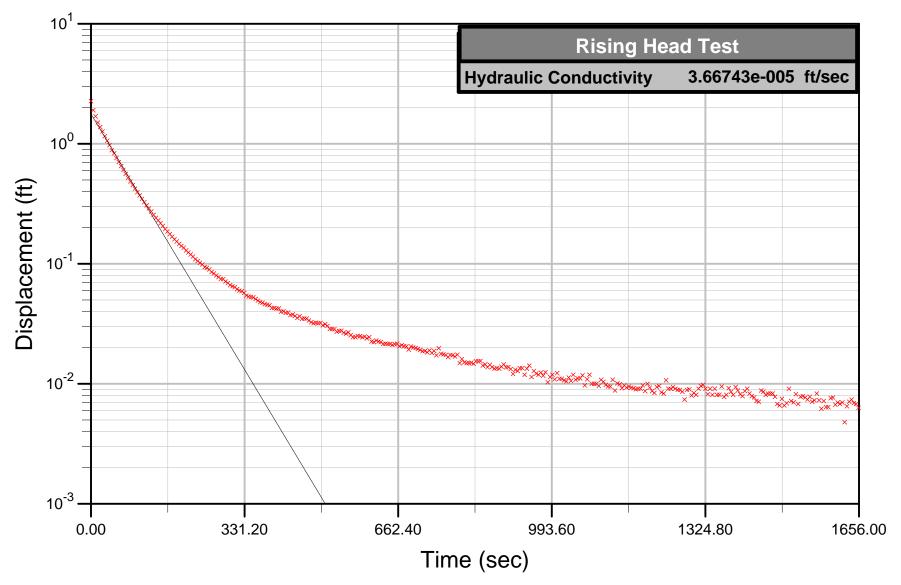


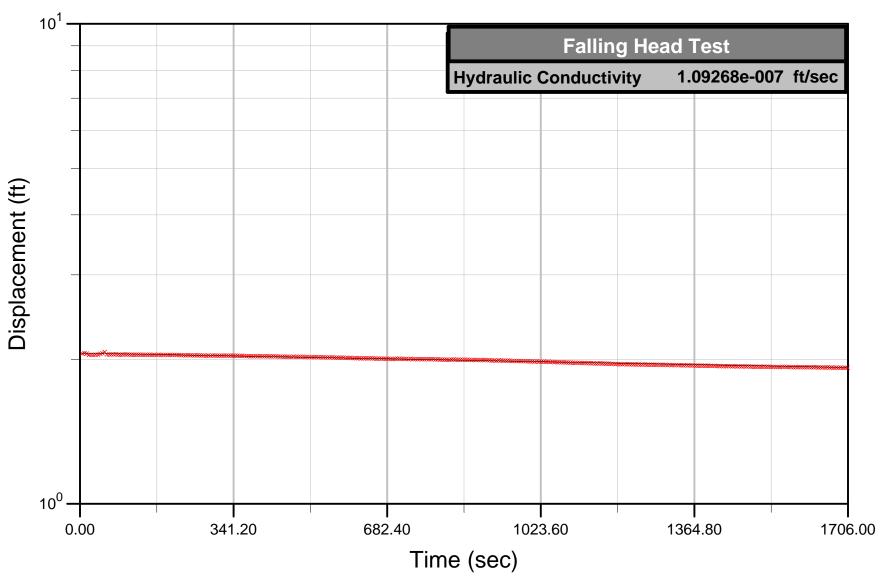


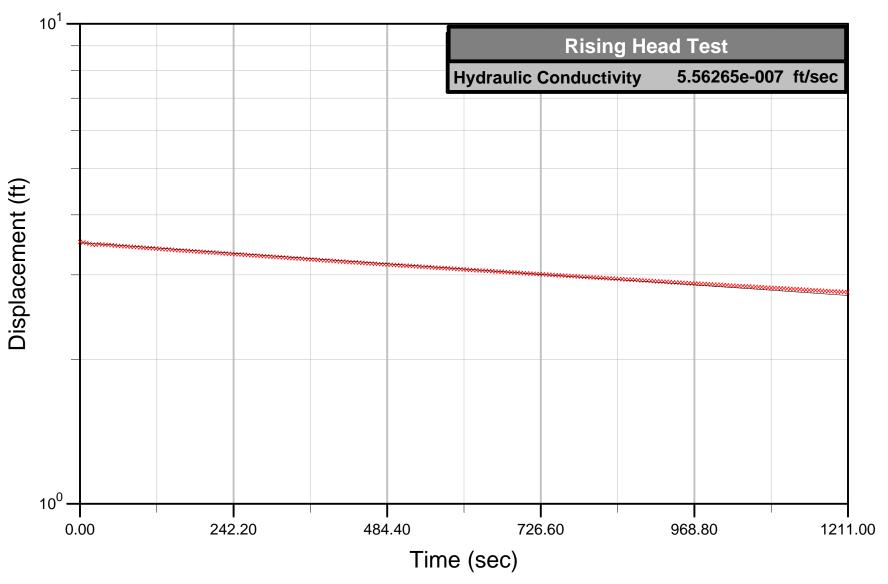




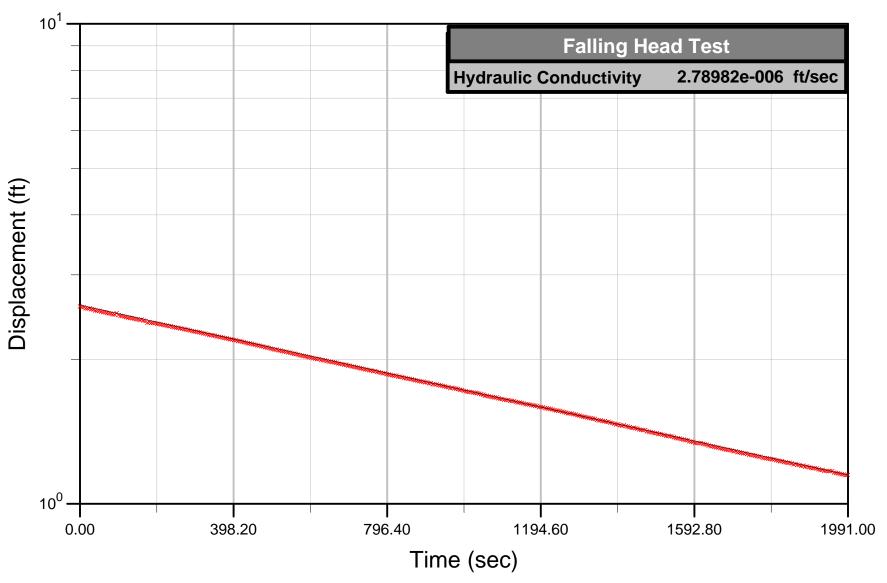




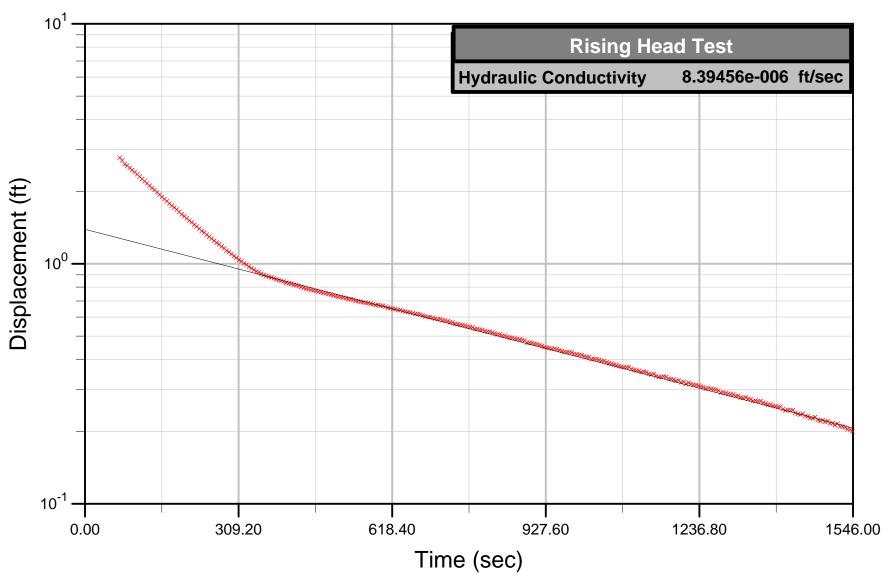




TS04-PDM004

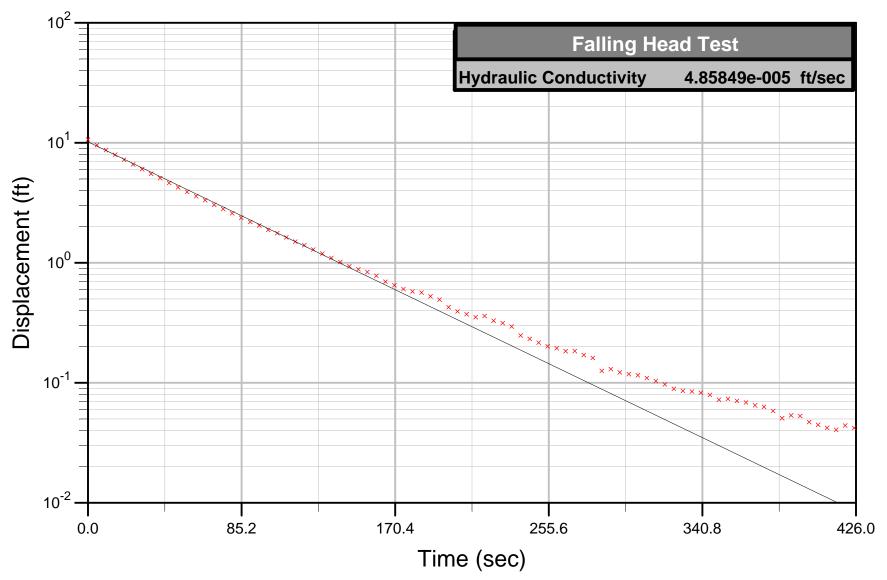


TS04-PDM004

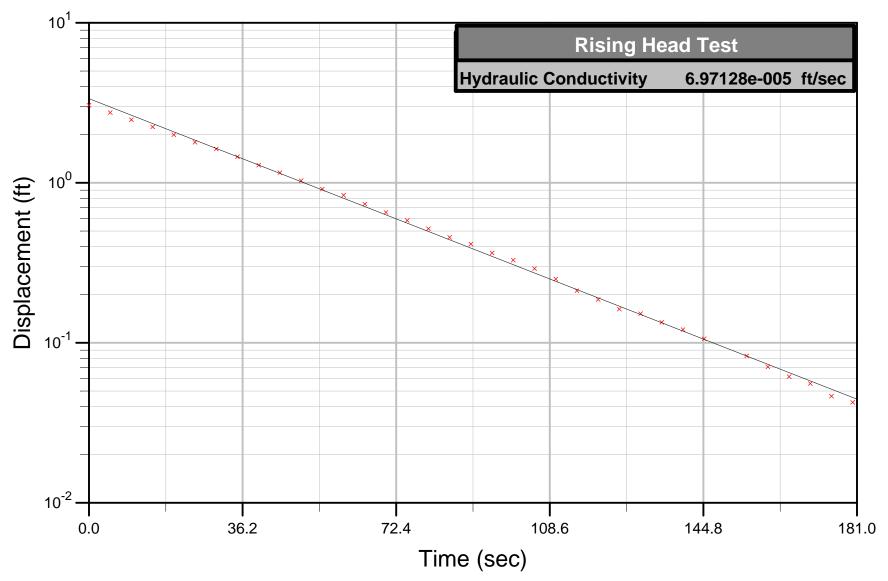


INTERMEDIATE MONITORING WELLS

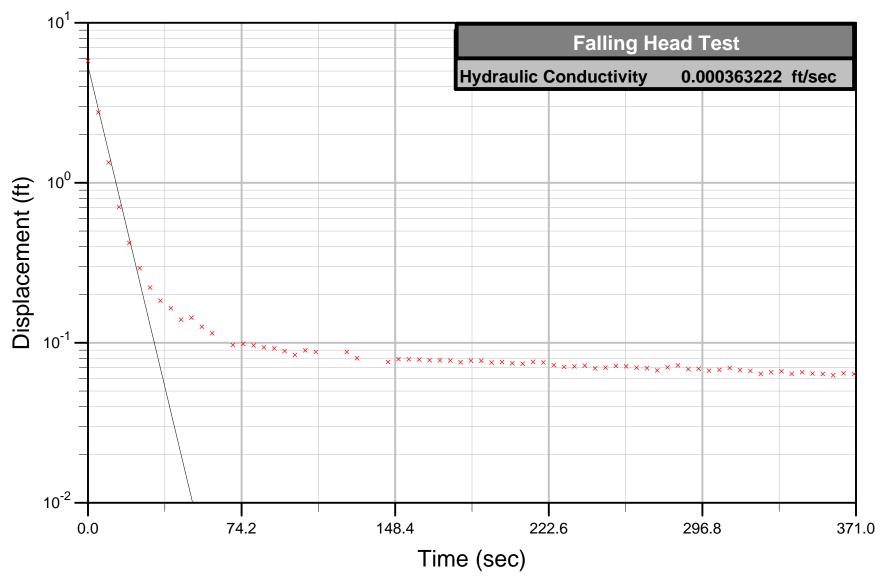
RW01-PZM020



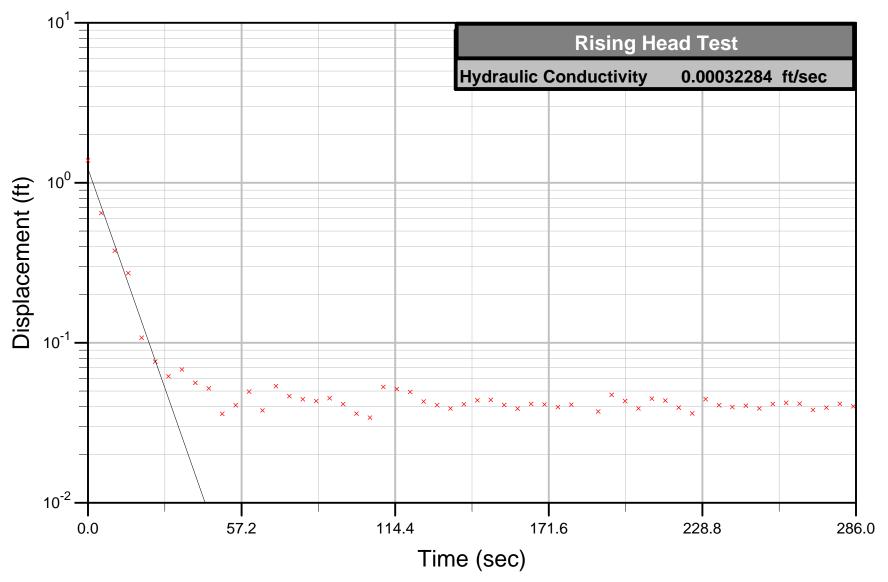
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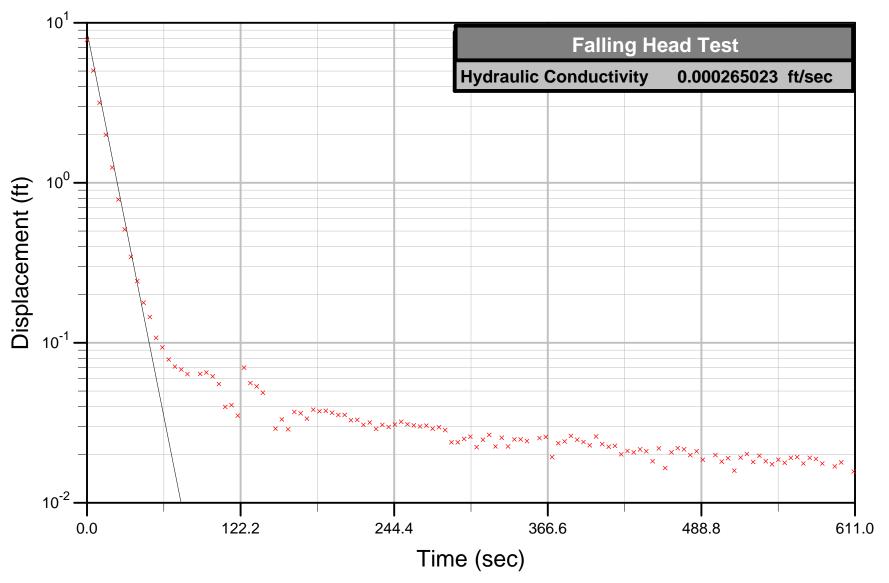
RW02-PZM020



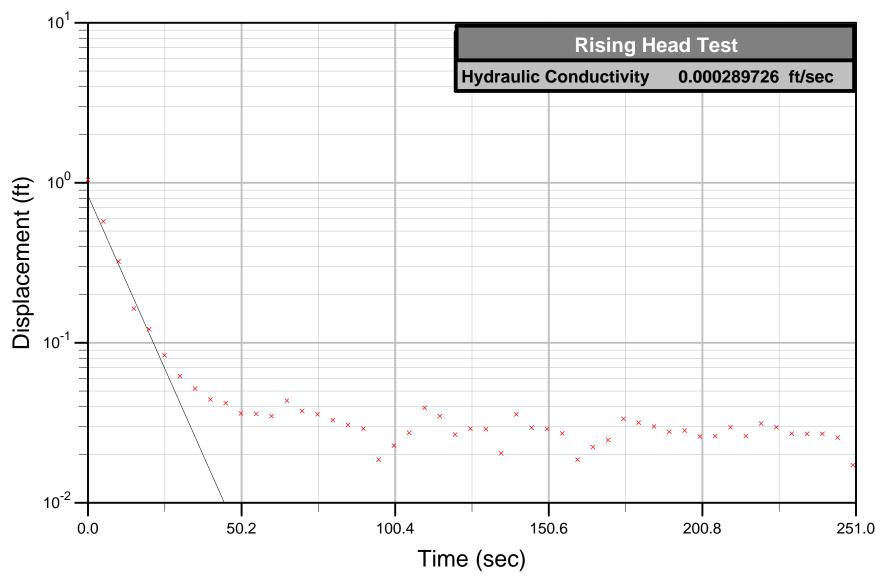
RW02-PZM020



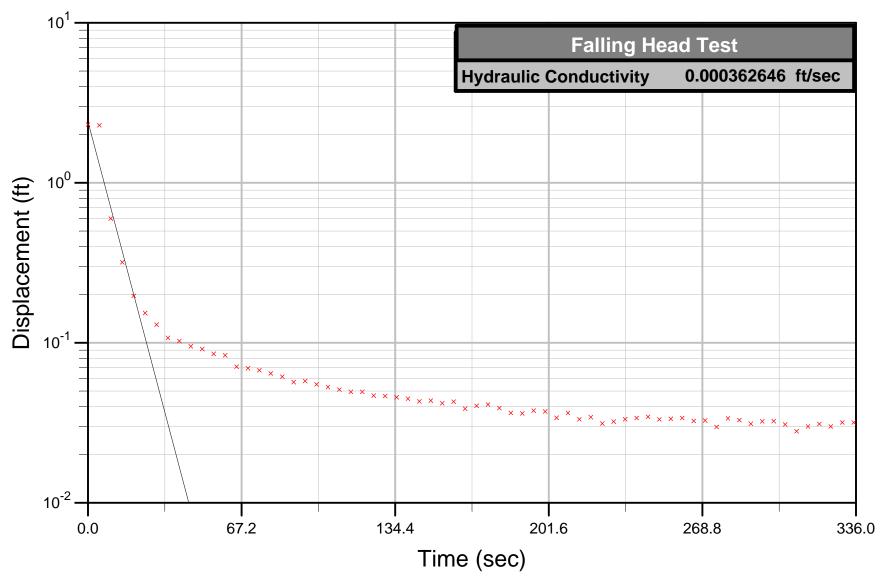
RW07-PZM017



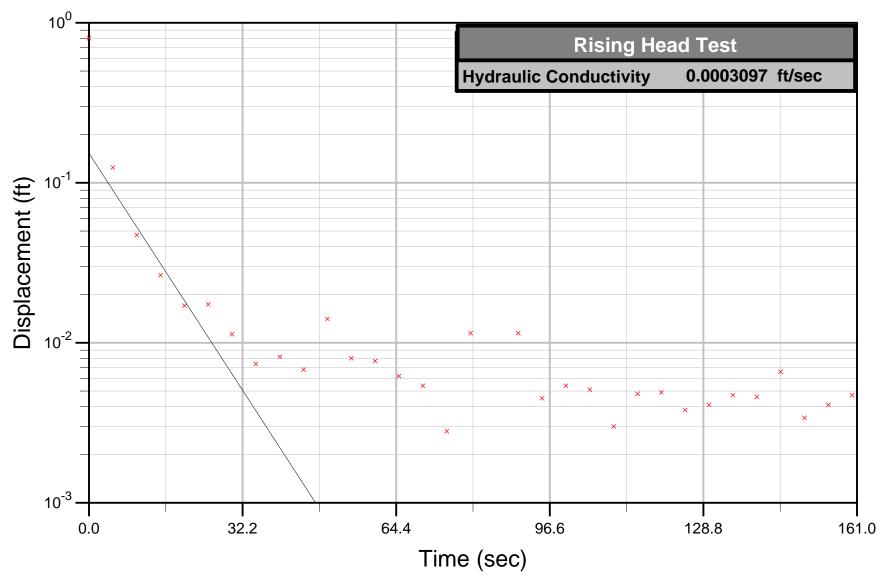
RW07-PZM017



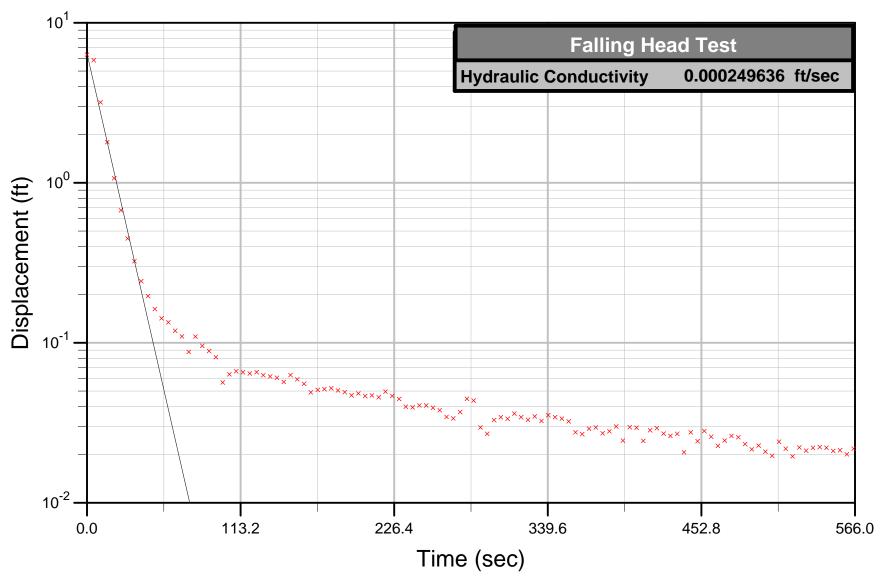
RW13-PZM020



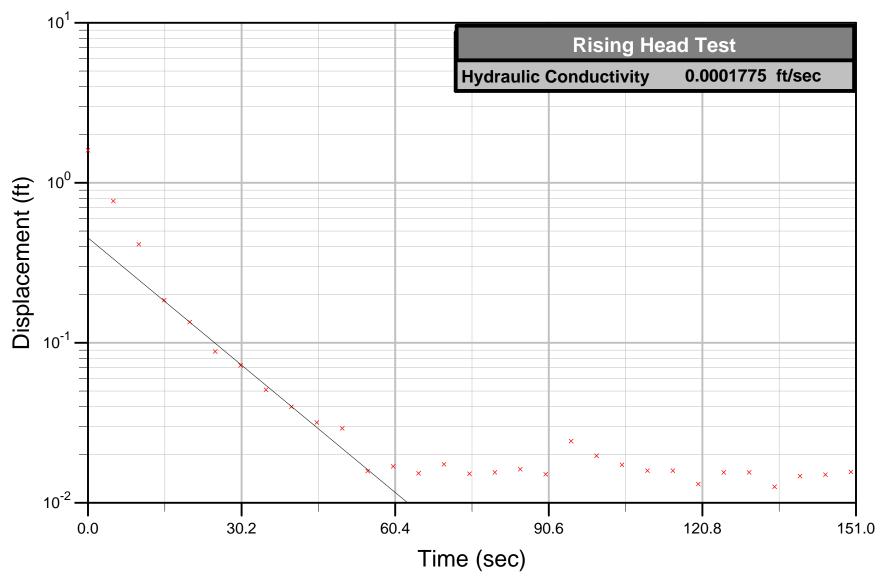
RW13-PZM020



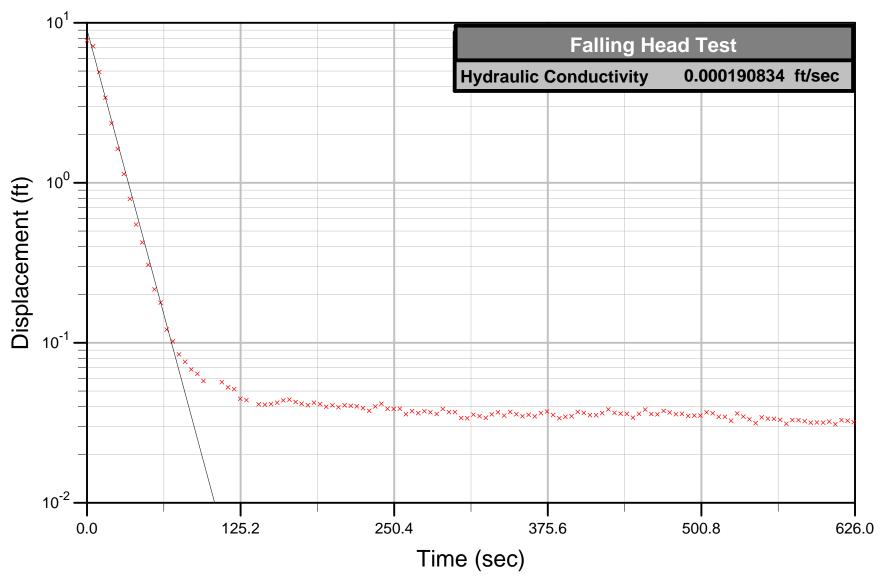
RW14-PZM020



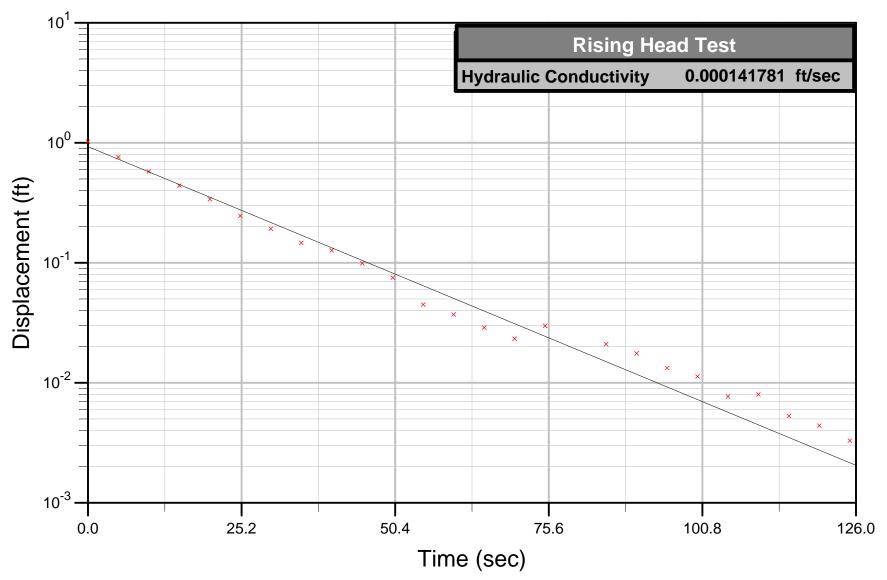
RW14-PZM020



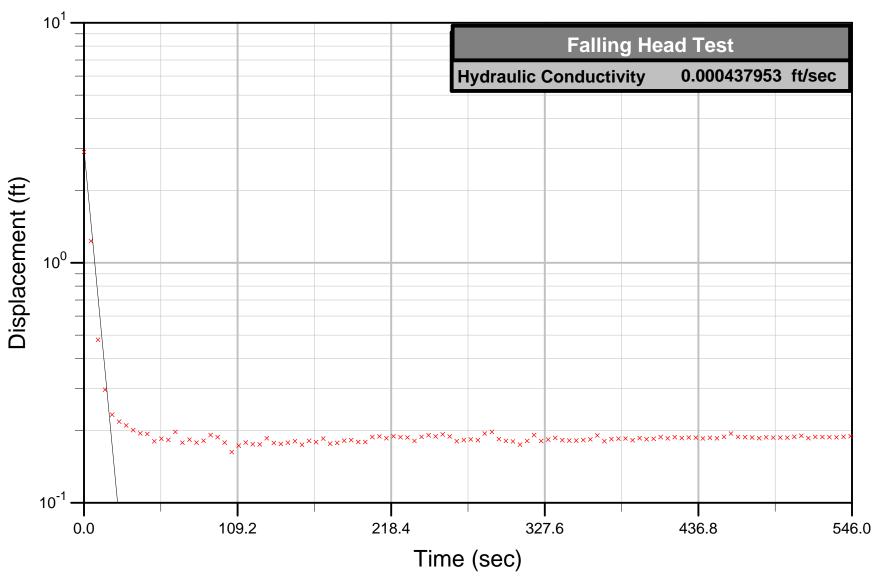
RW16-PZM020



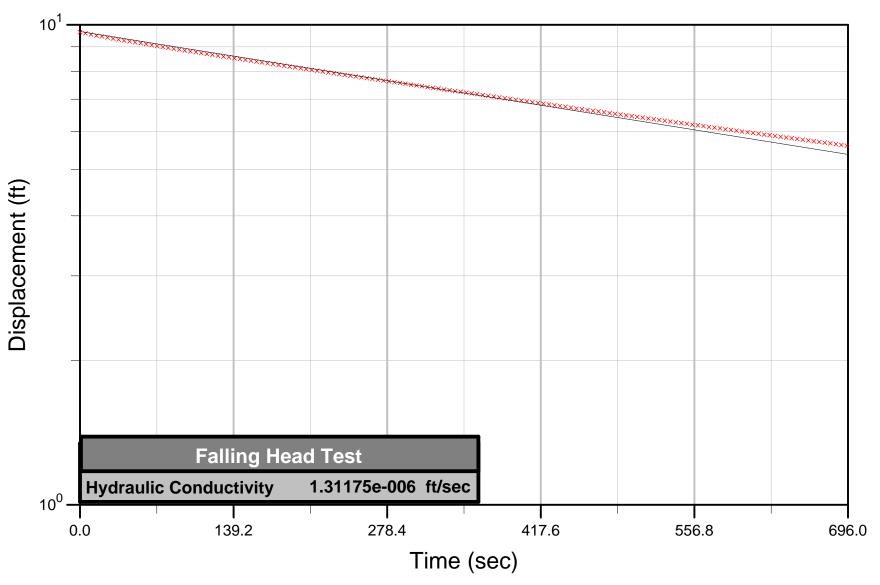
RW16-PZM020



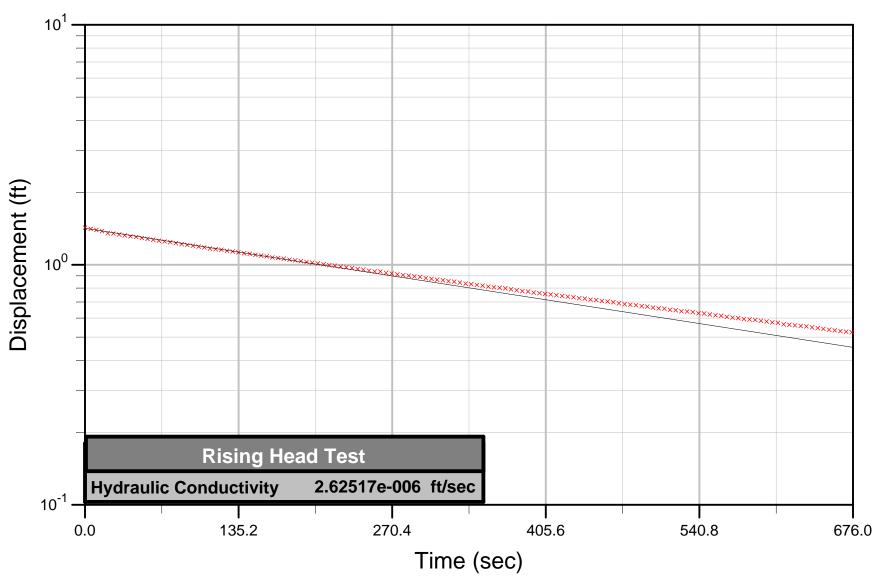
RW17-PZM019



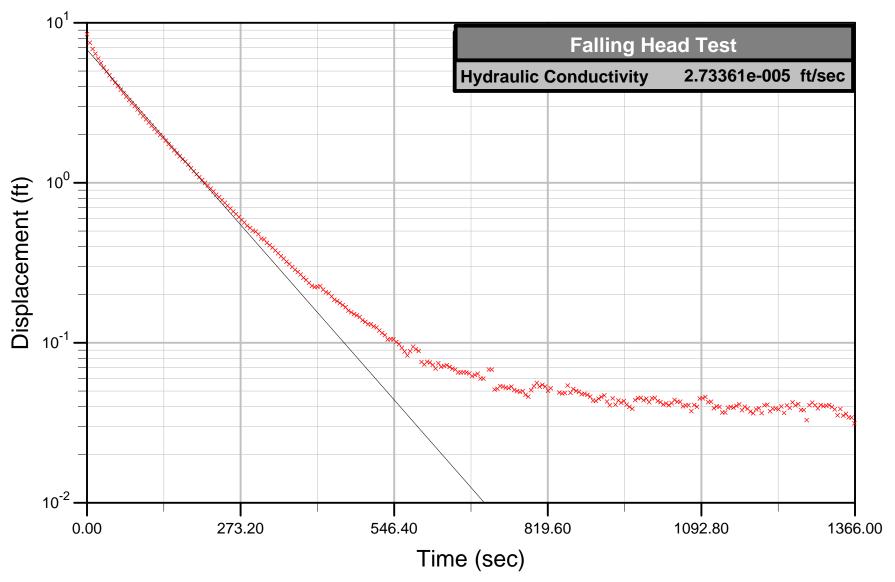
RW20-PZM020



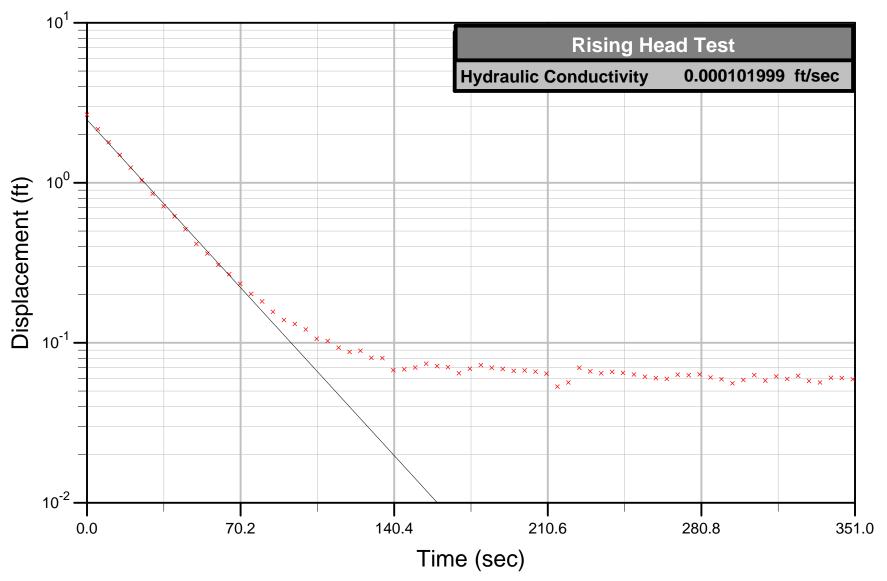
RW20-PZM020



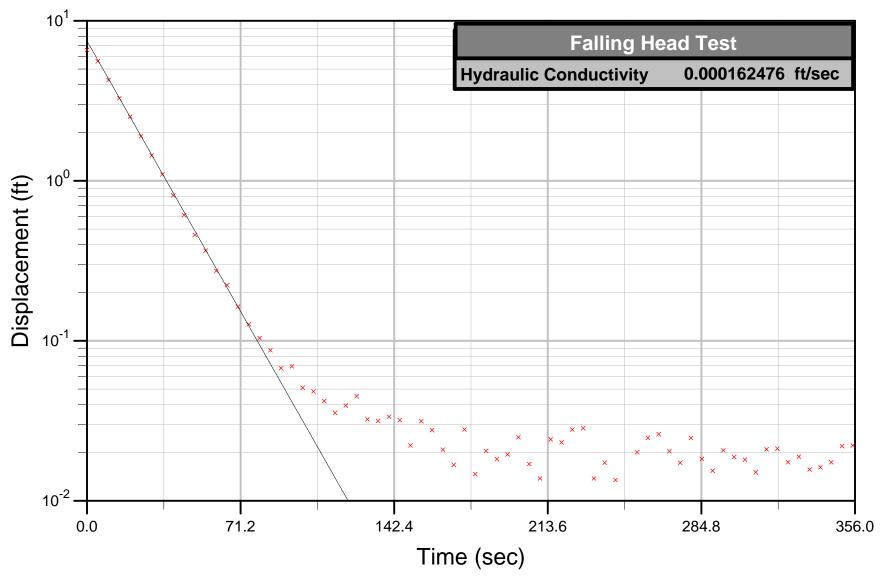
RW21-PZM023



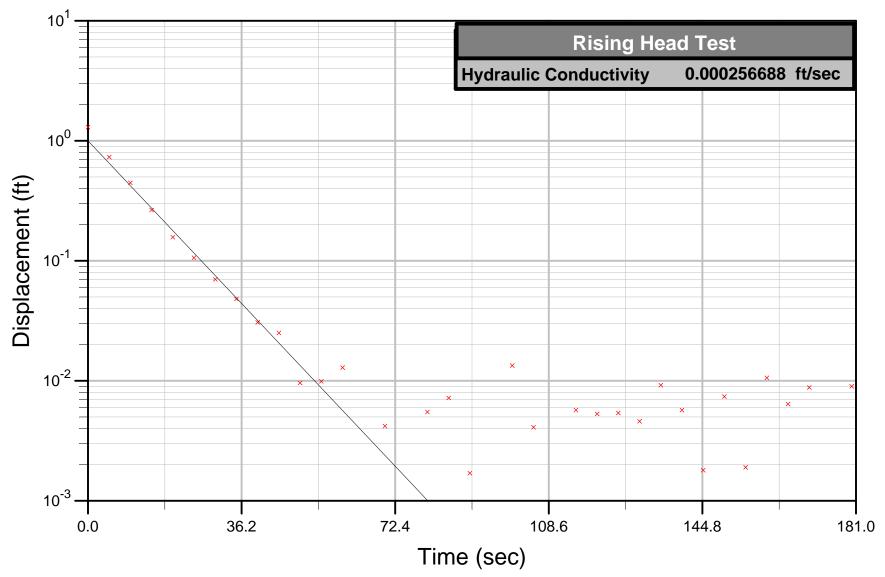
RW21-PZM023



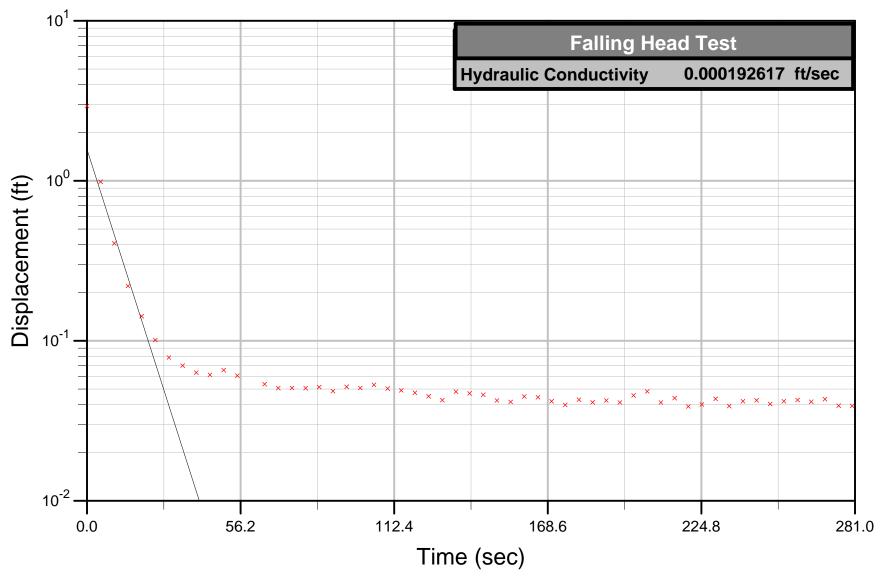
RW-22(I)



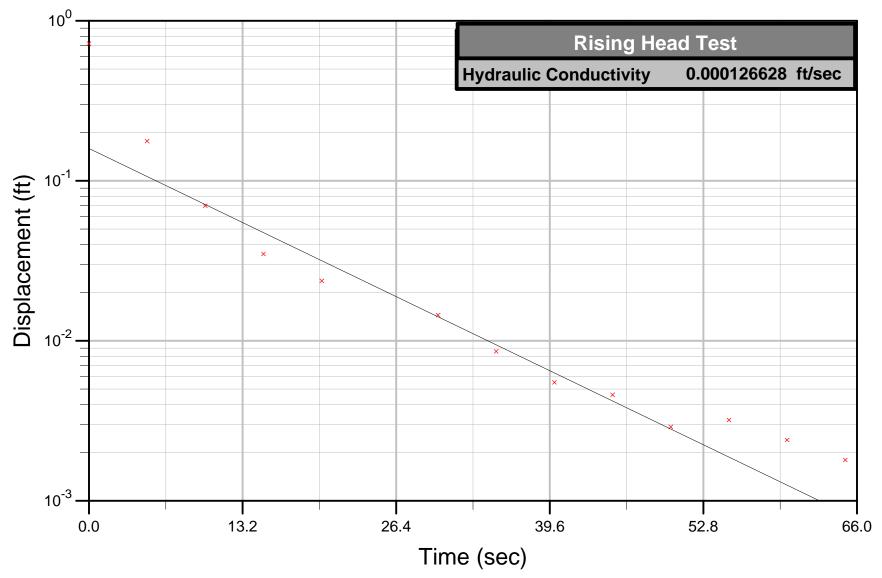
RW-22(I)



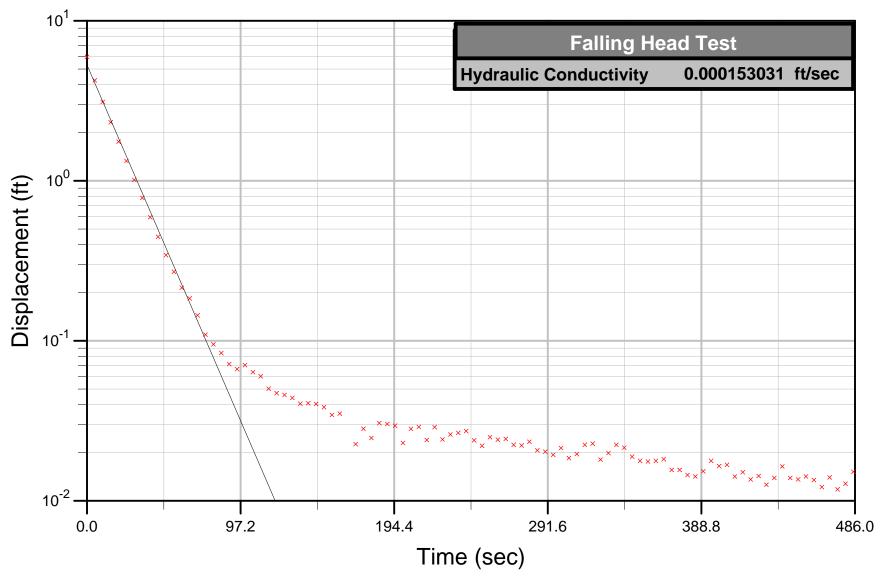
RW-23(I)



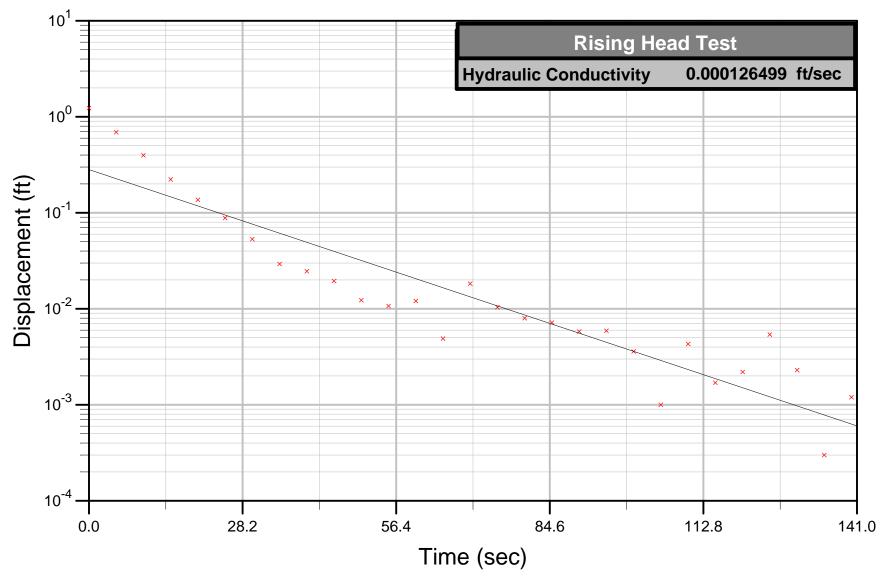
RW-23(I)



RW-24(I)

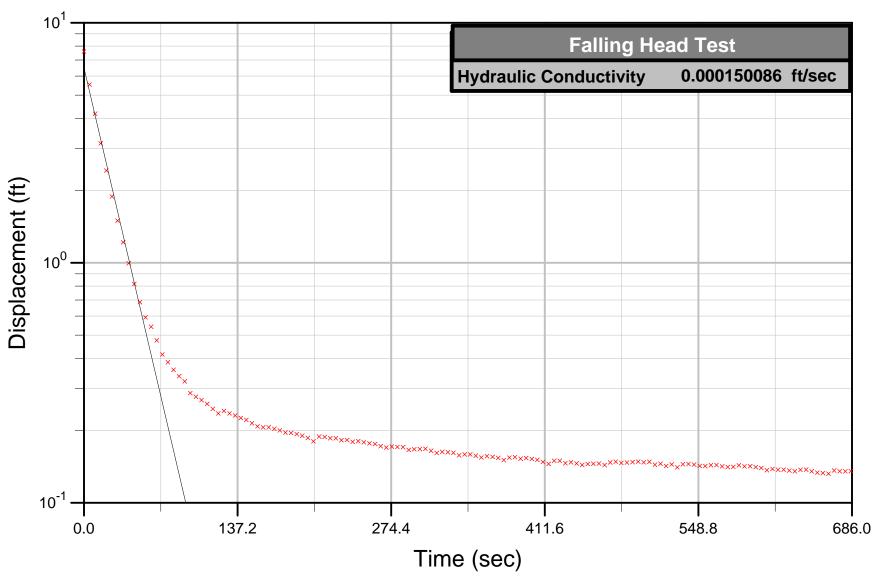


RW-24(I)

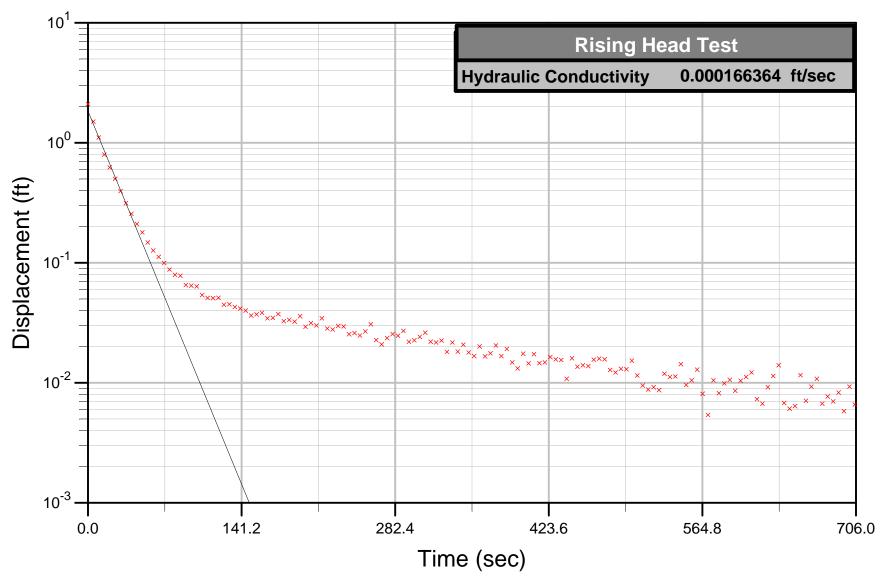


DEEP MONITORING WELLS

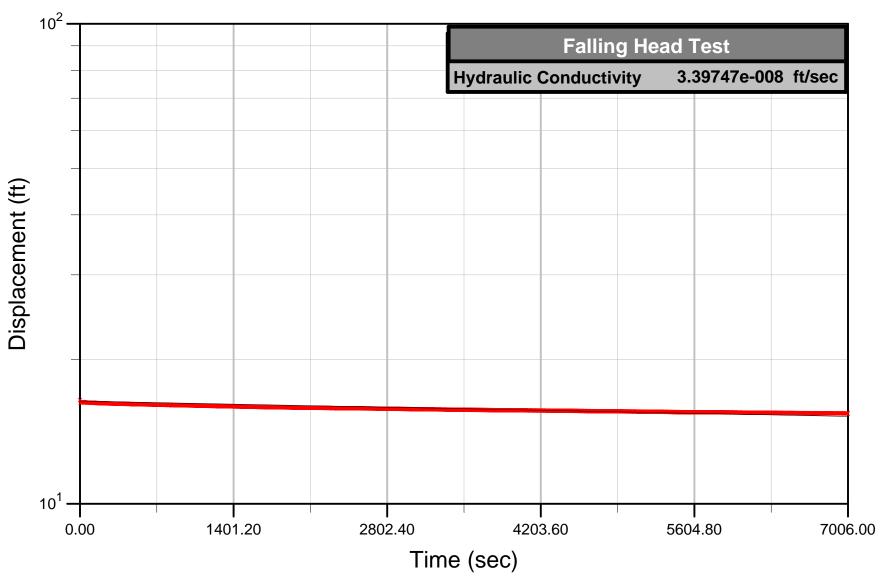
RW10-PZM065



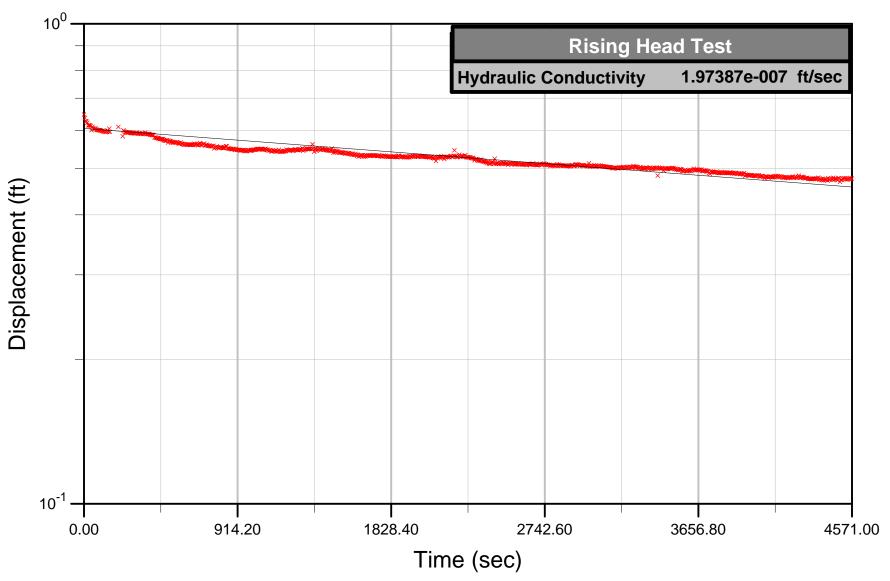
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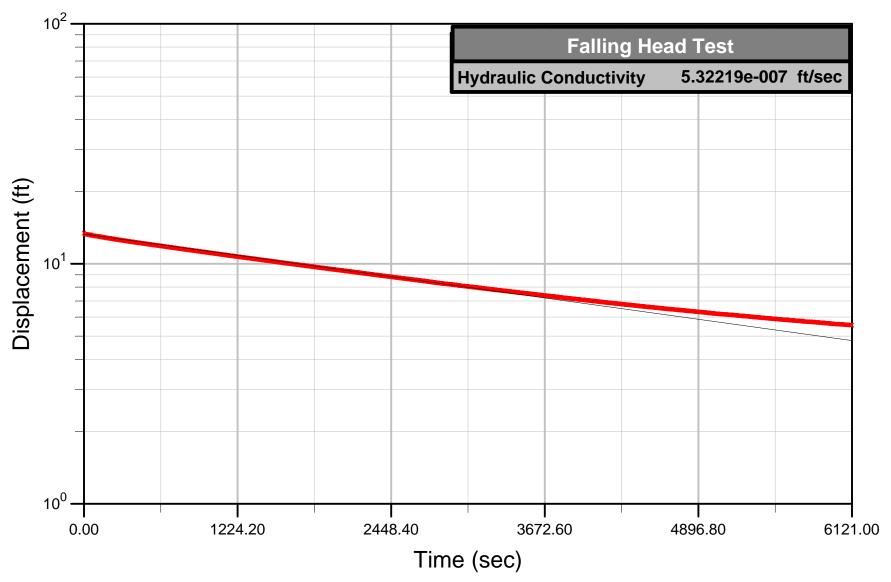
RW18-PZM047



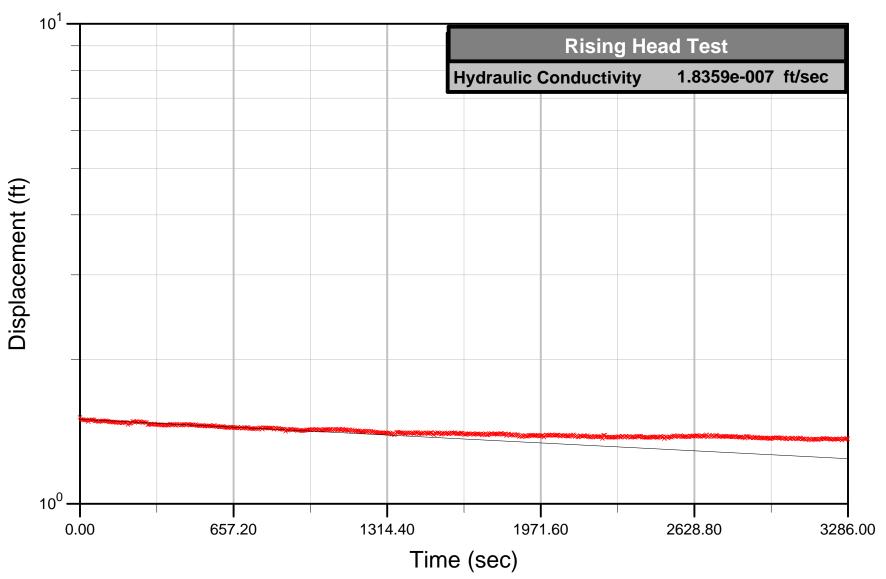
RW18-PZM047



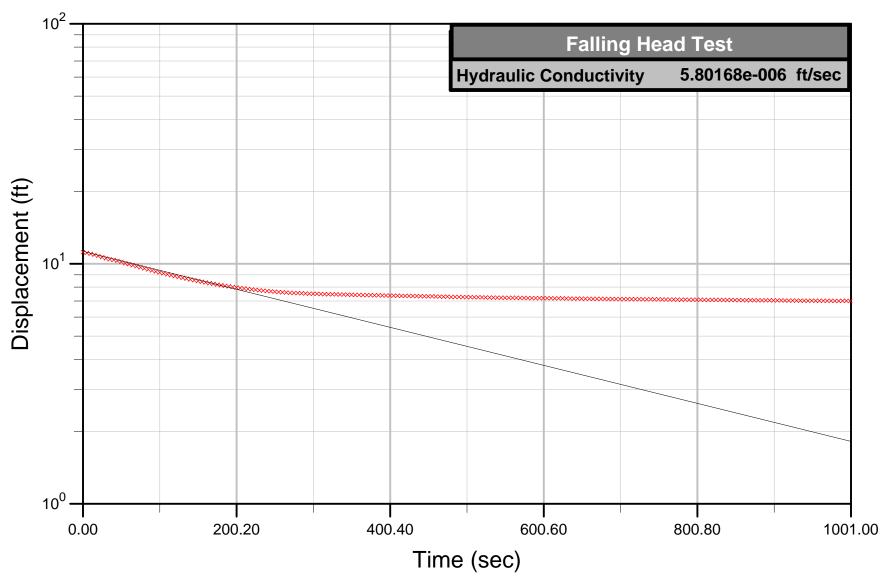
RW19-PZM050



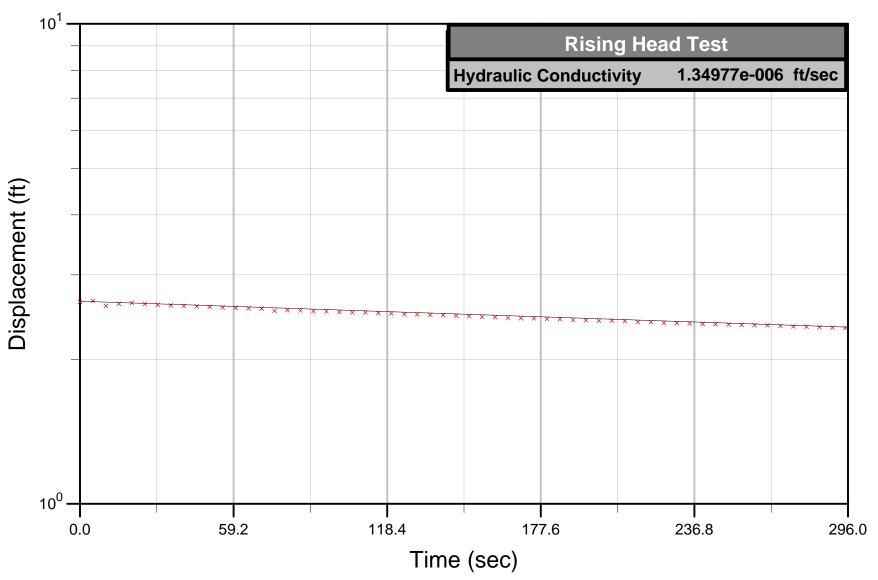
RW19-PZM050



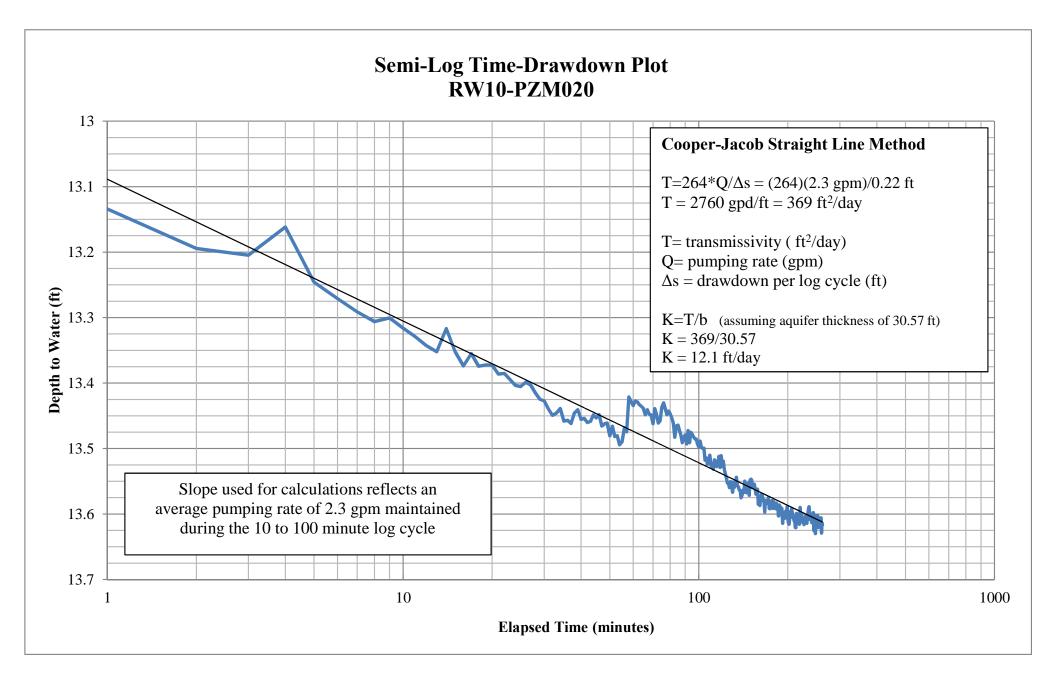
RW20-PZM050



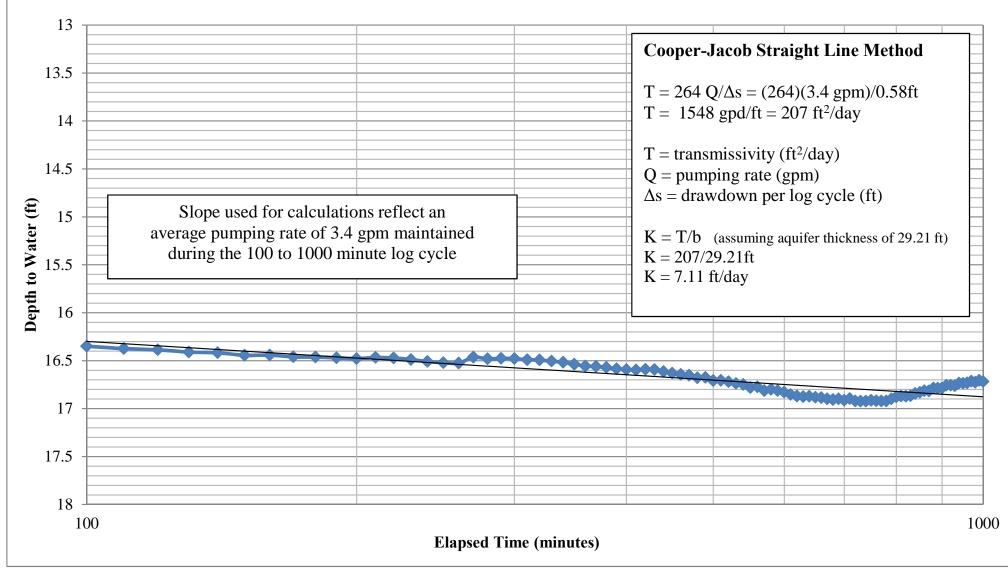
RW20-PZM050

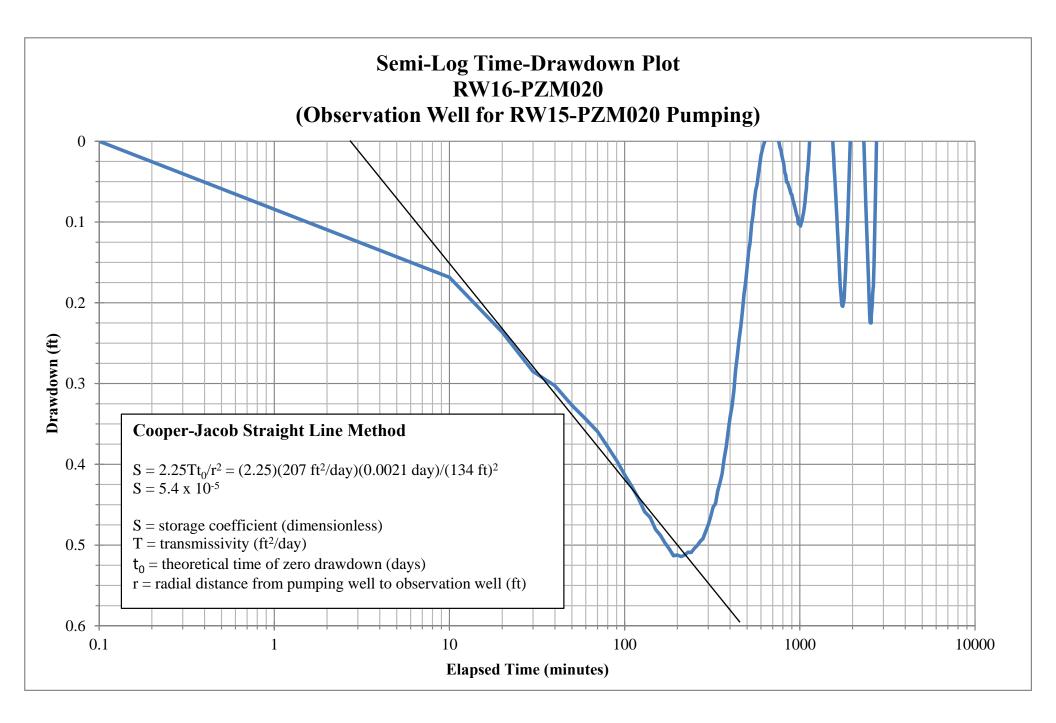


PUMPING WELLS

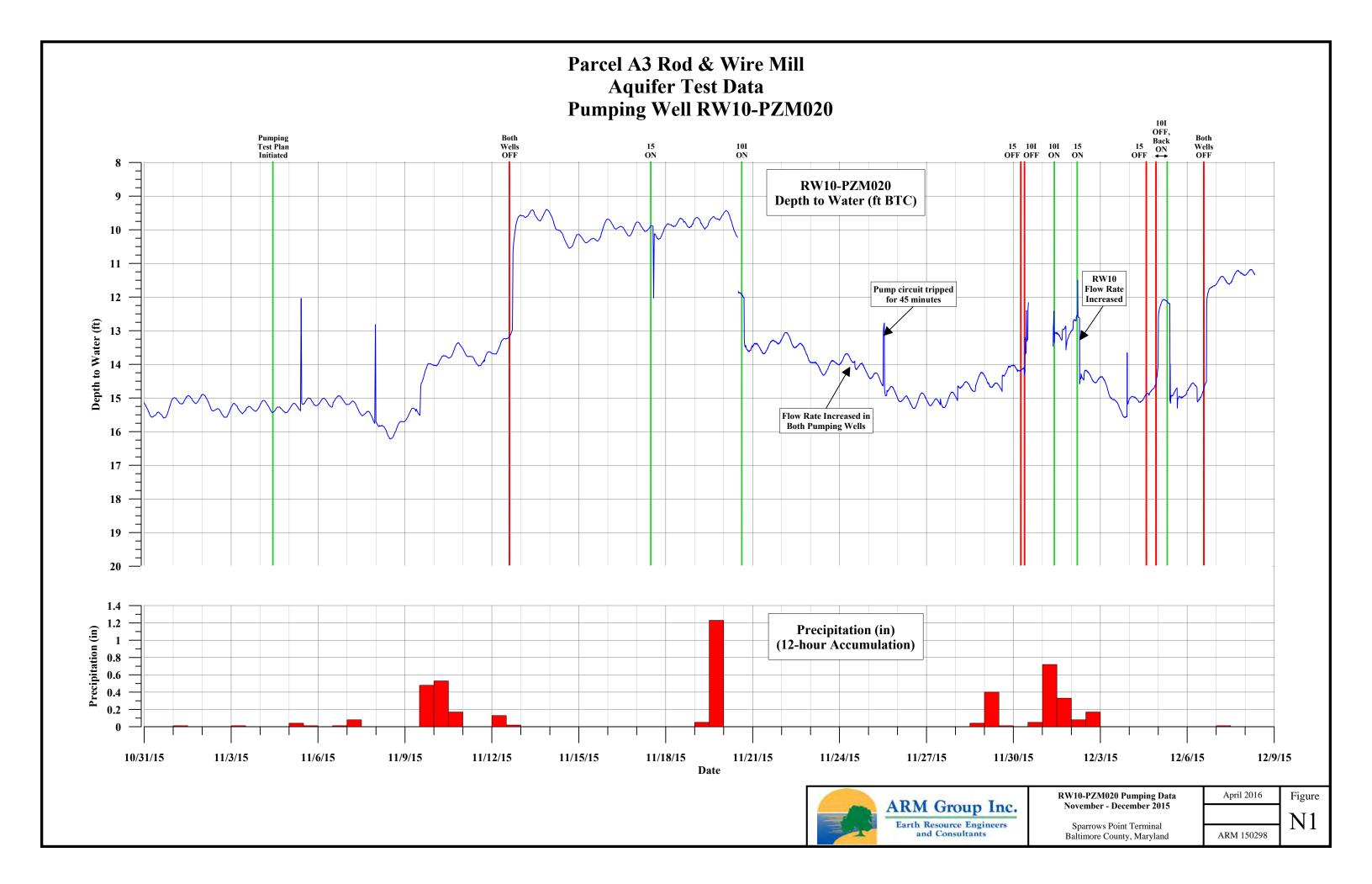


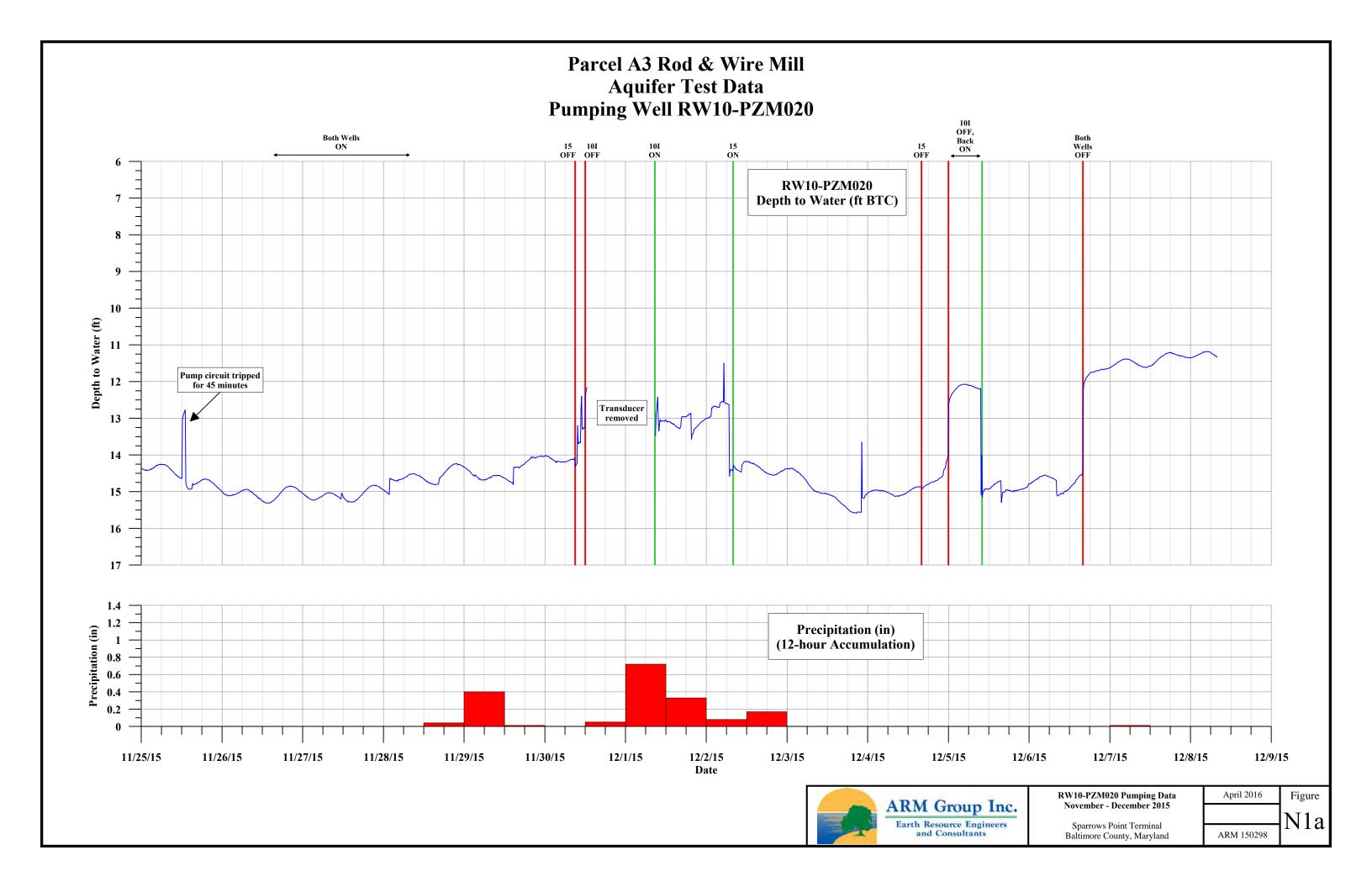
Semi-Log Time-Drawdown Plot RW15-PZM020

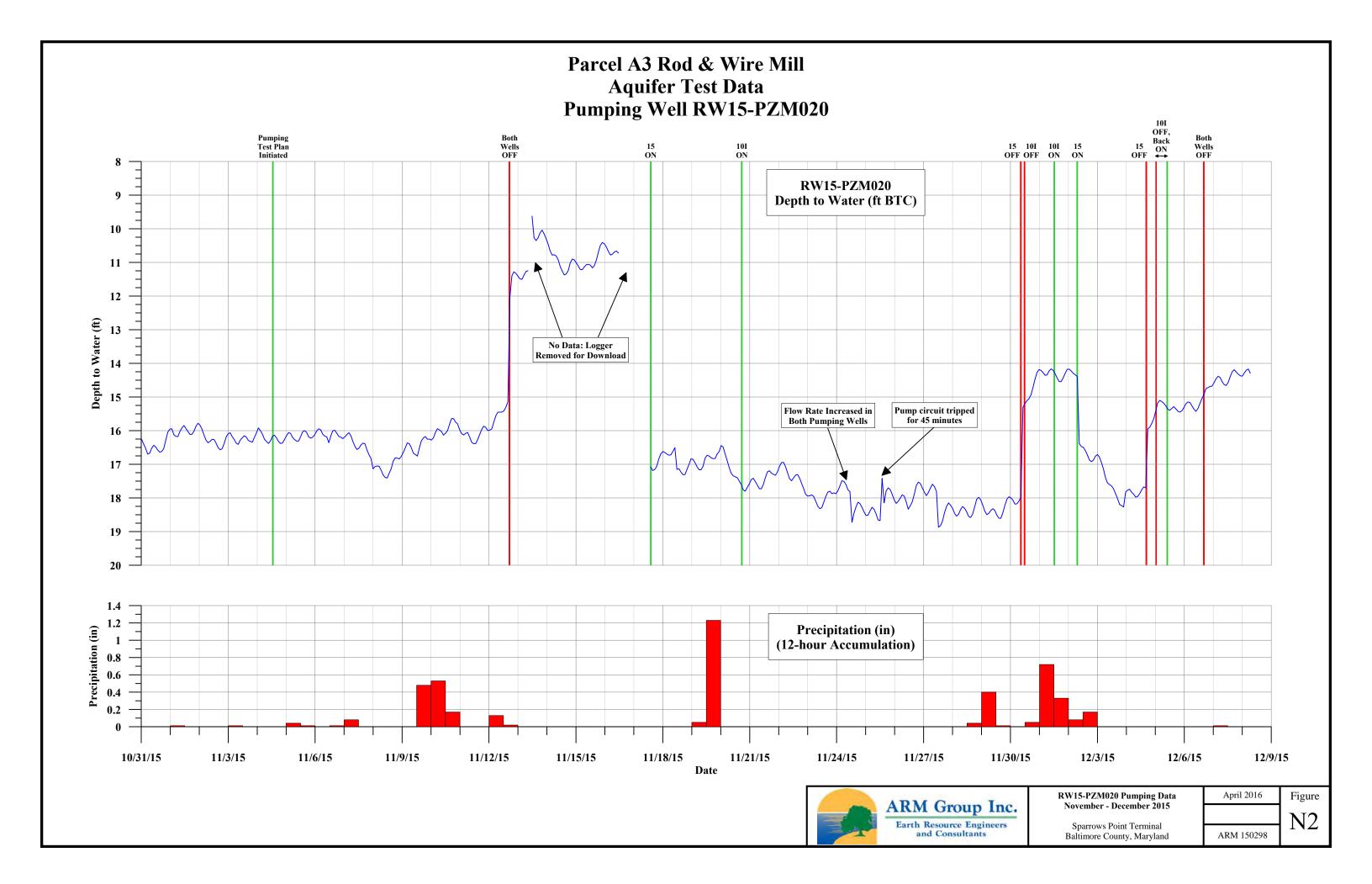


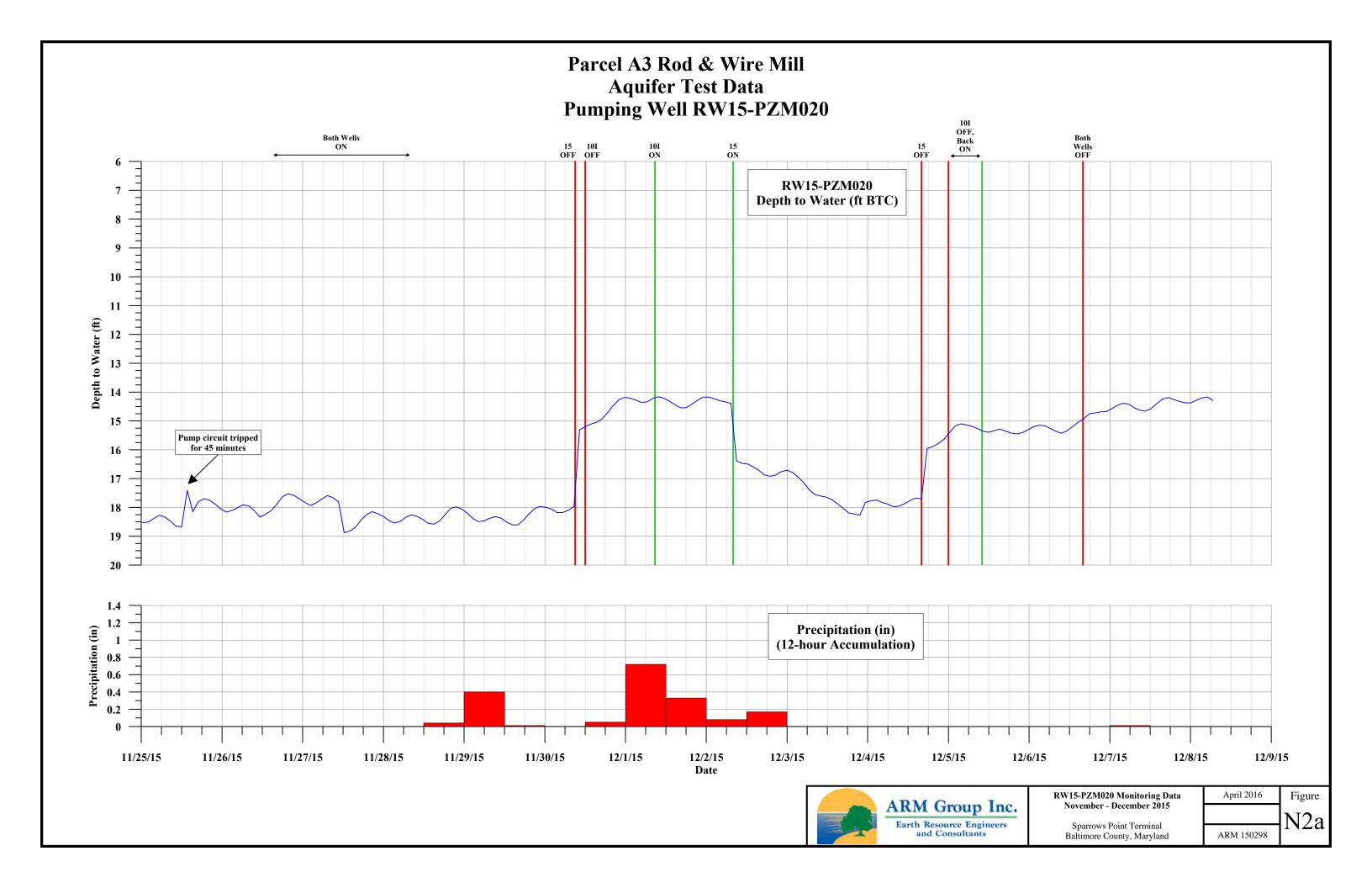


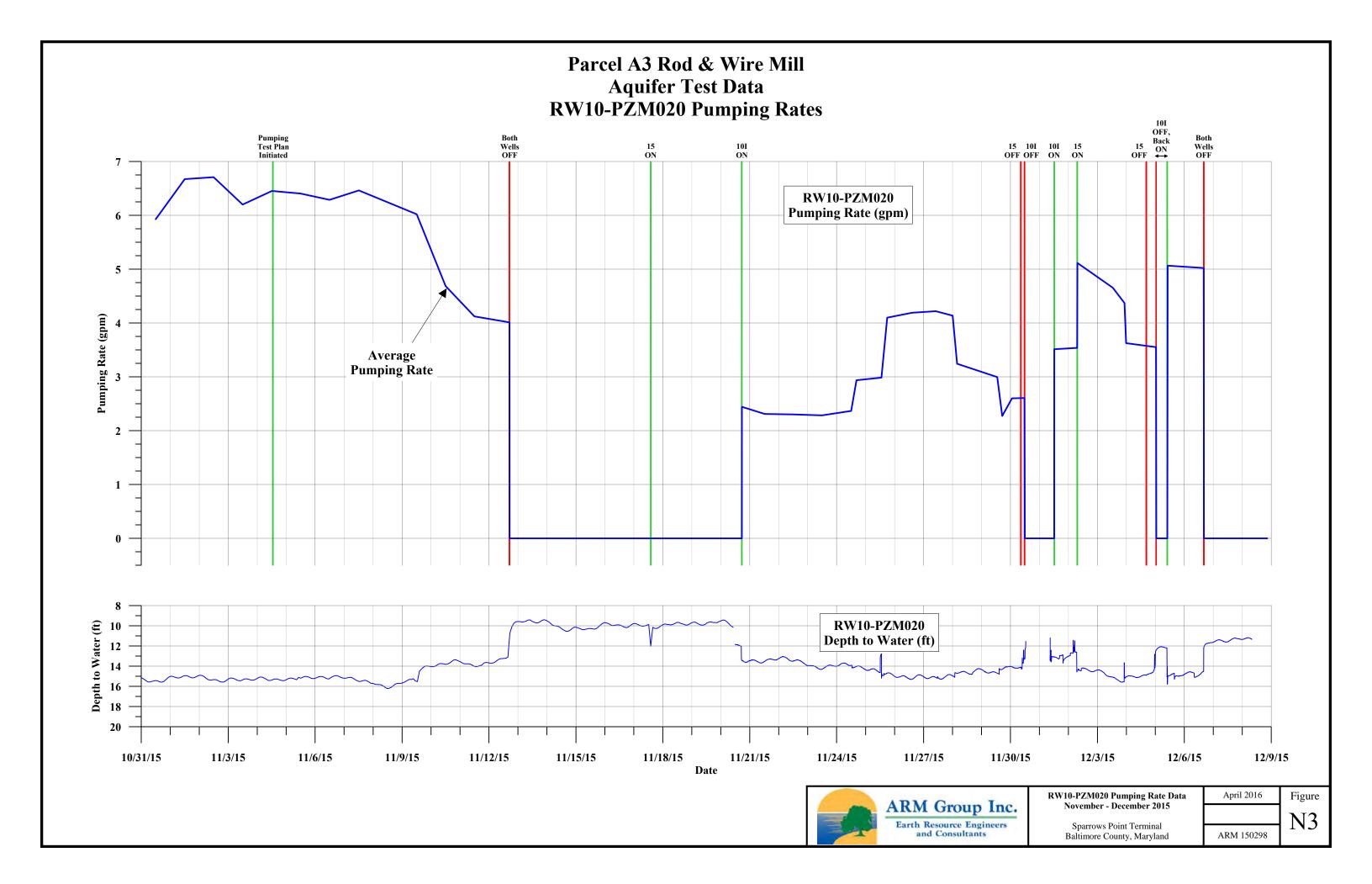
APPENDIX N

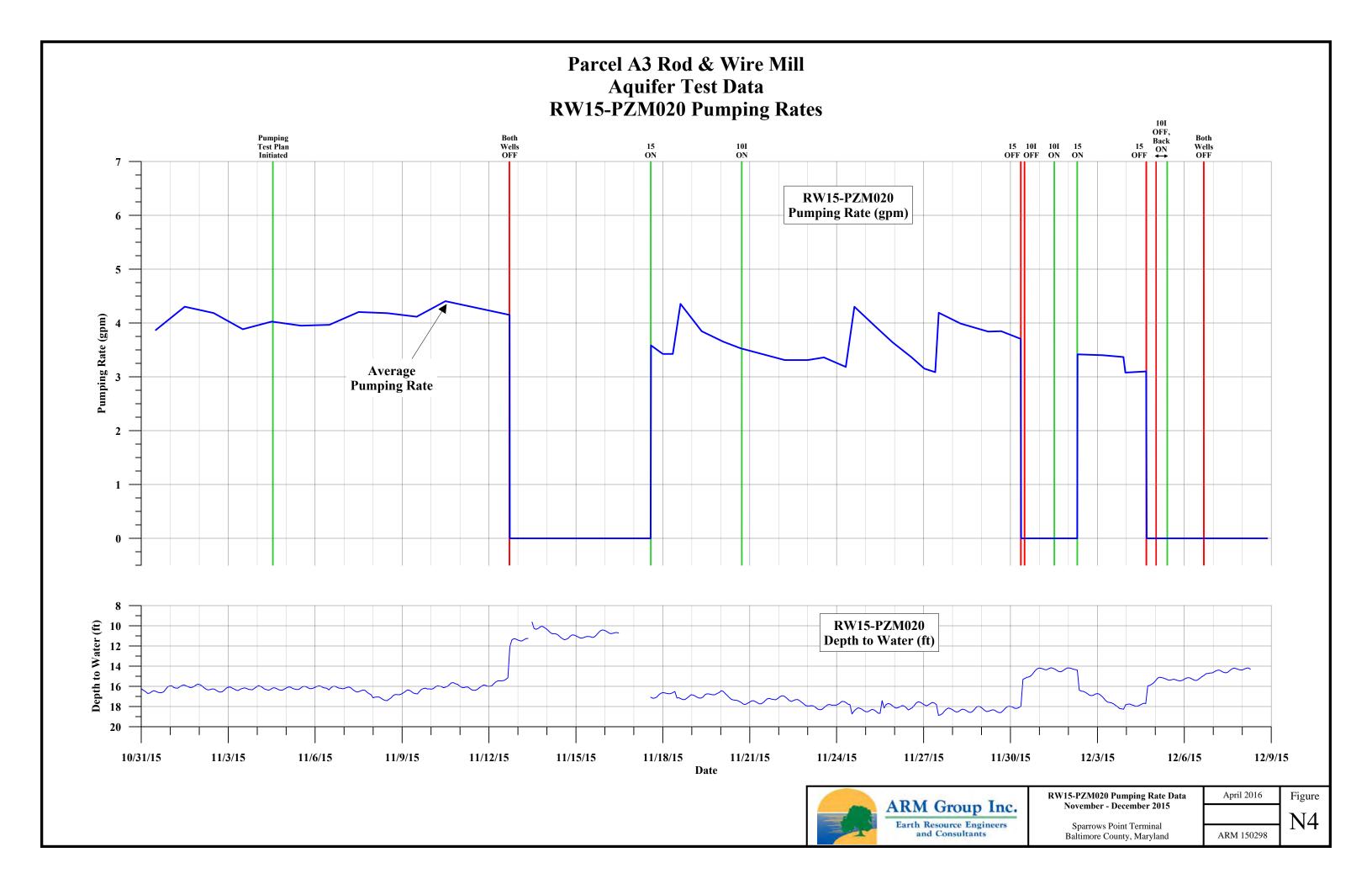


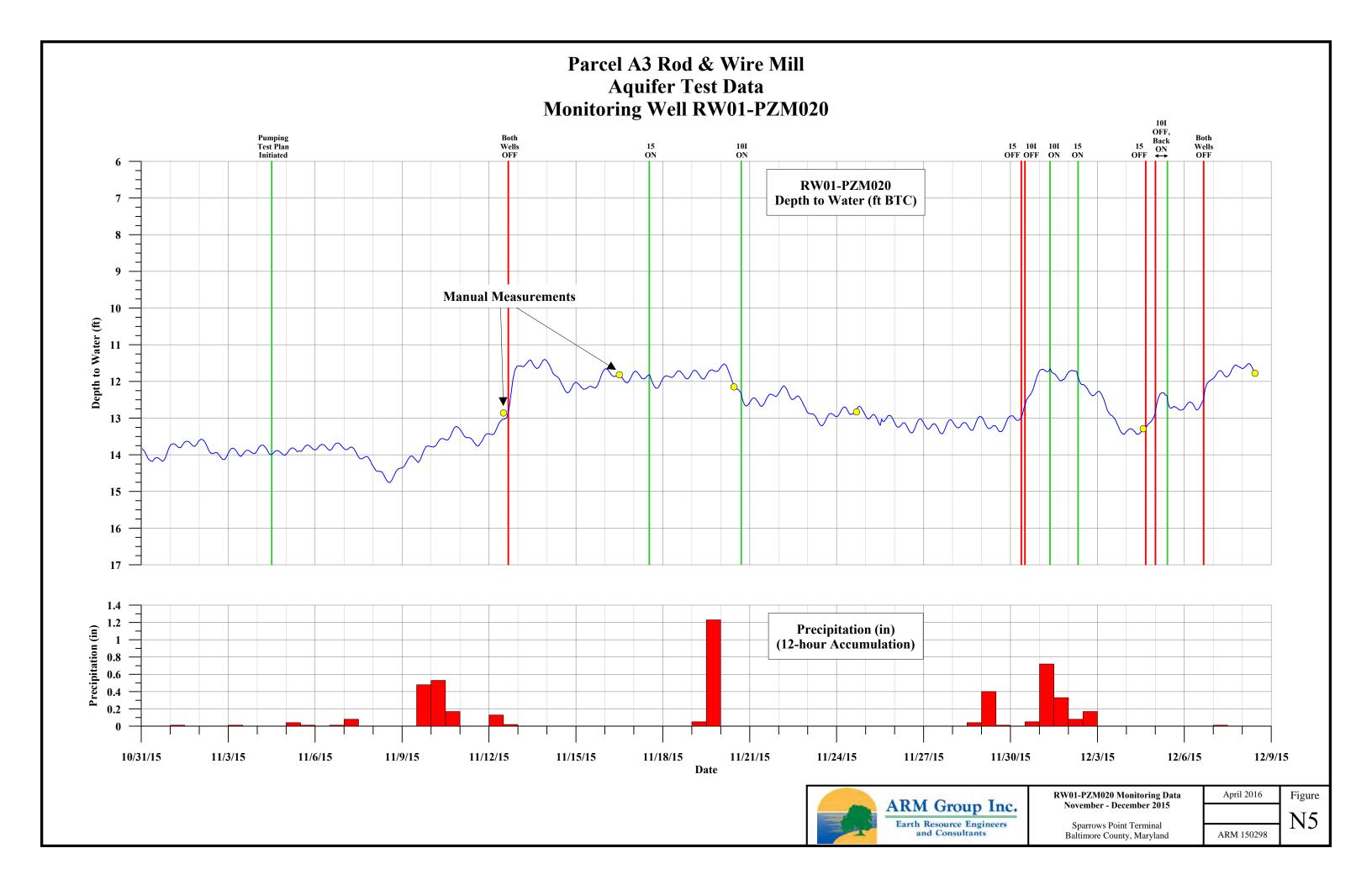


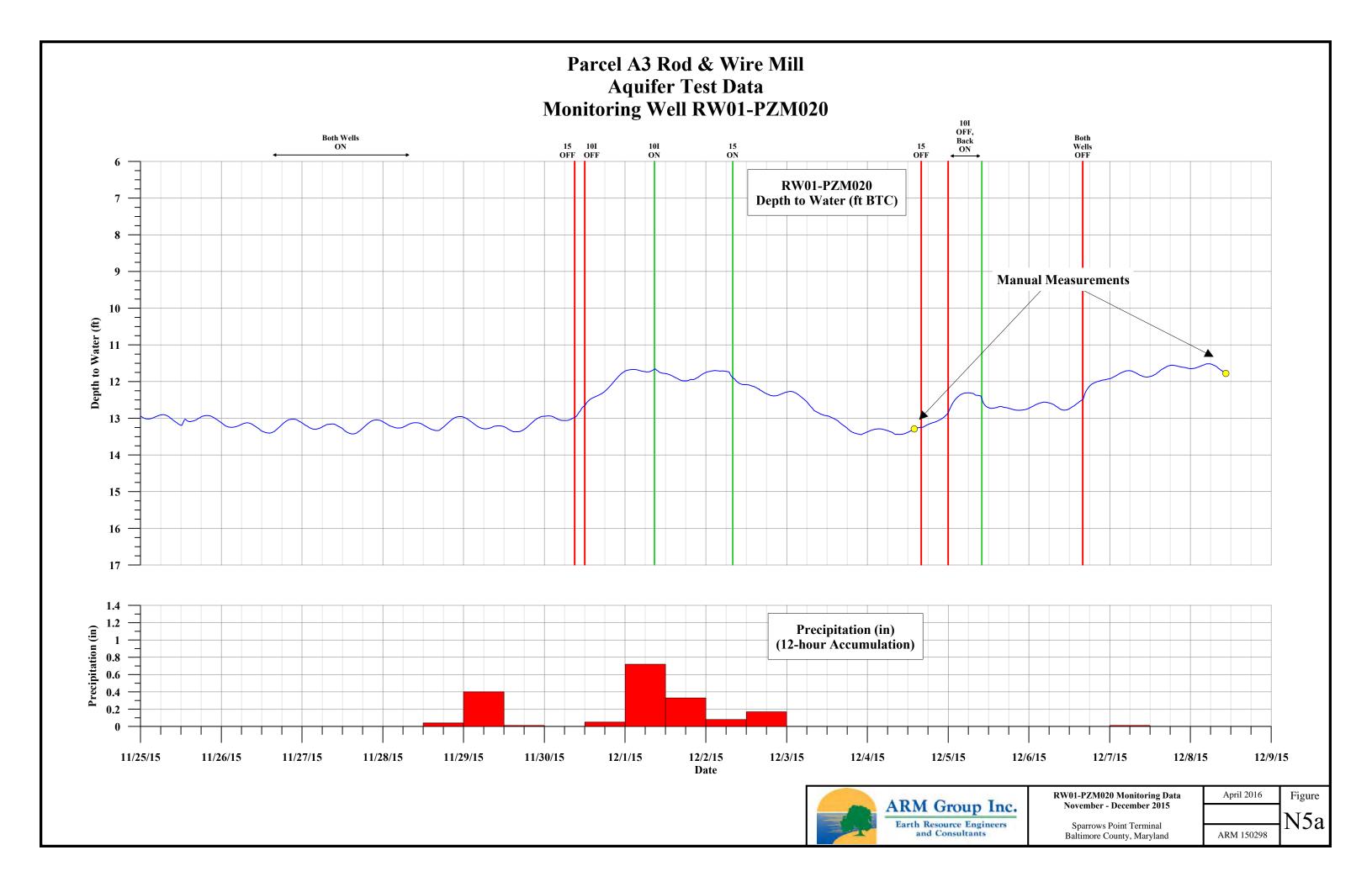


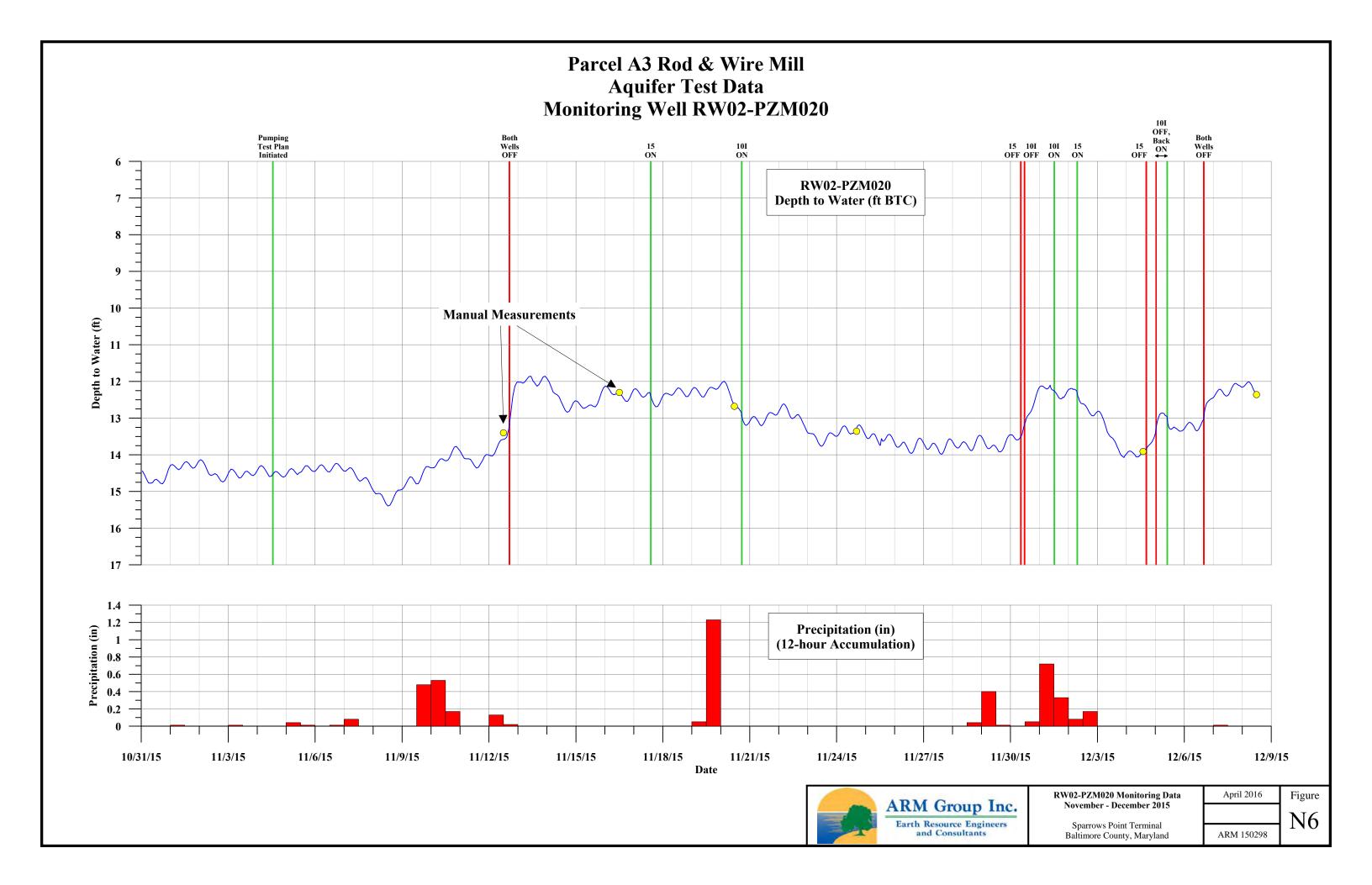


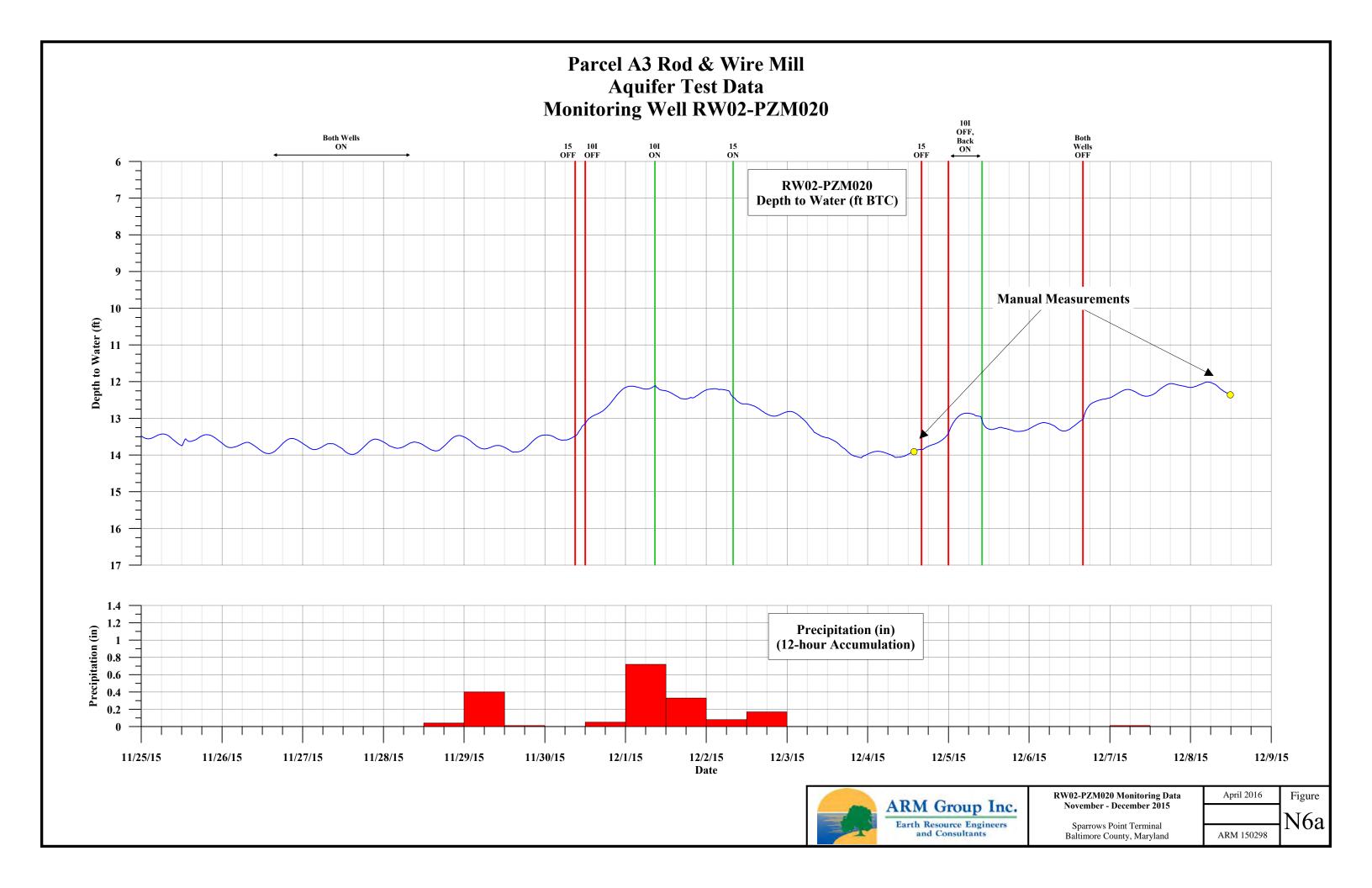


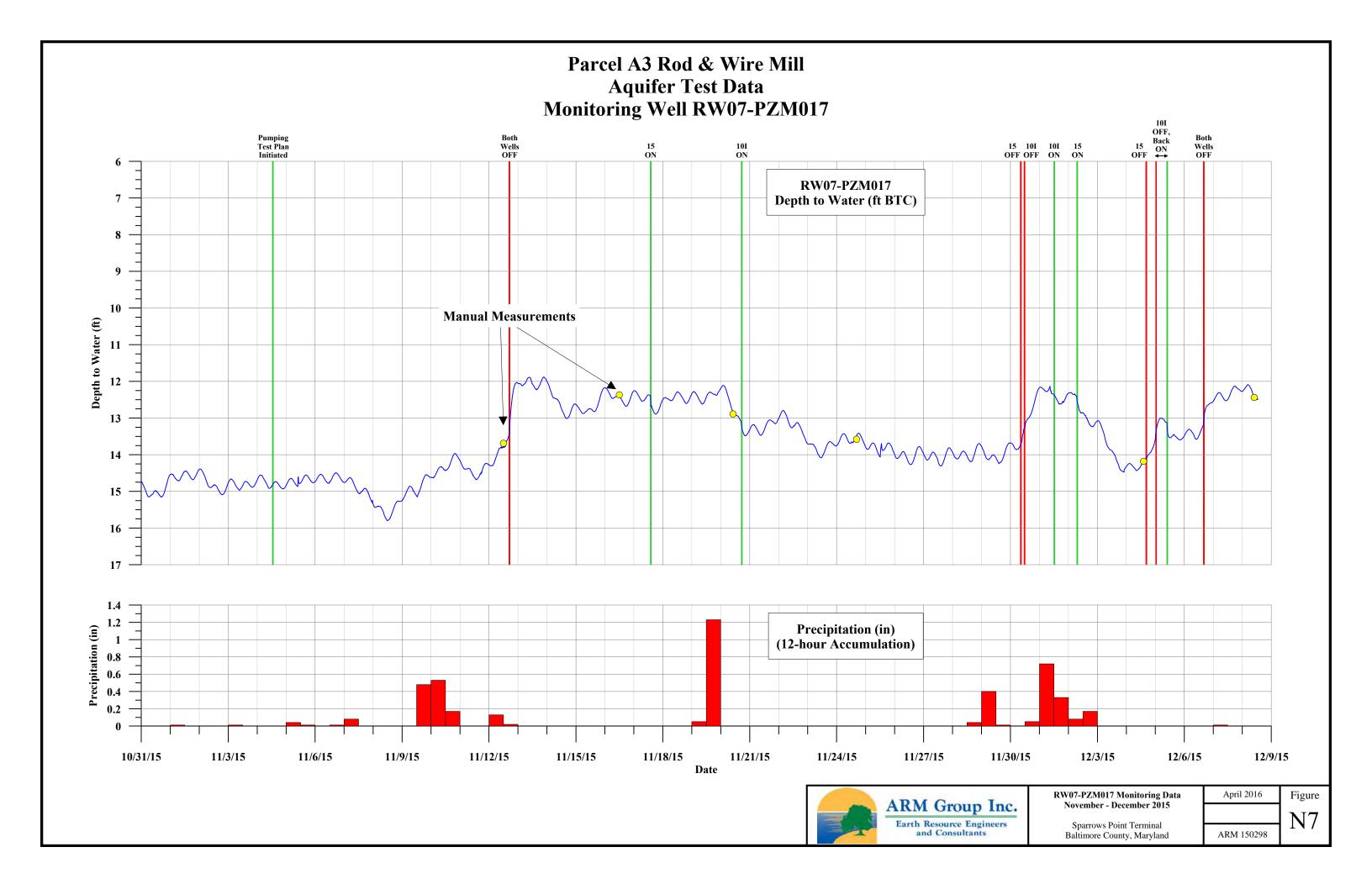


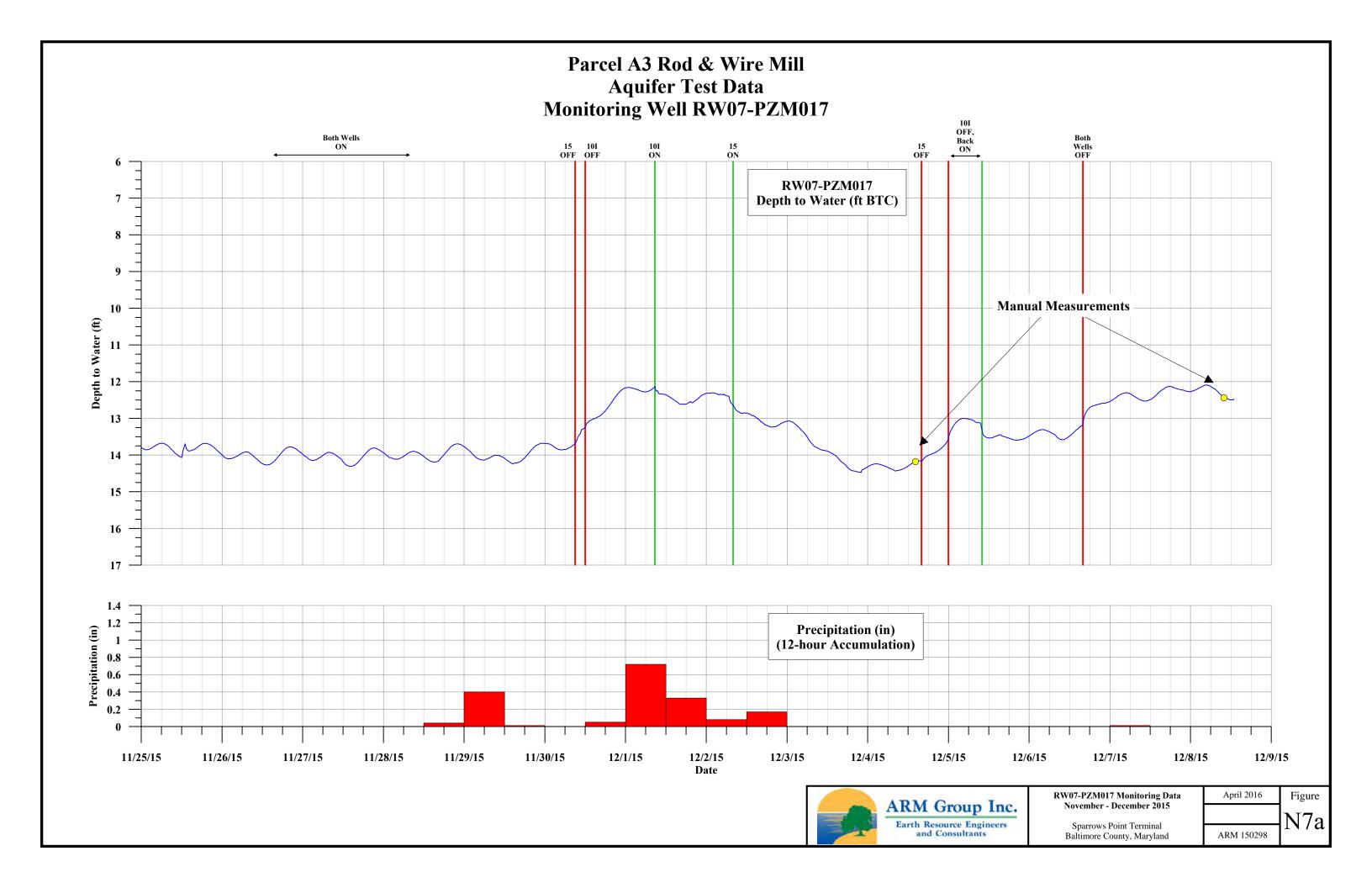


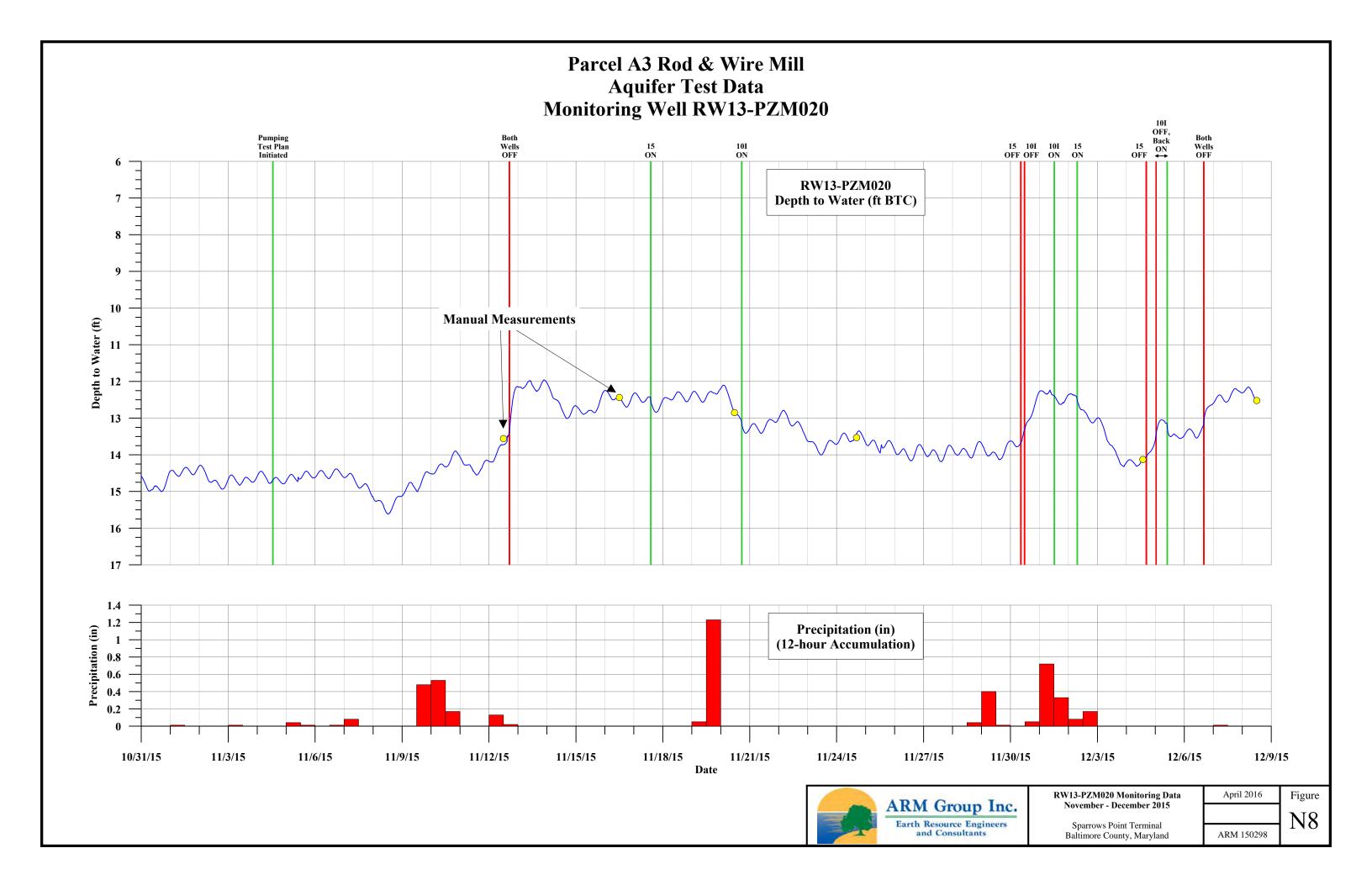


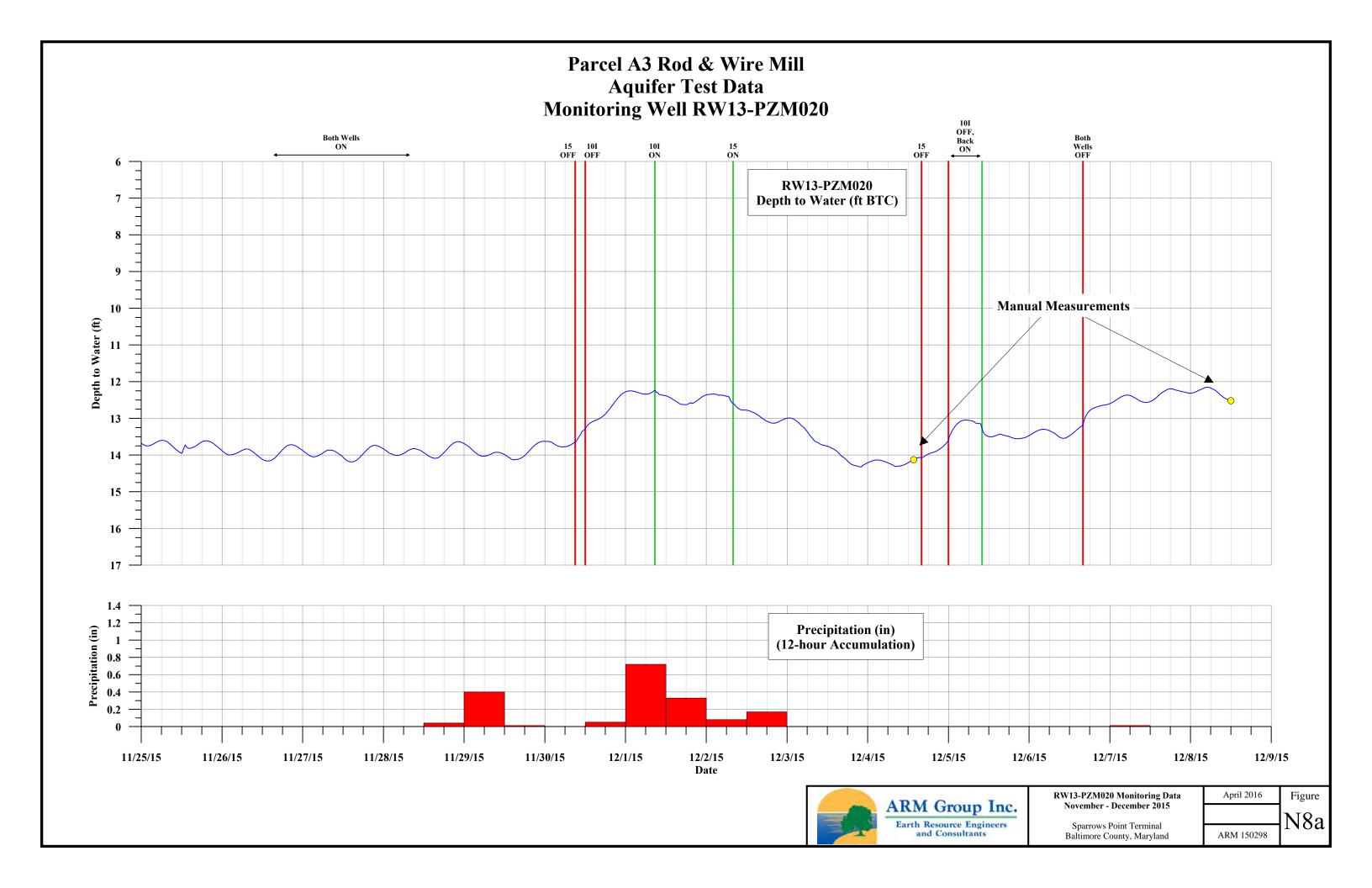


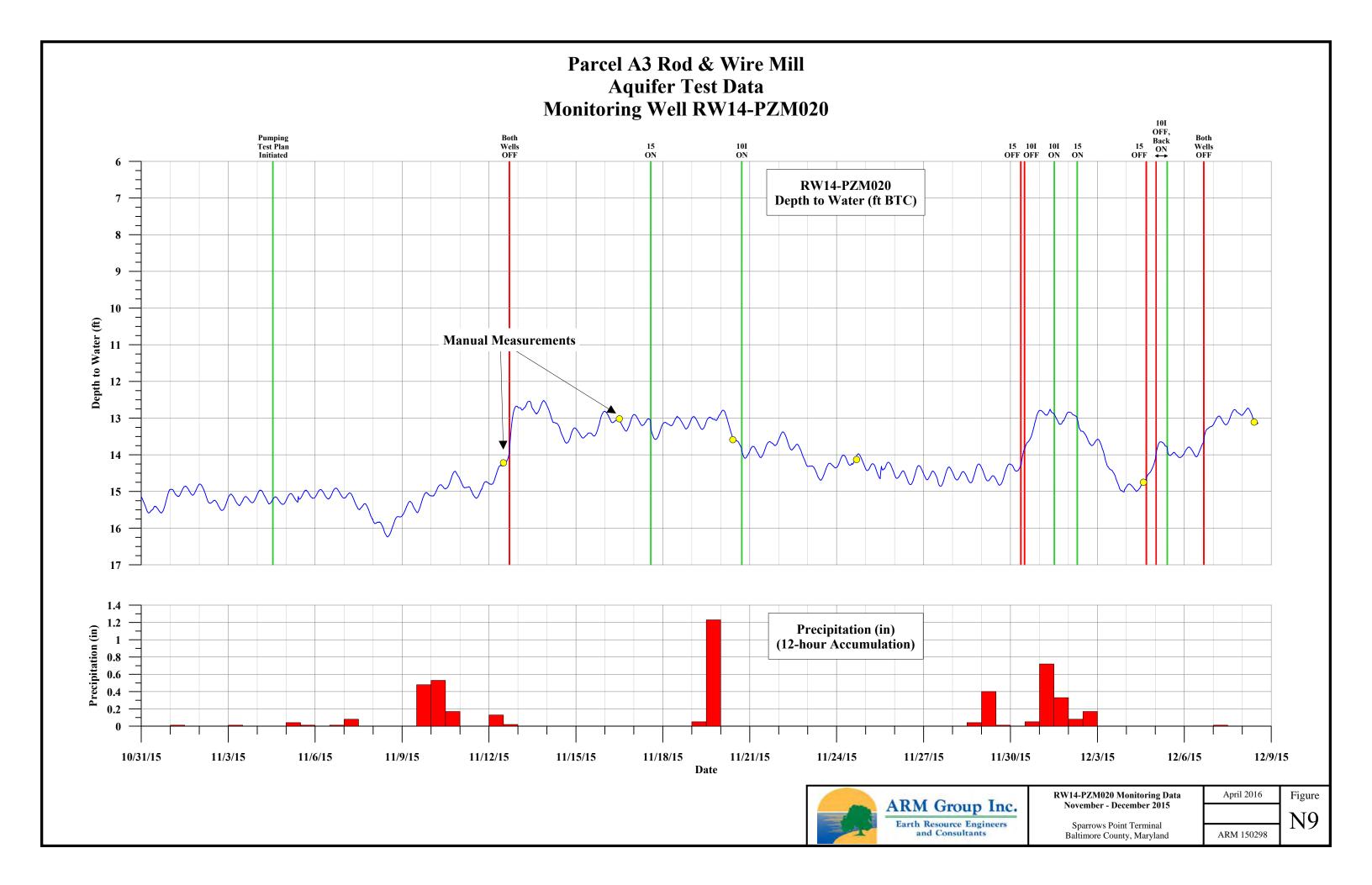


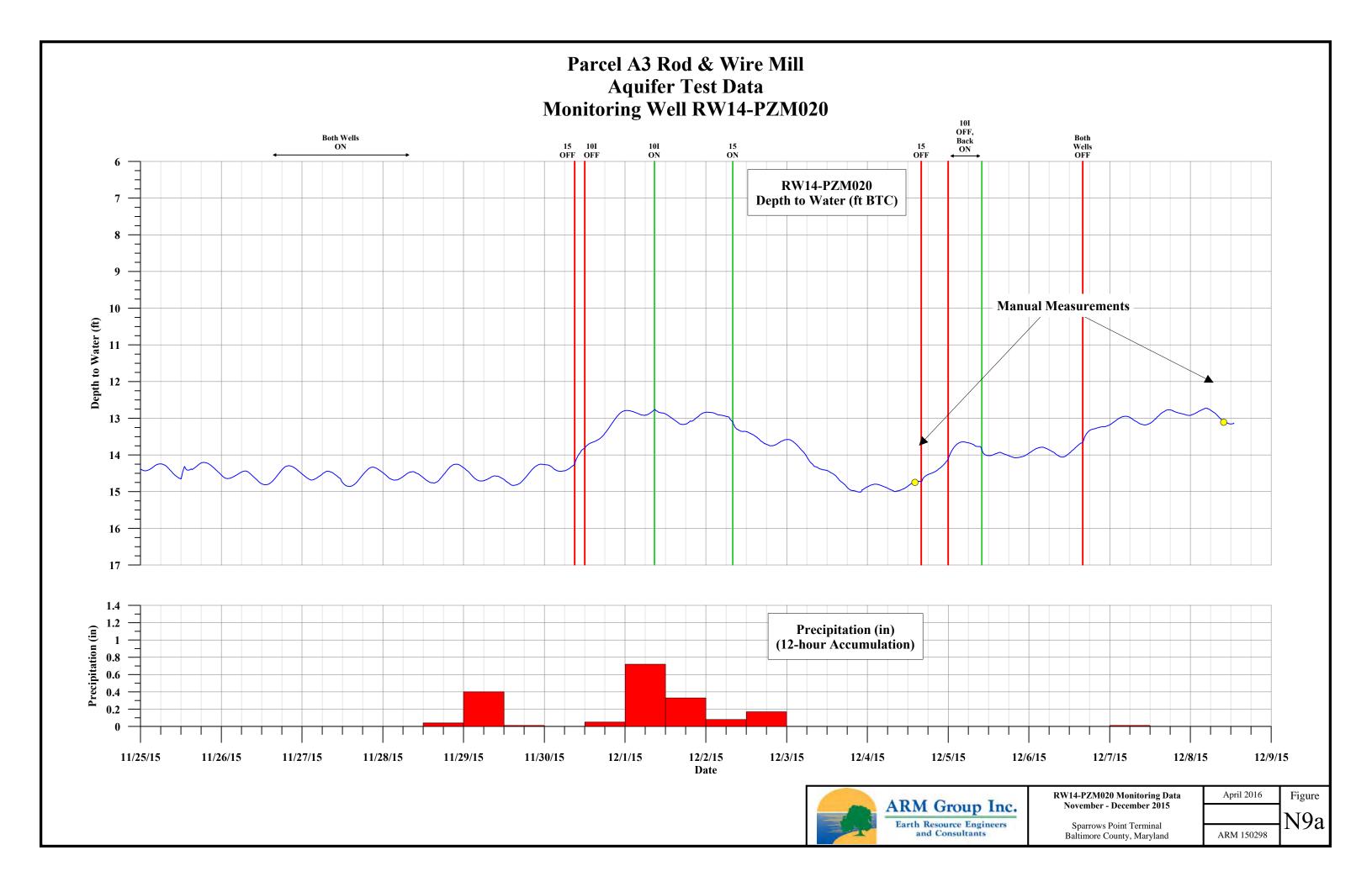


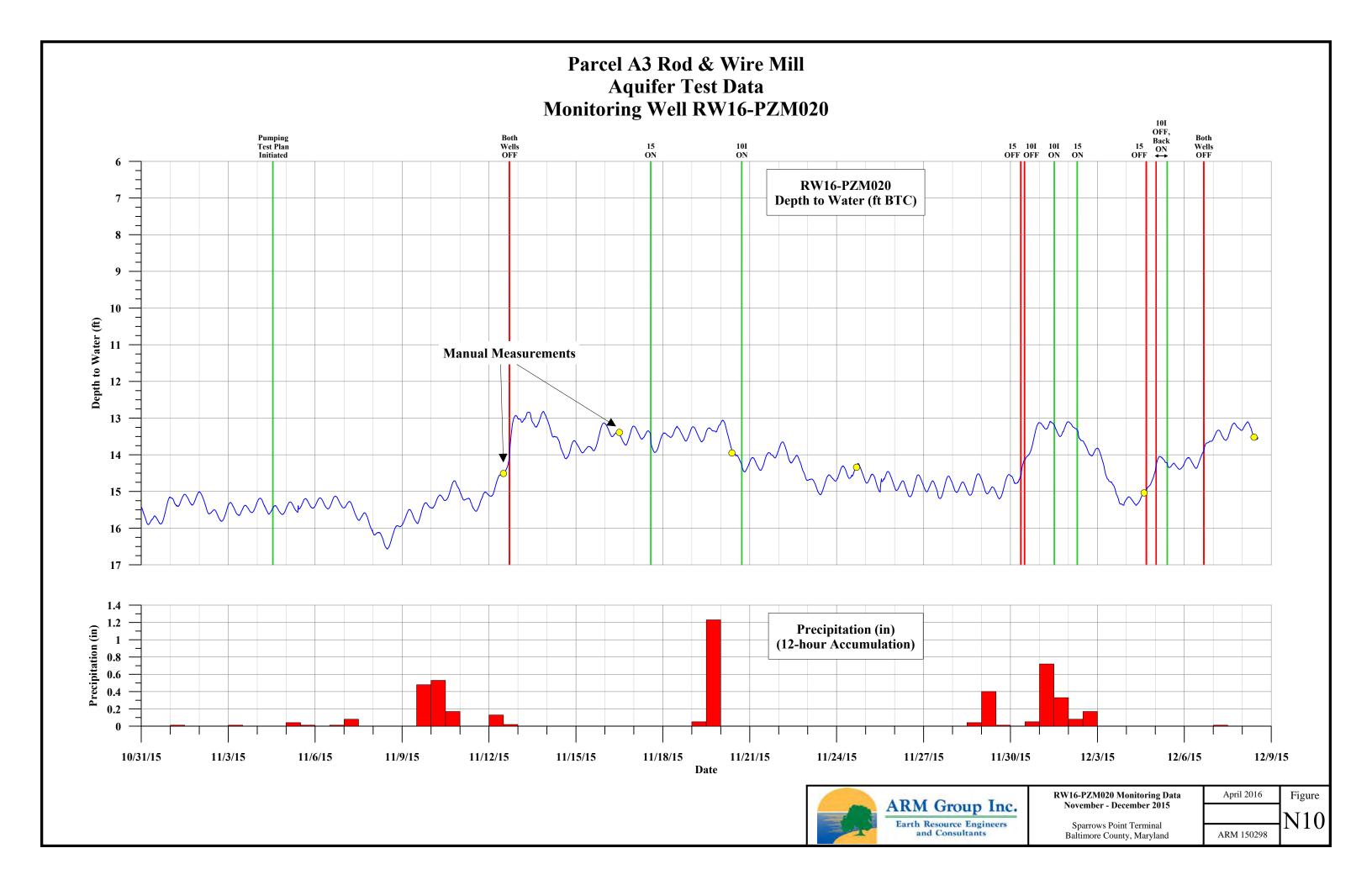


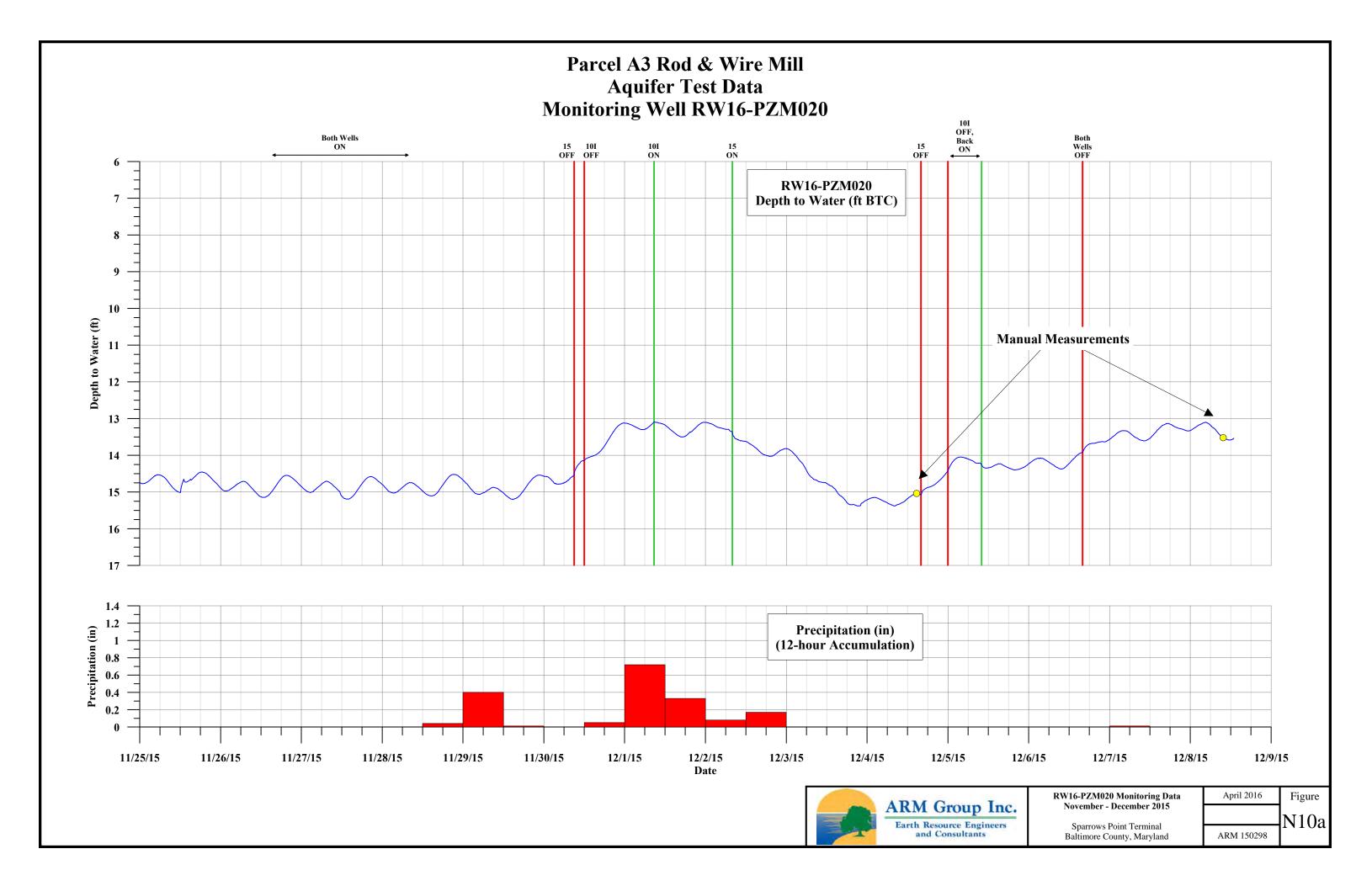


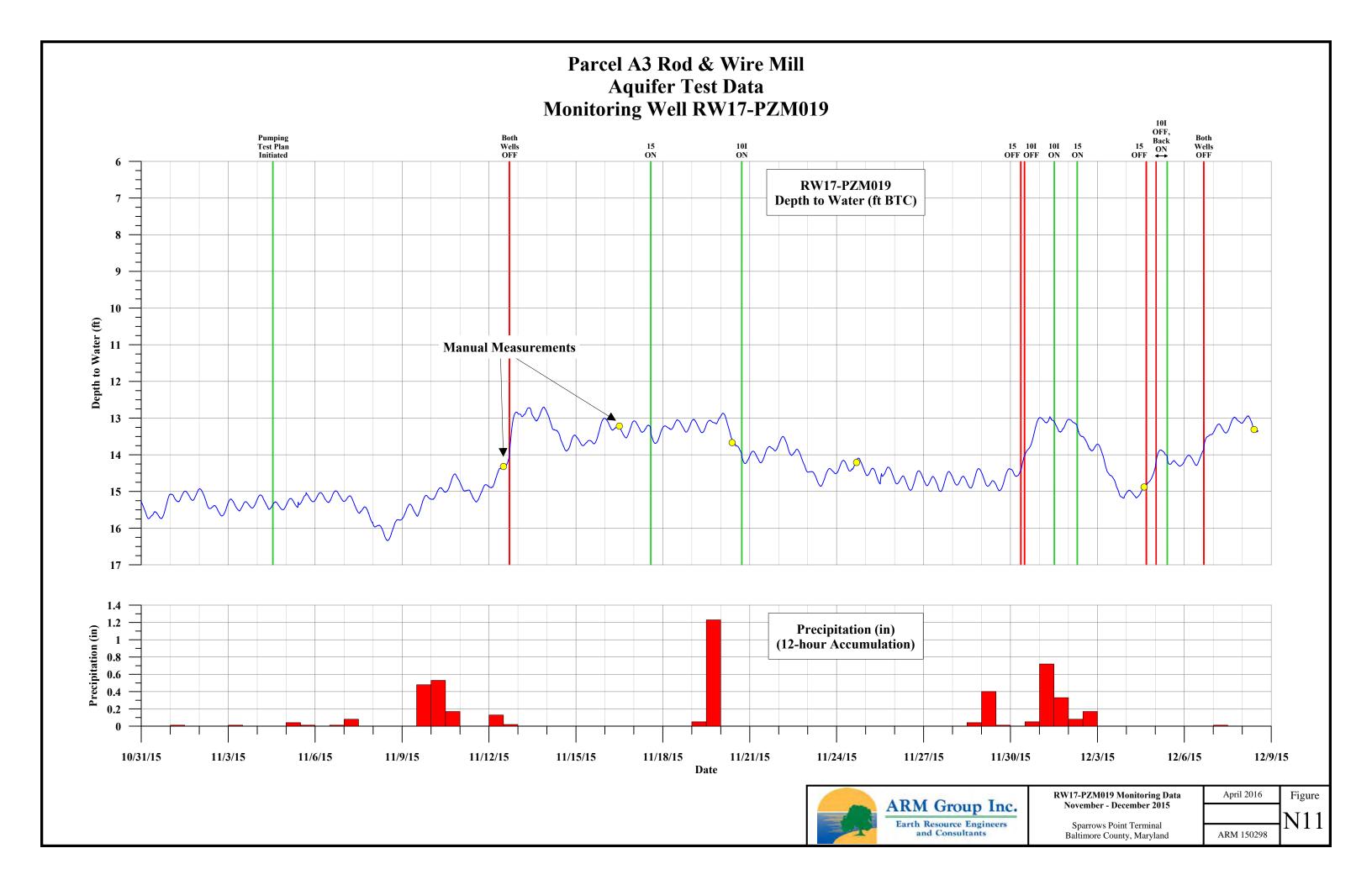


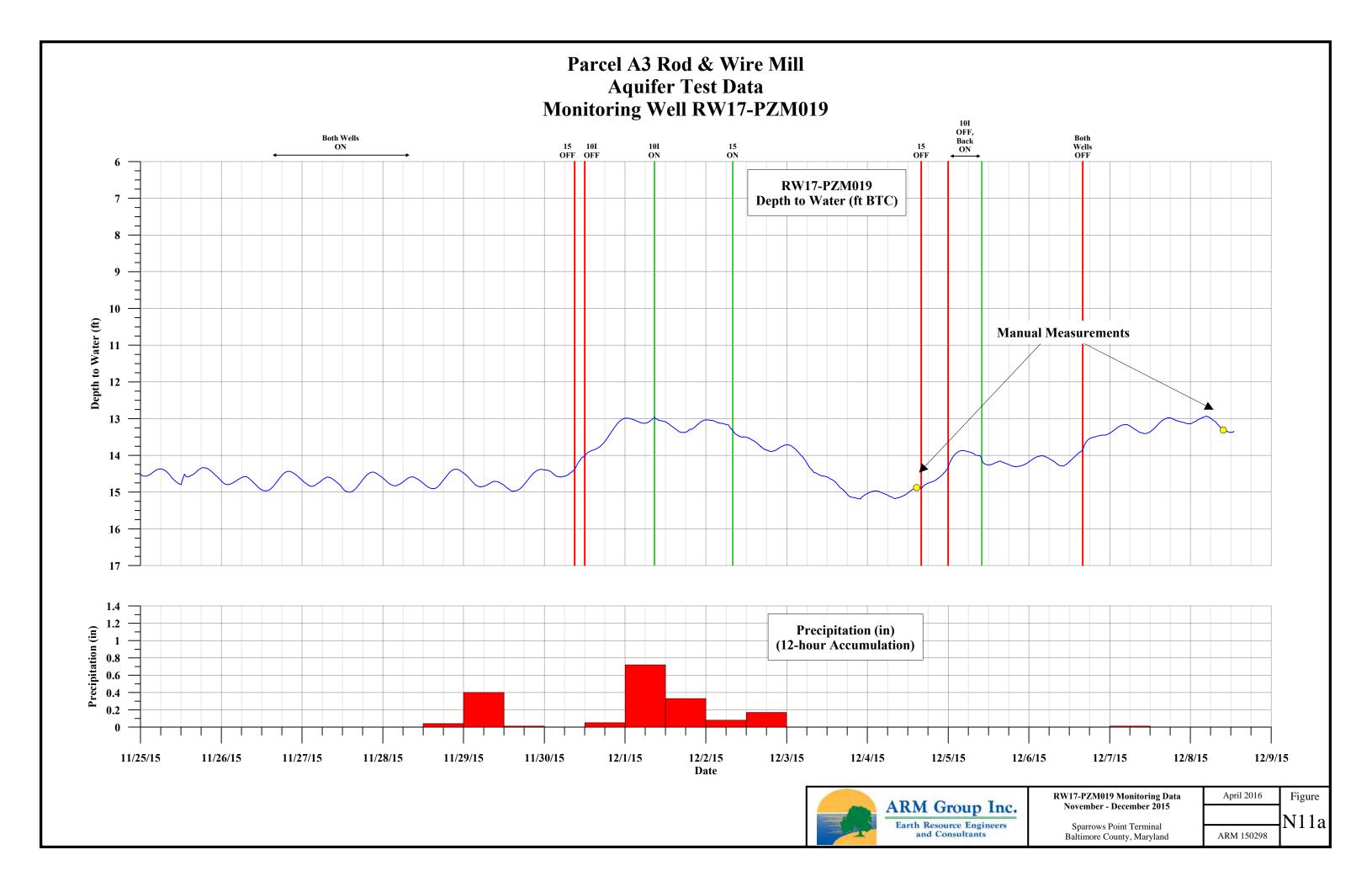


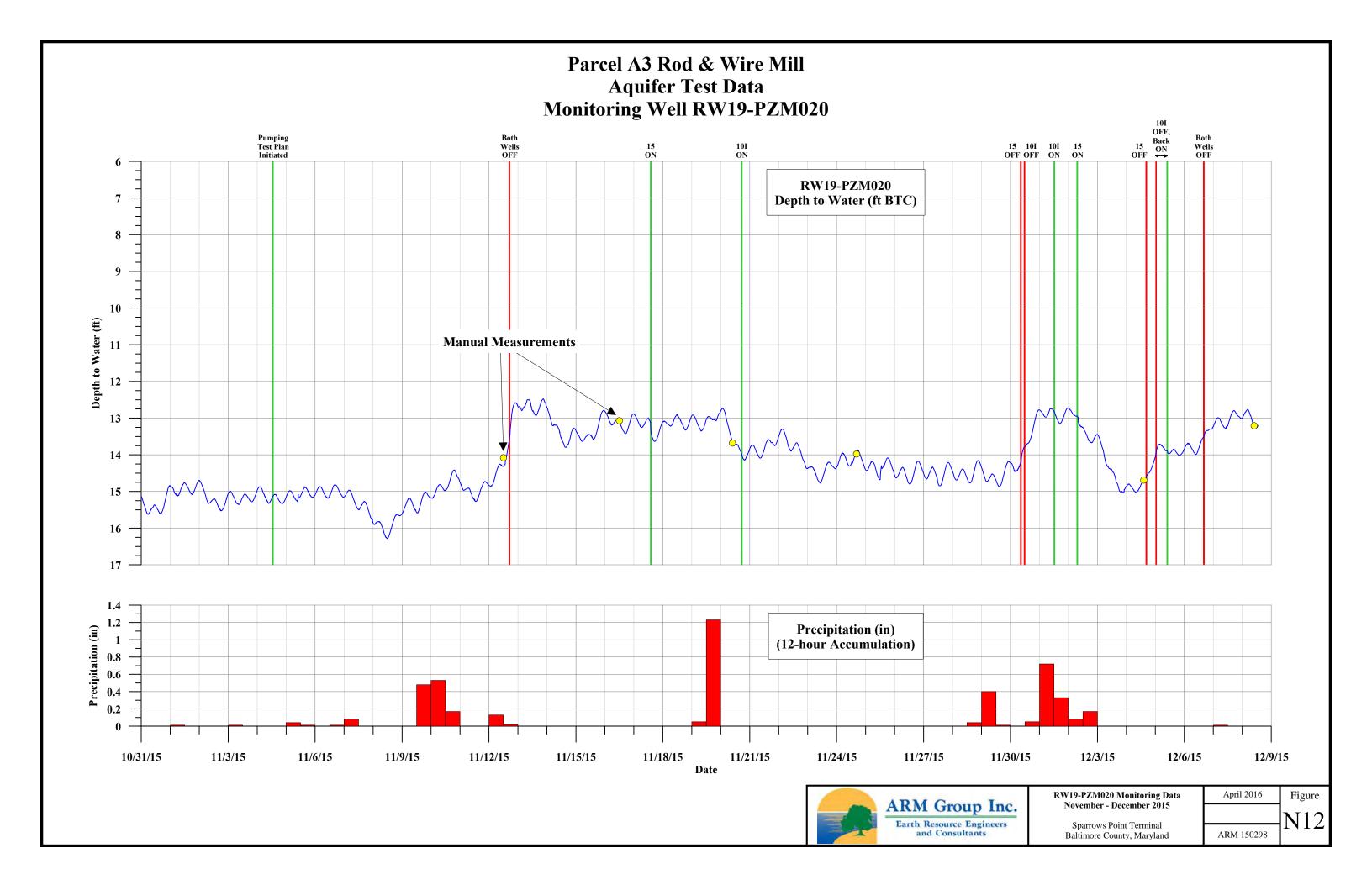


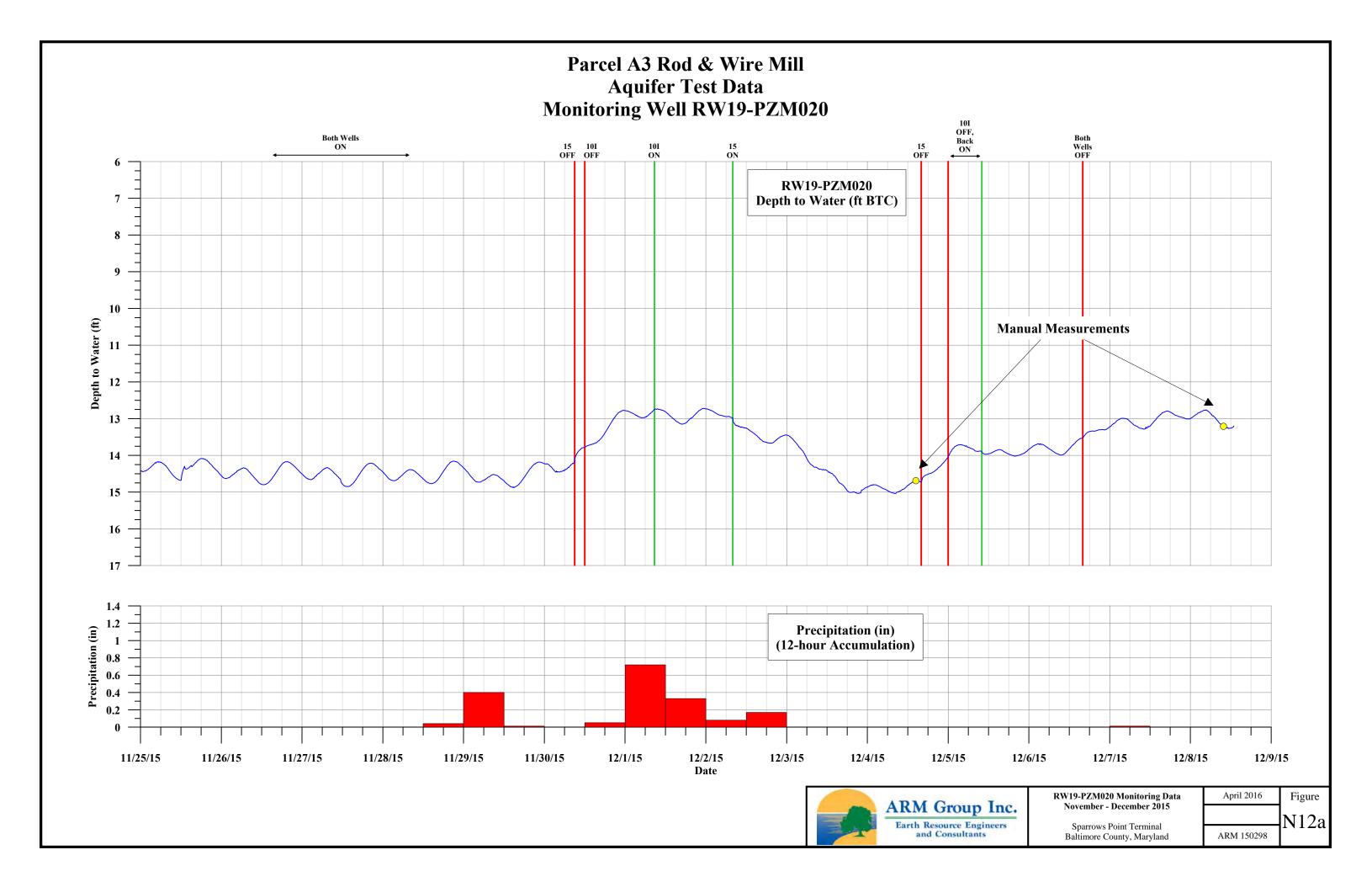


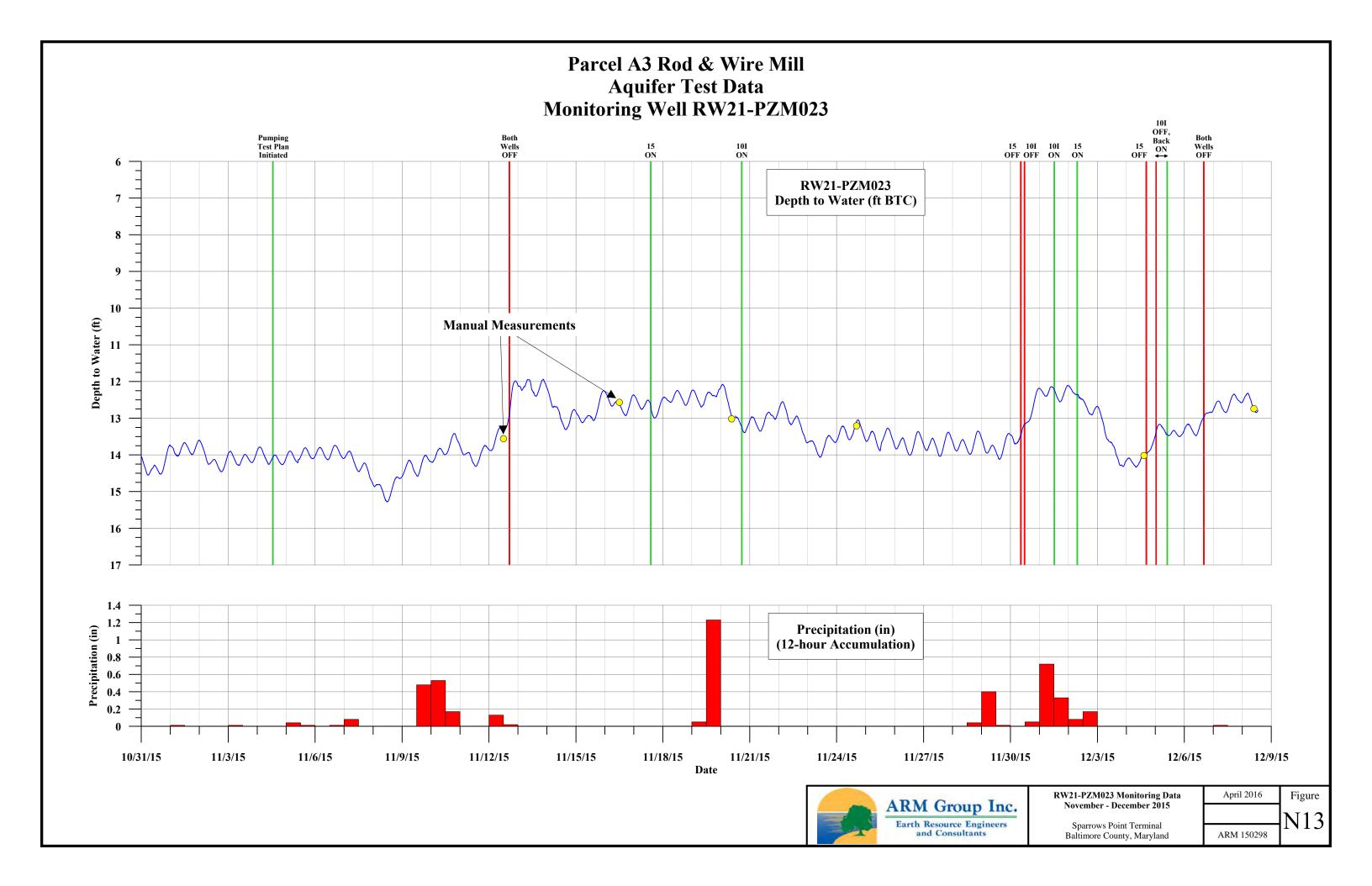


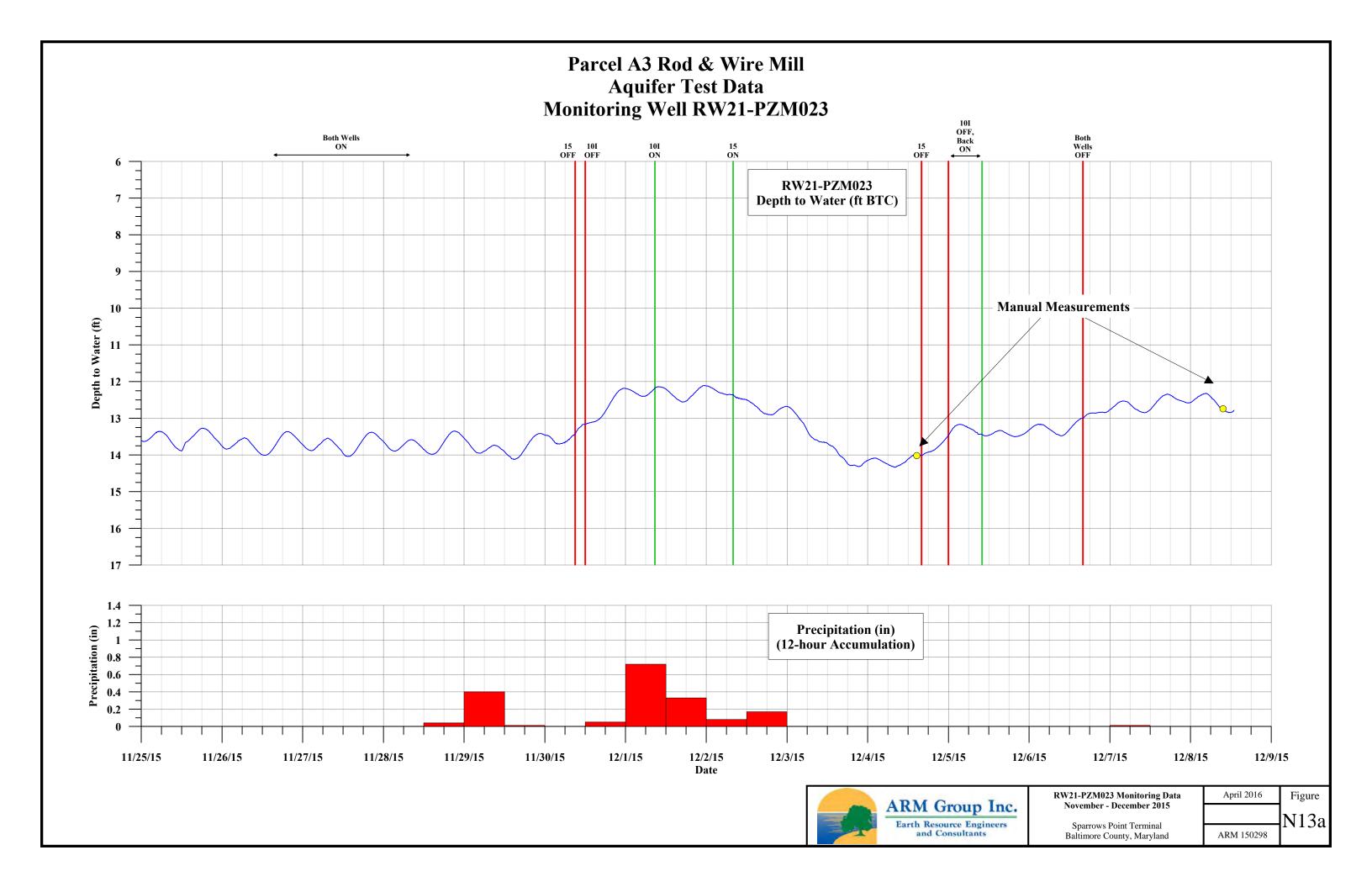


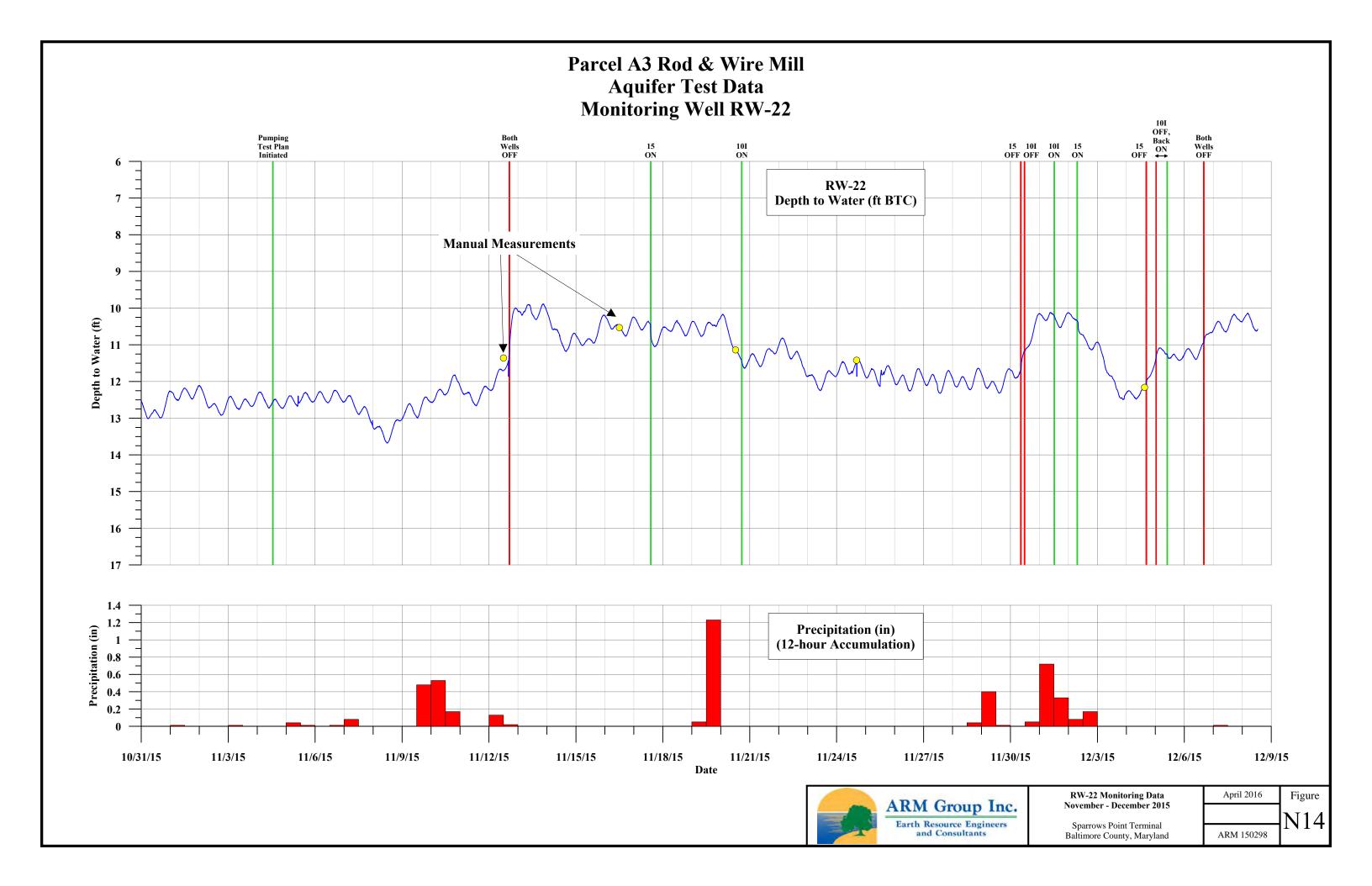


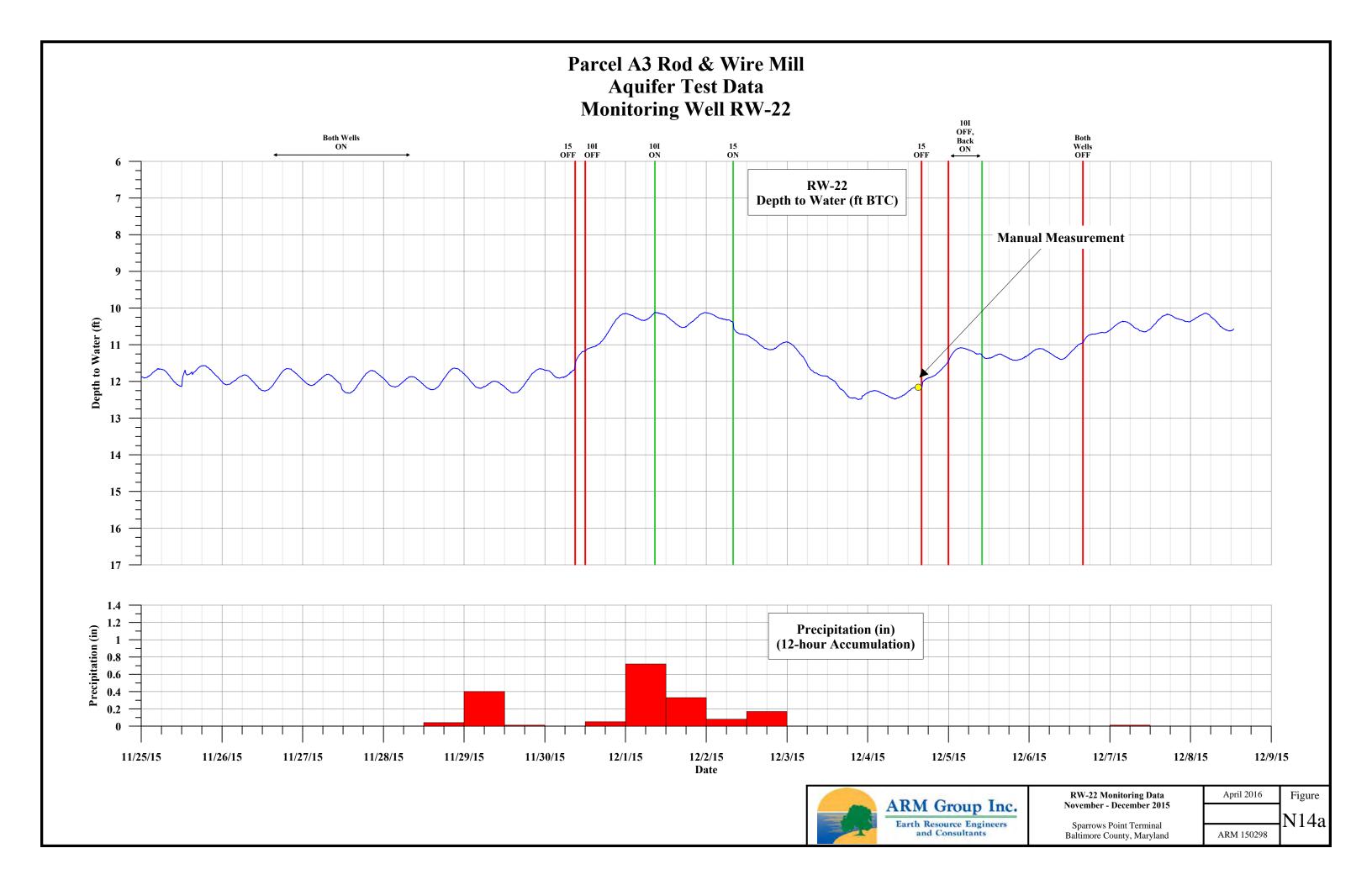


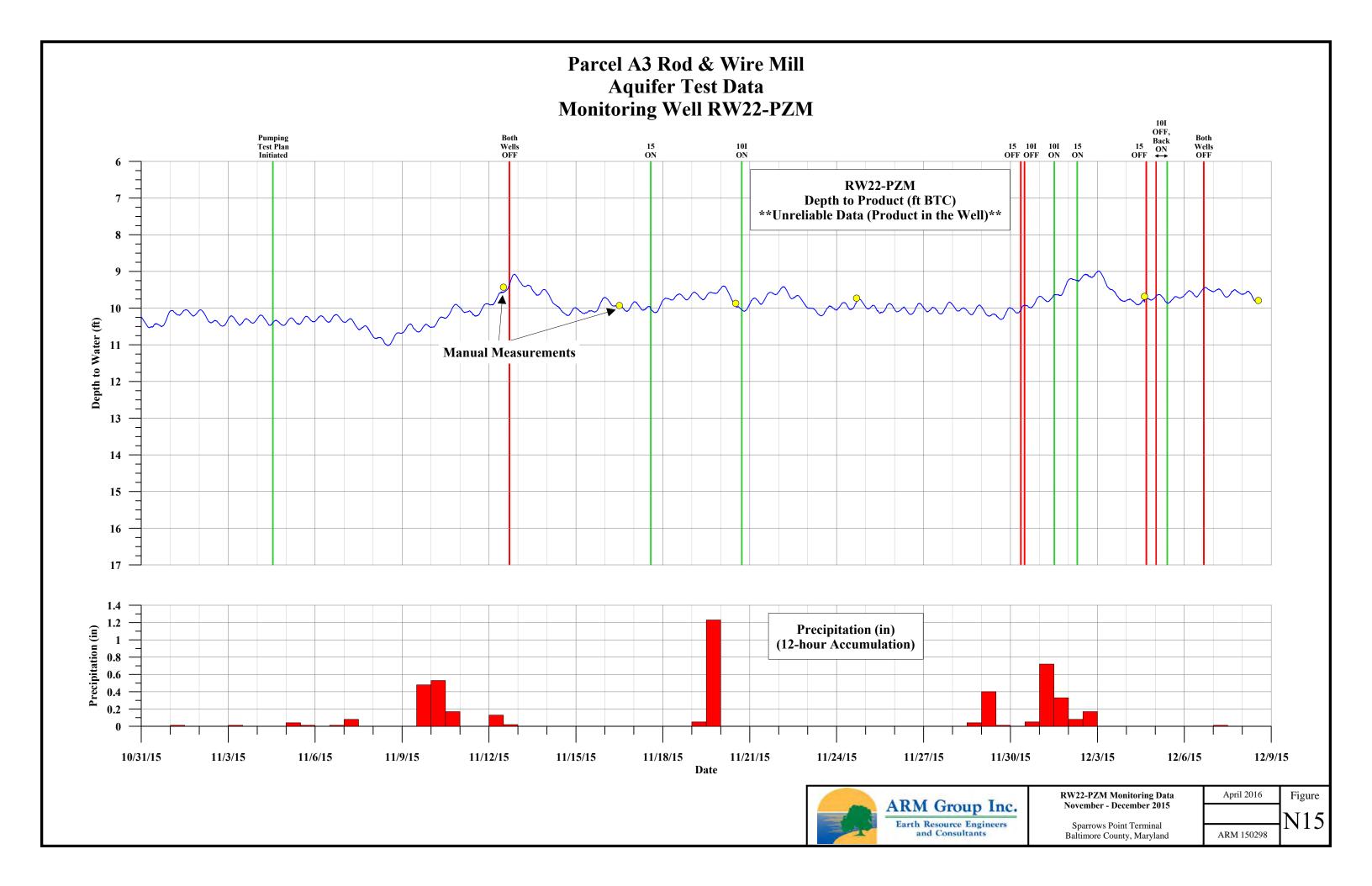


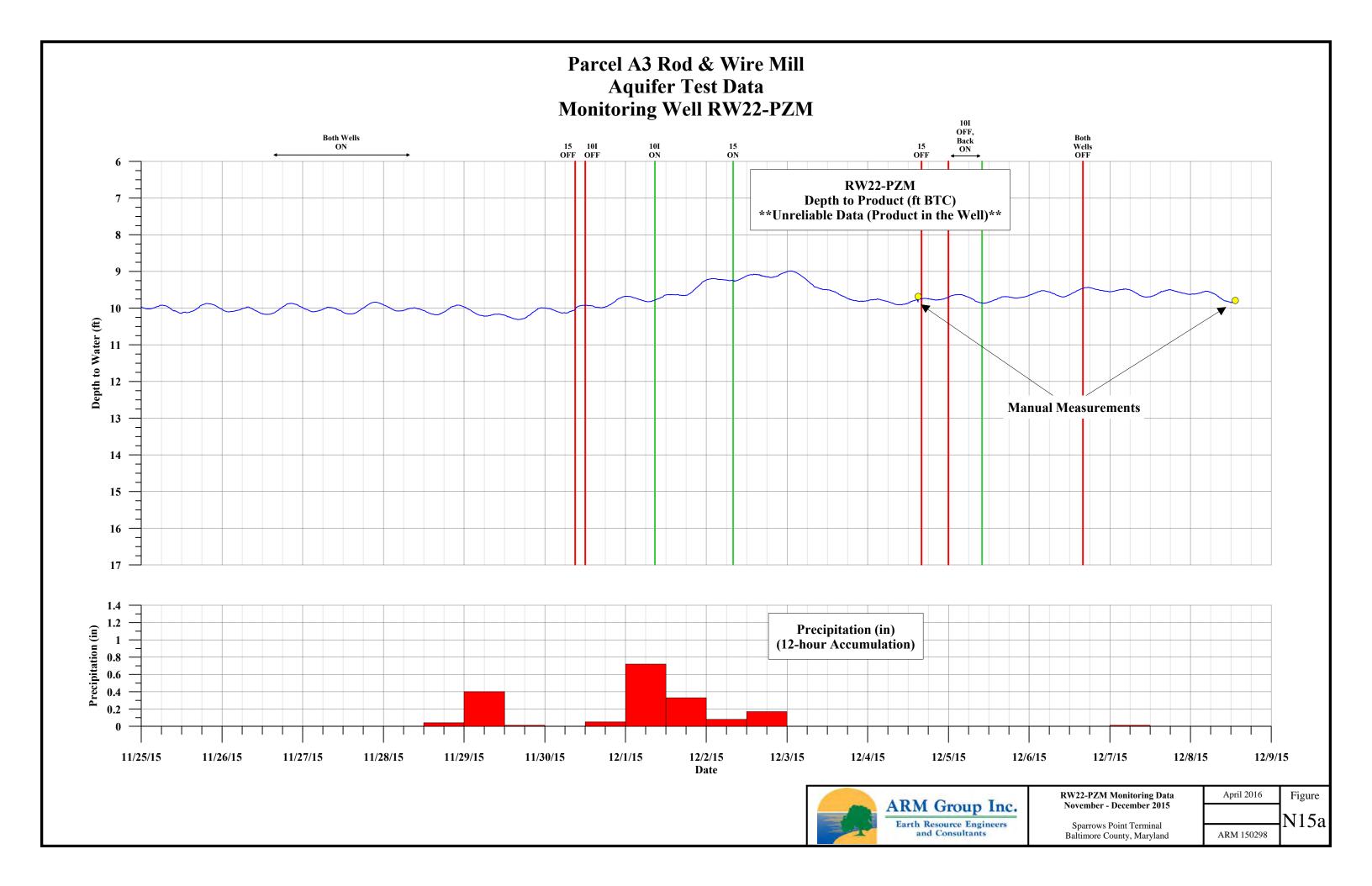


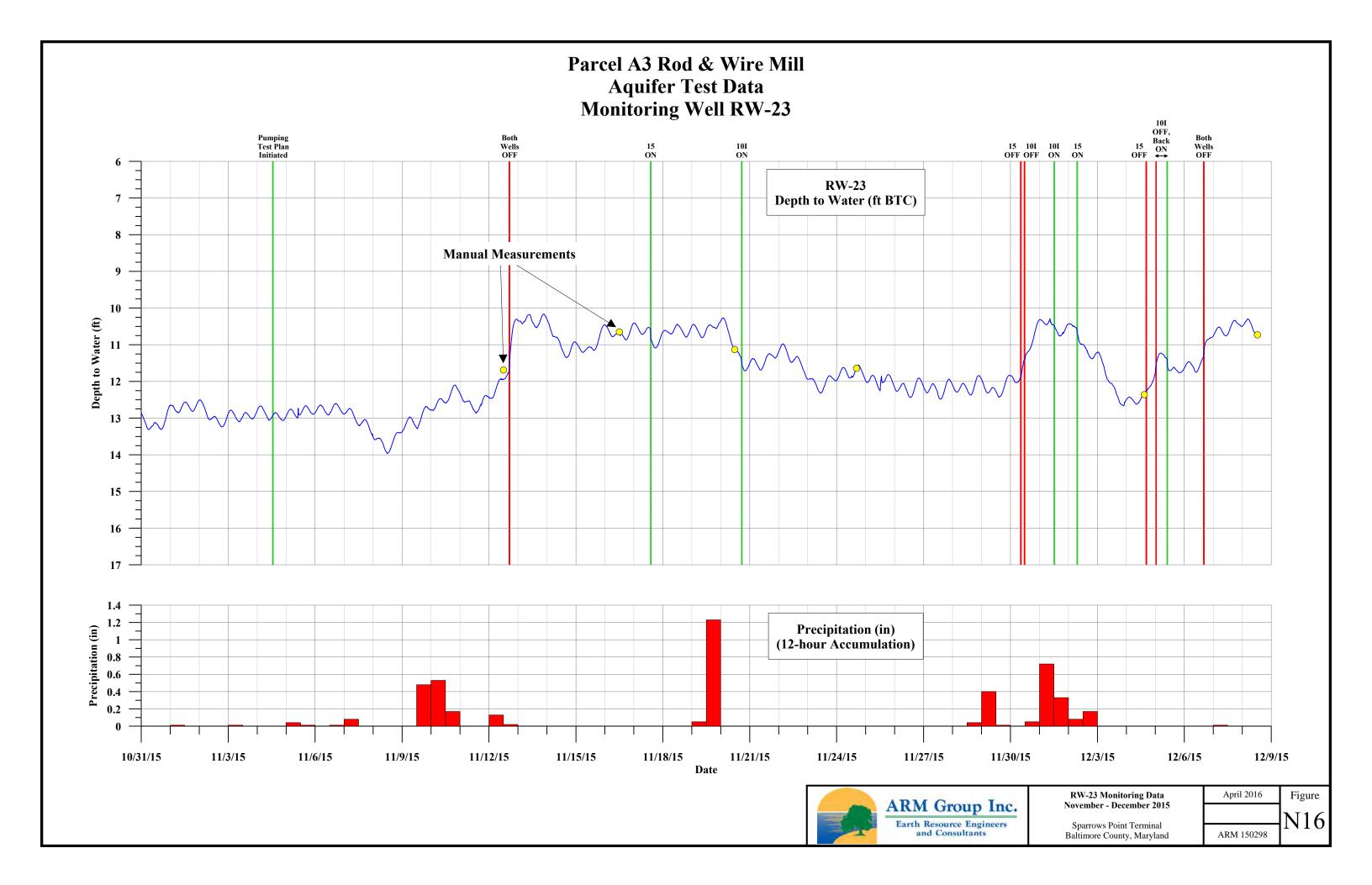


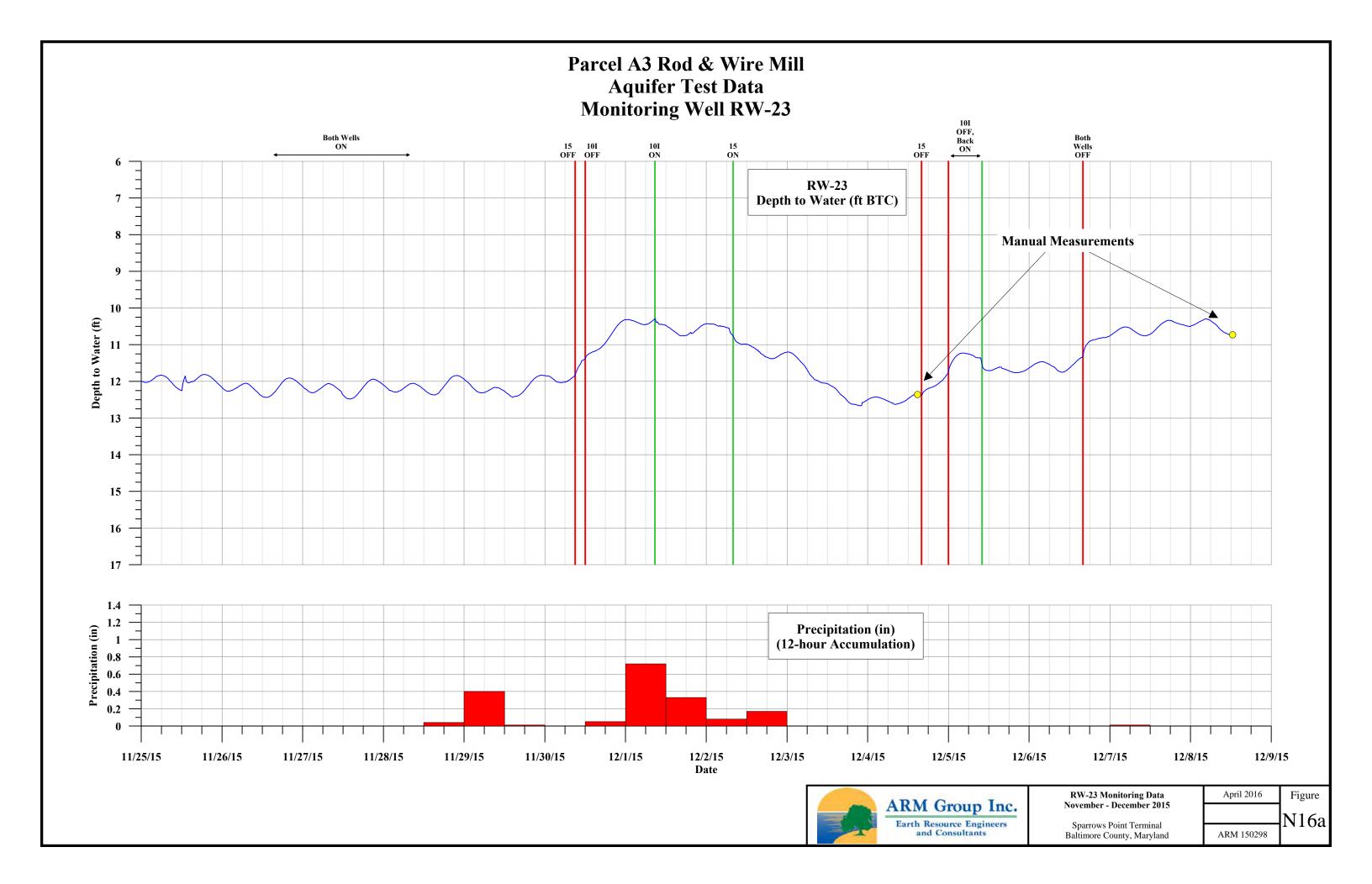


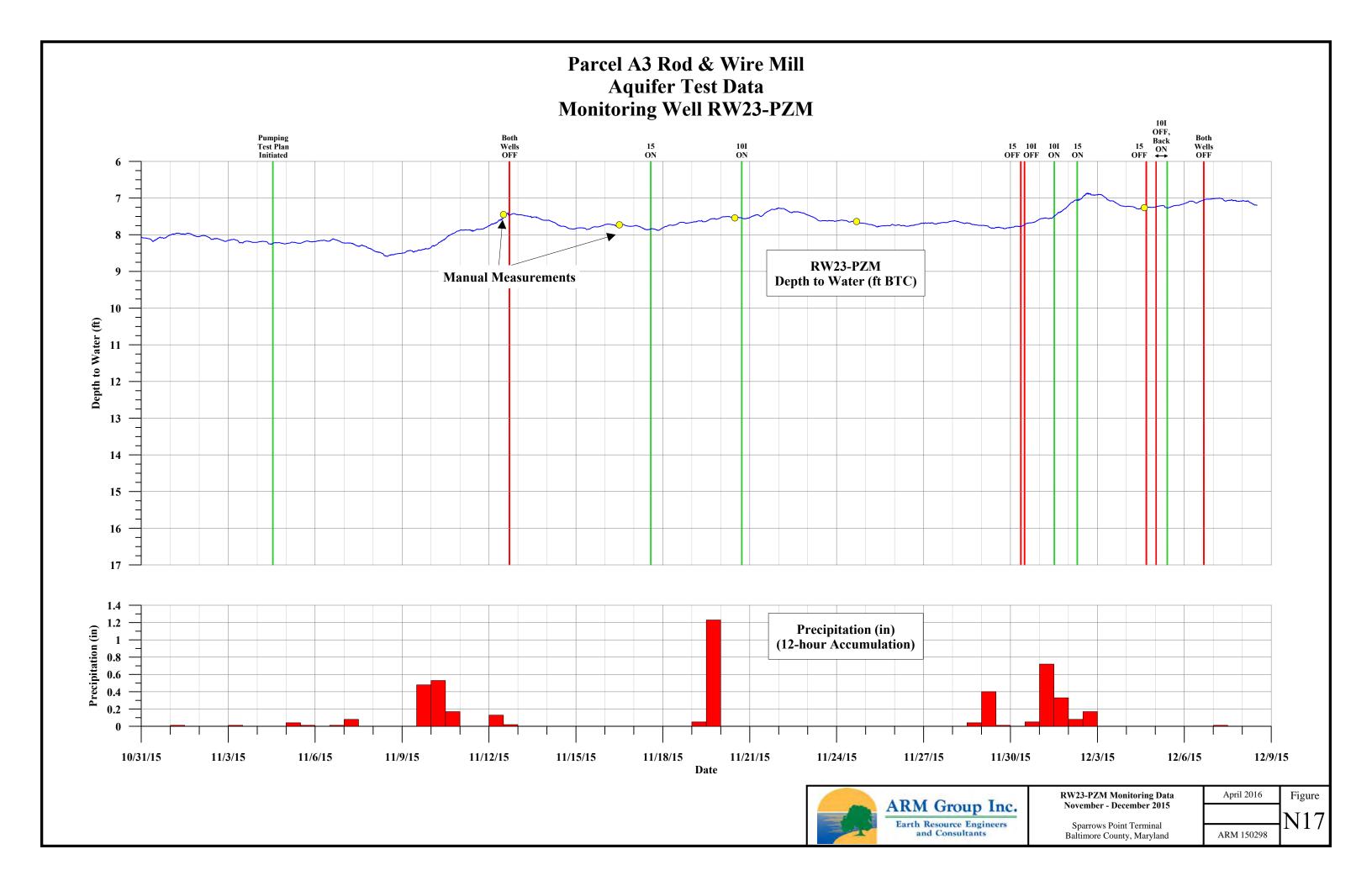


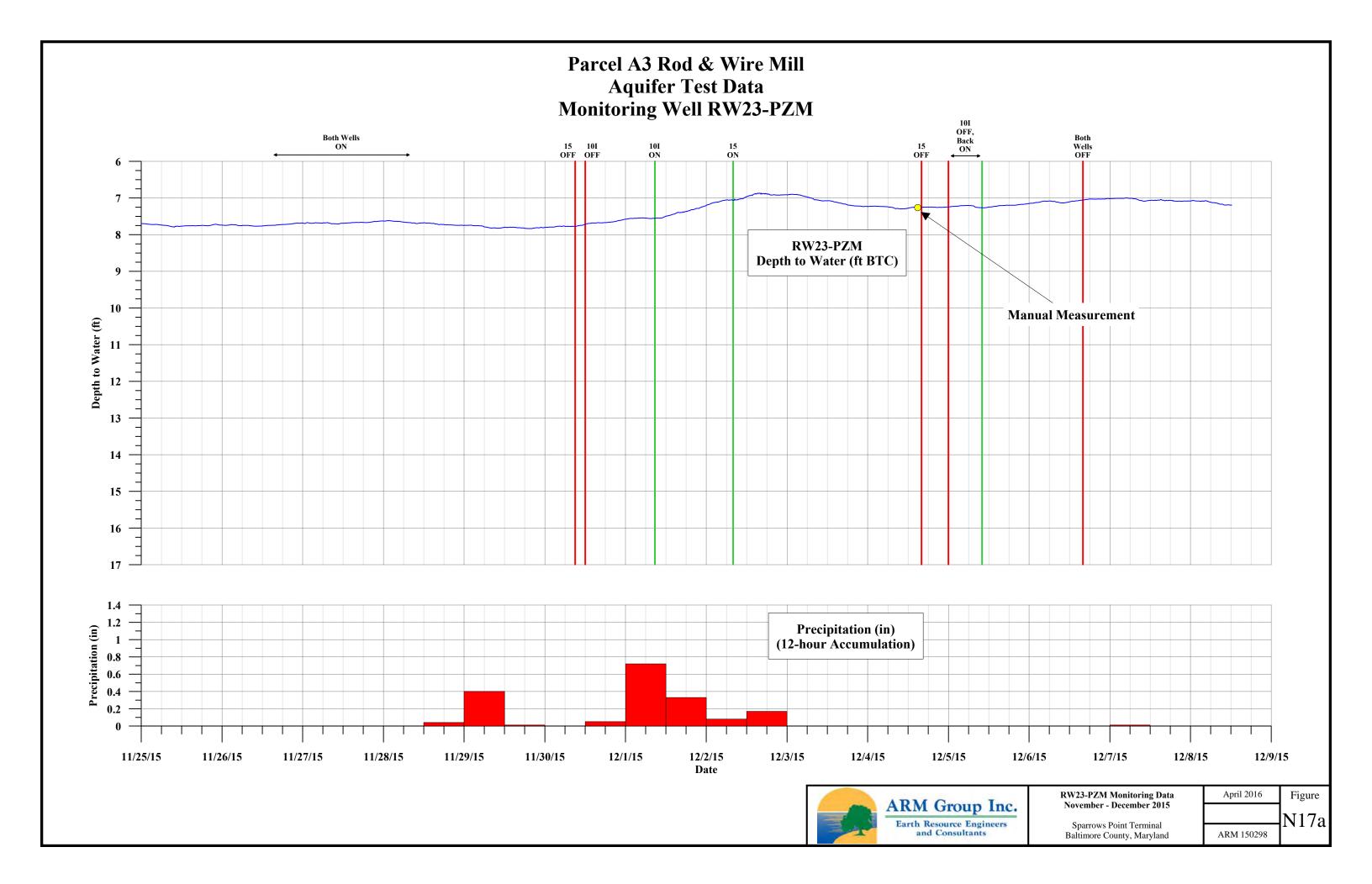


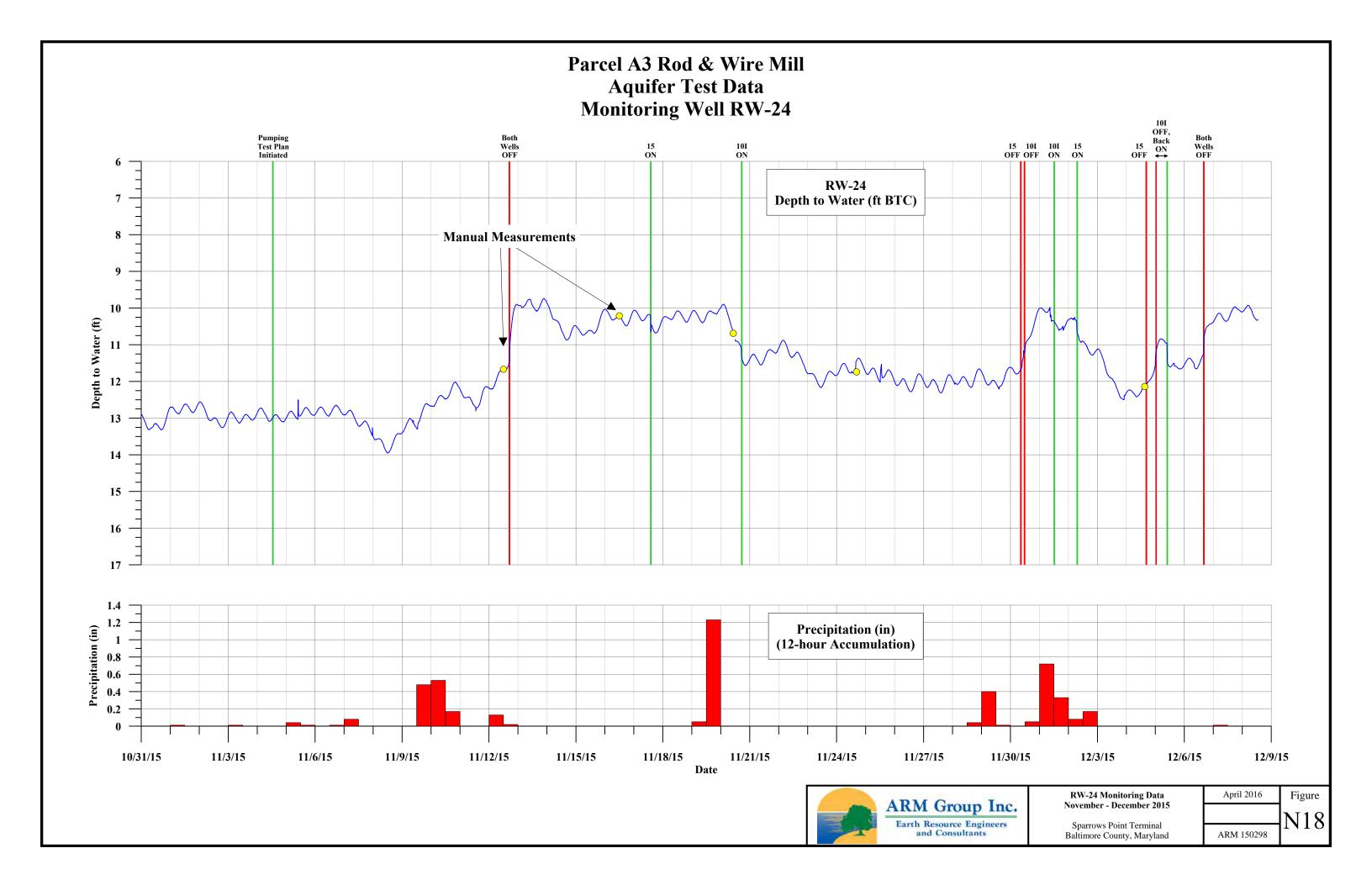


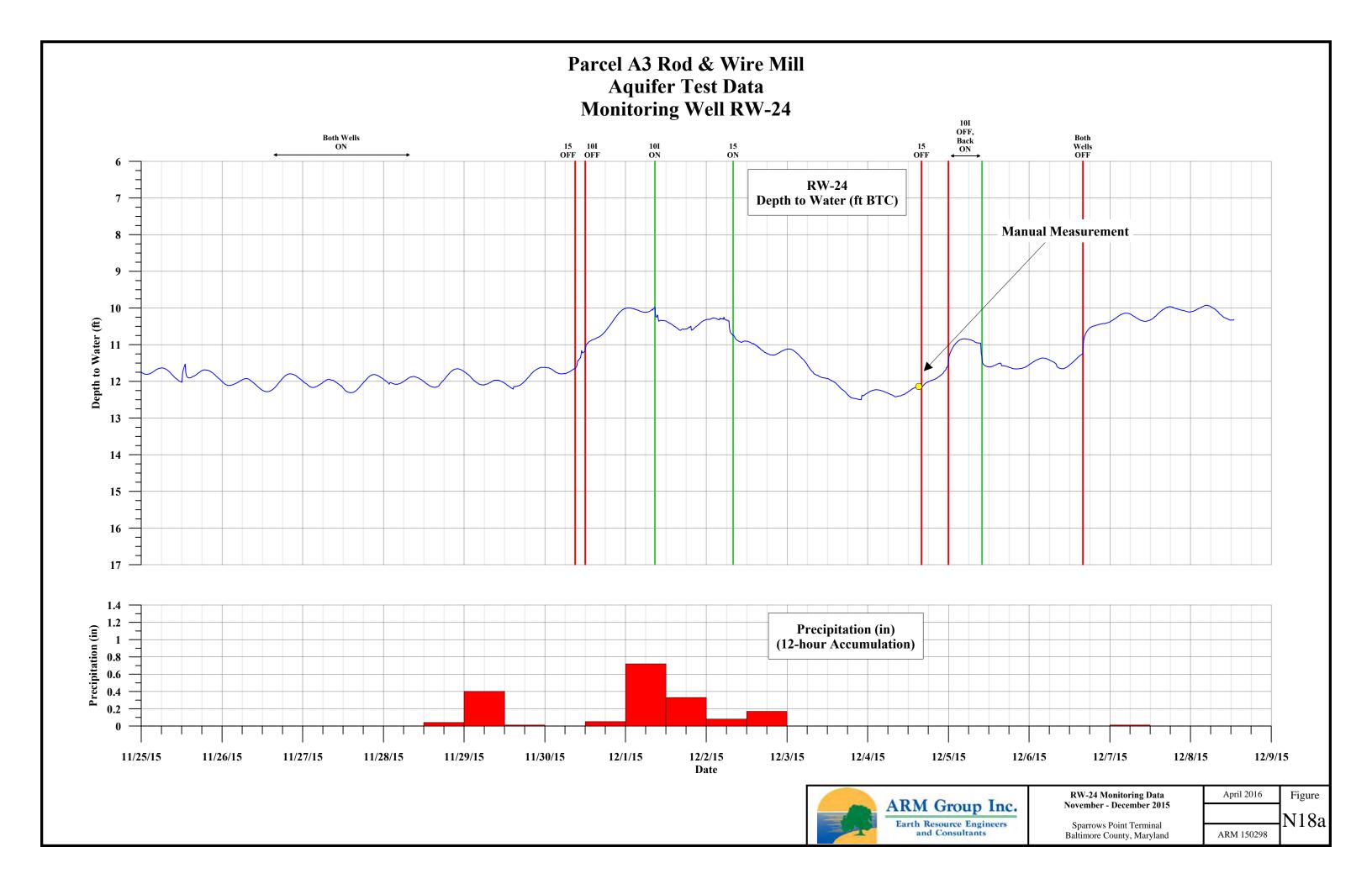


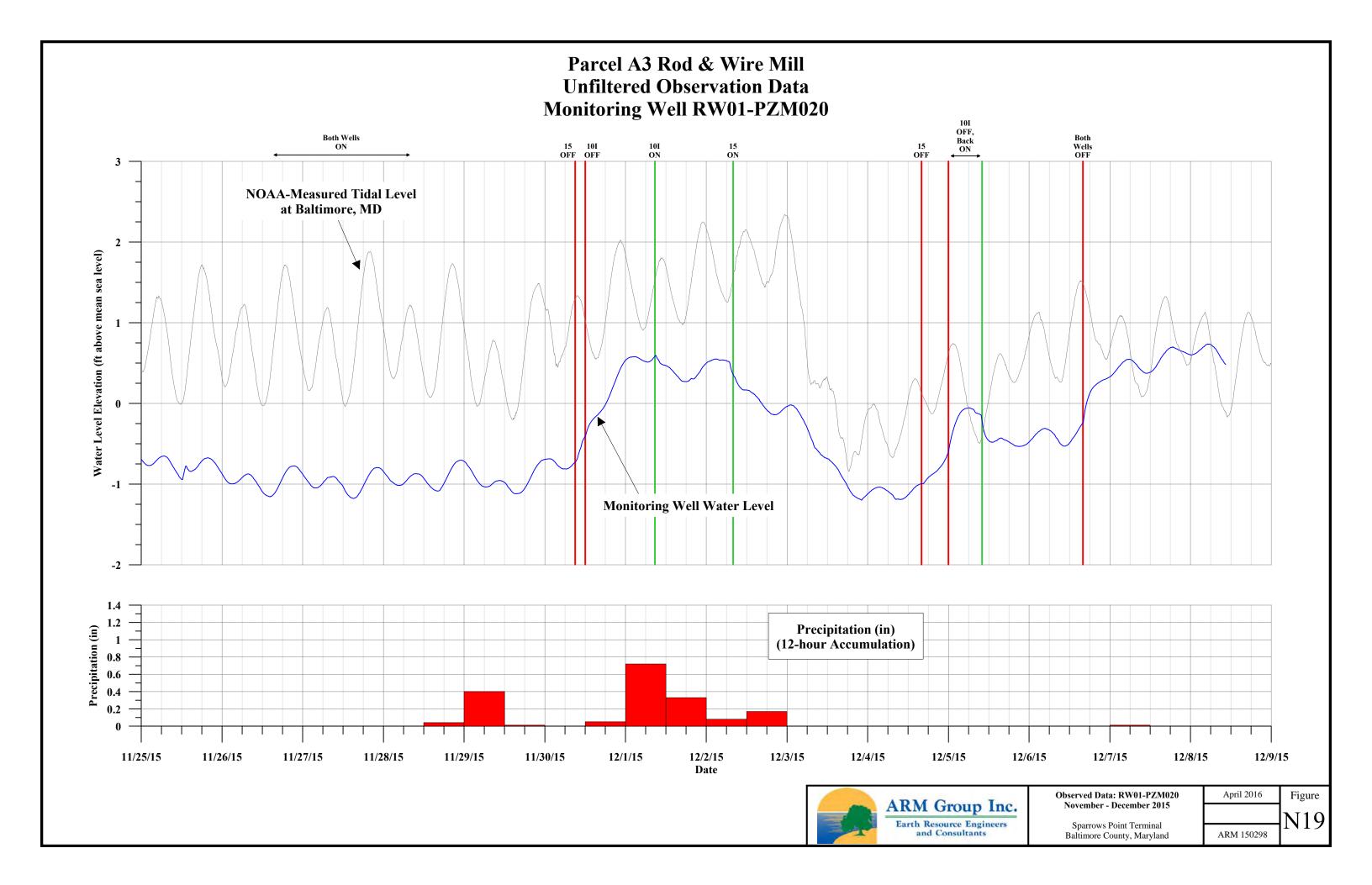


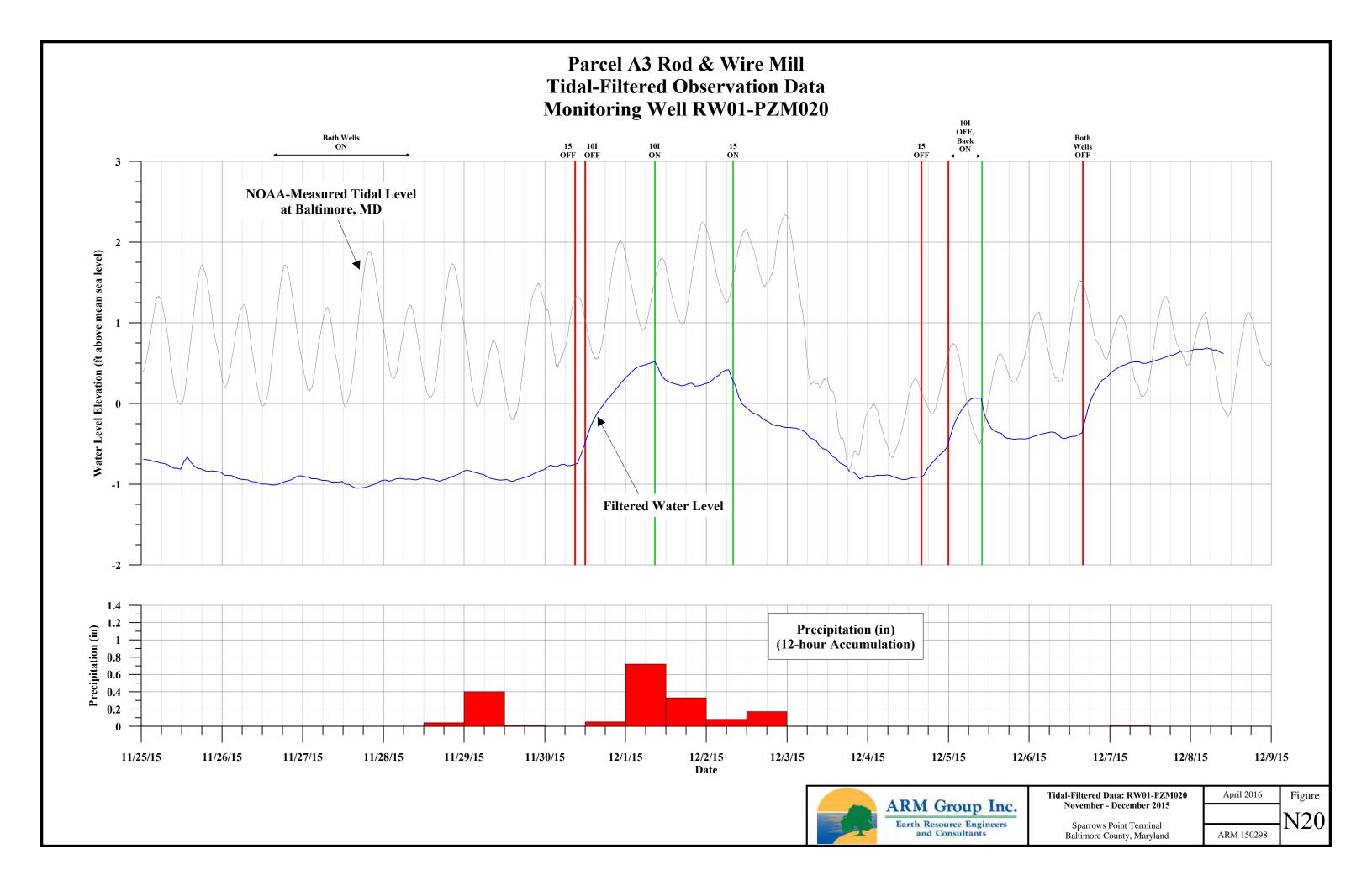


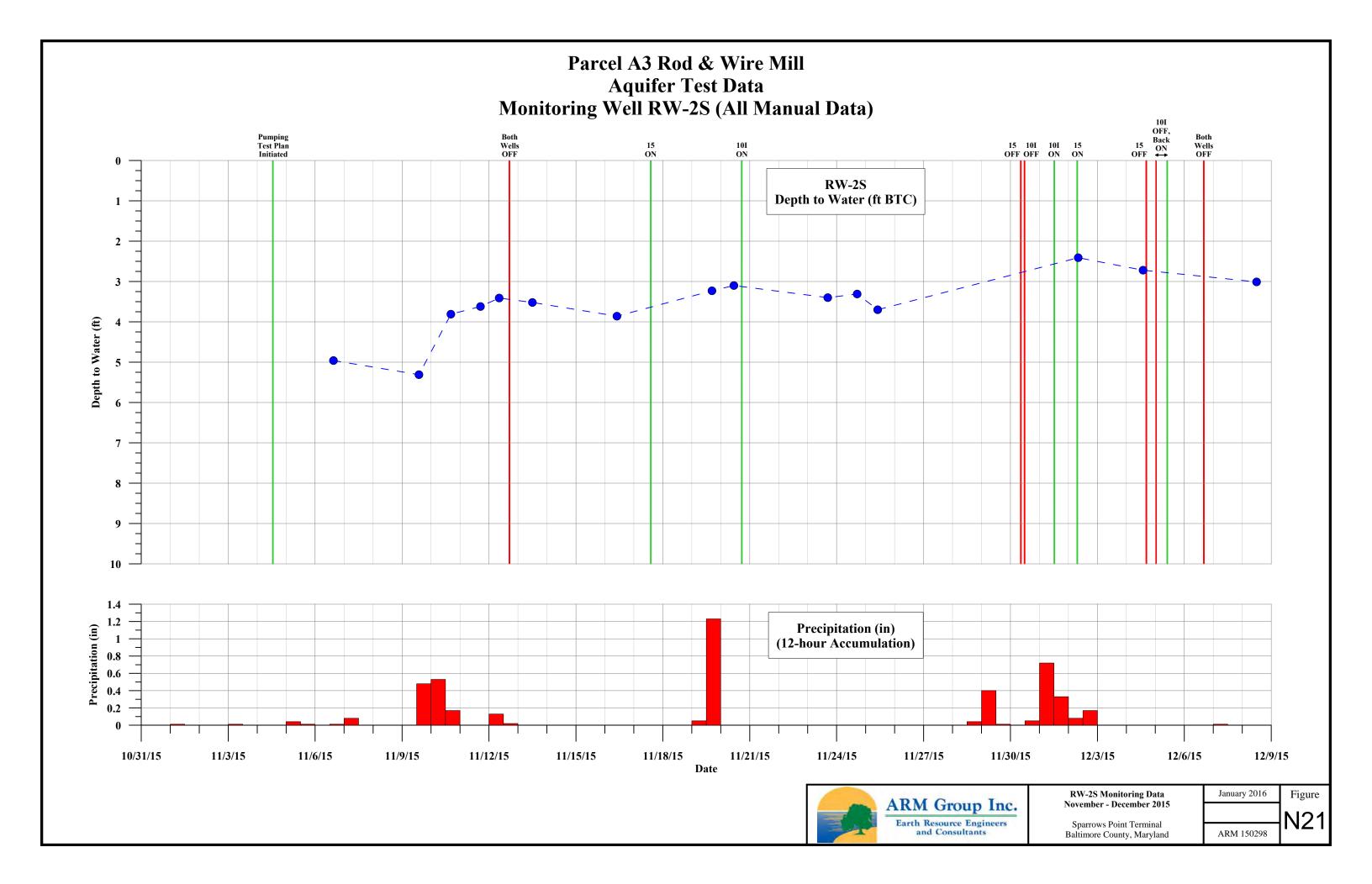


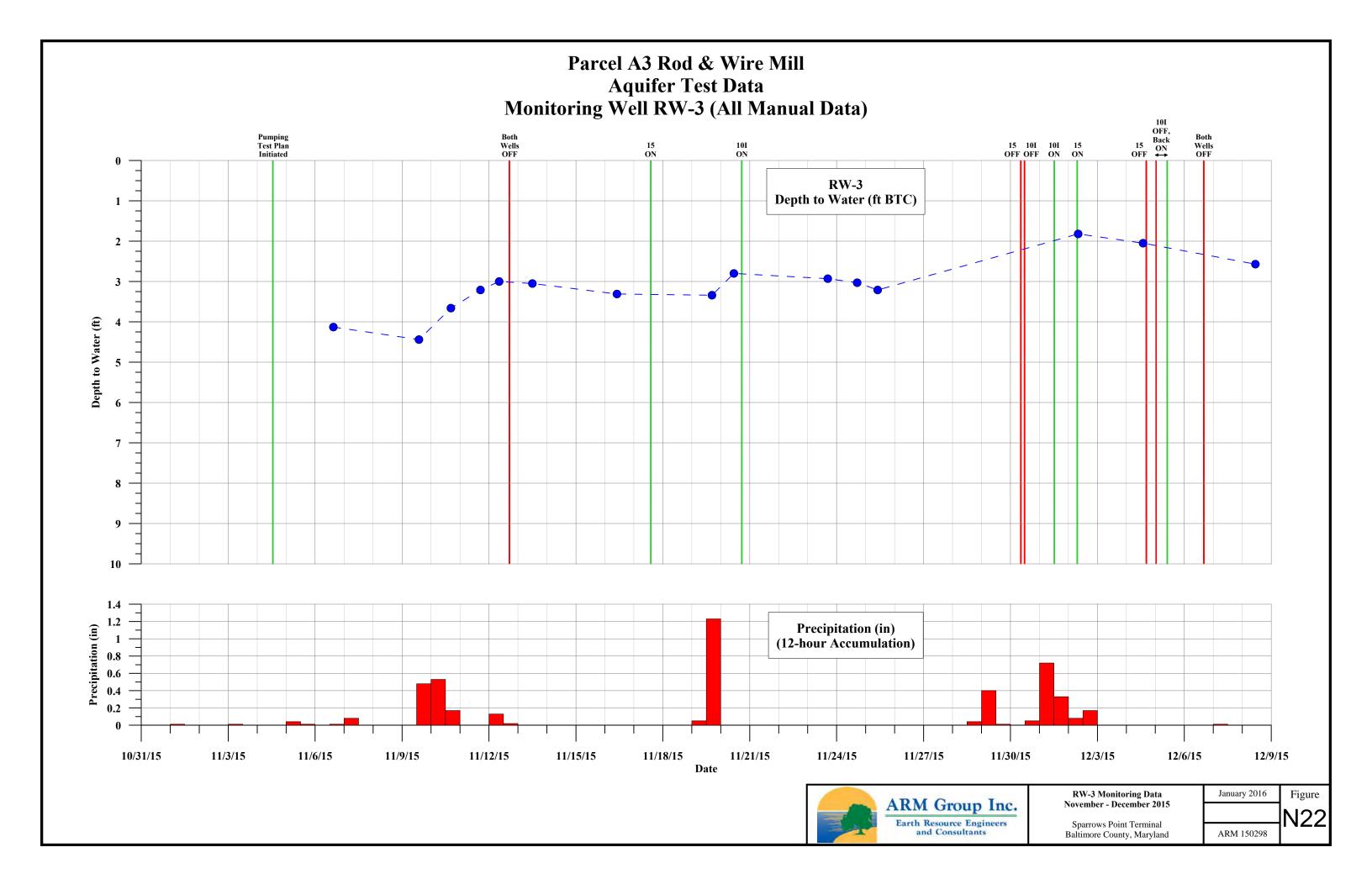


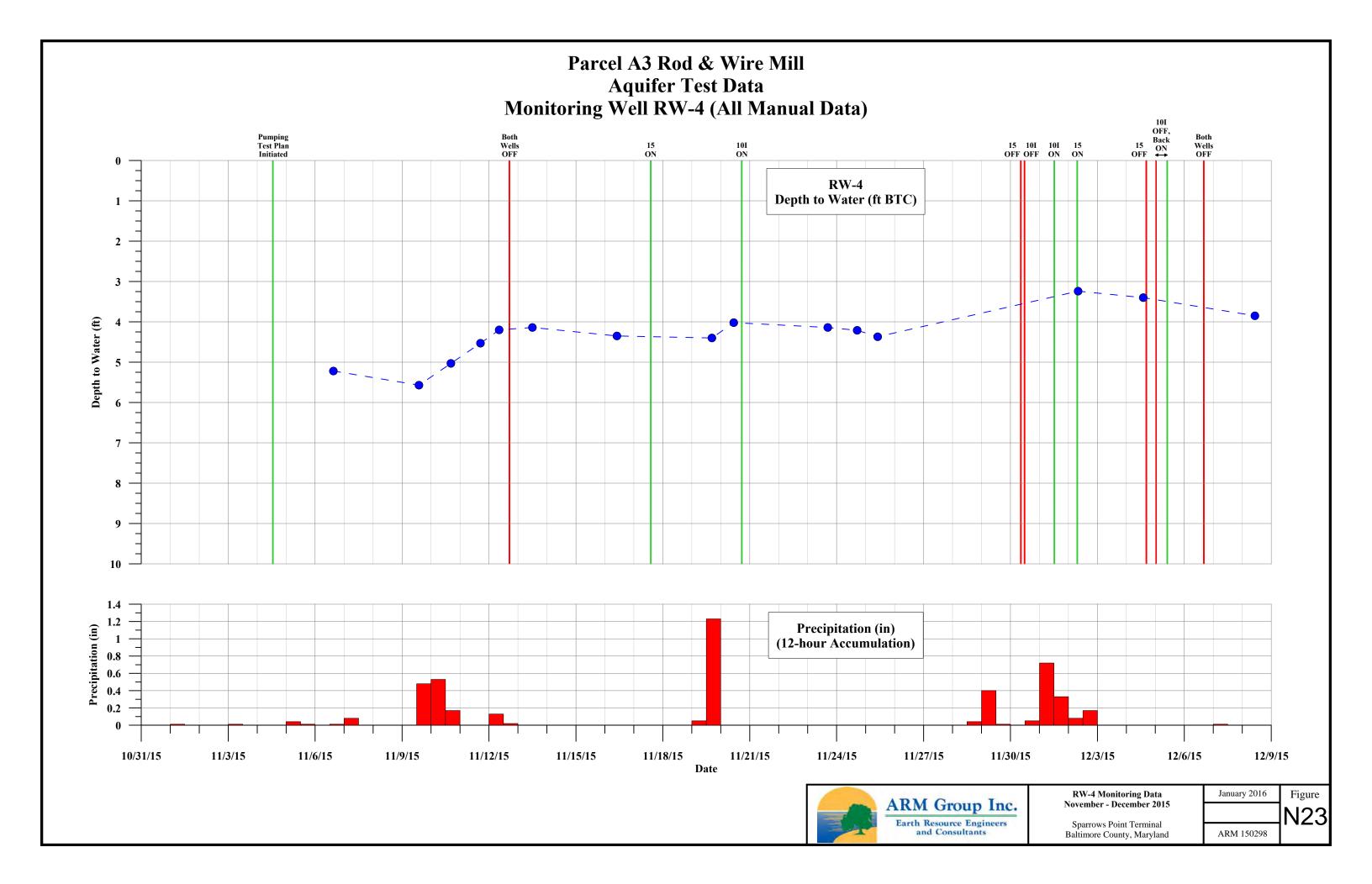


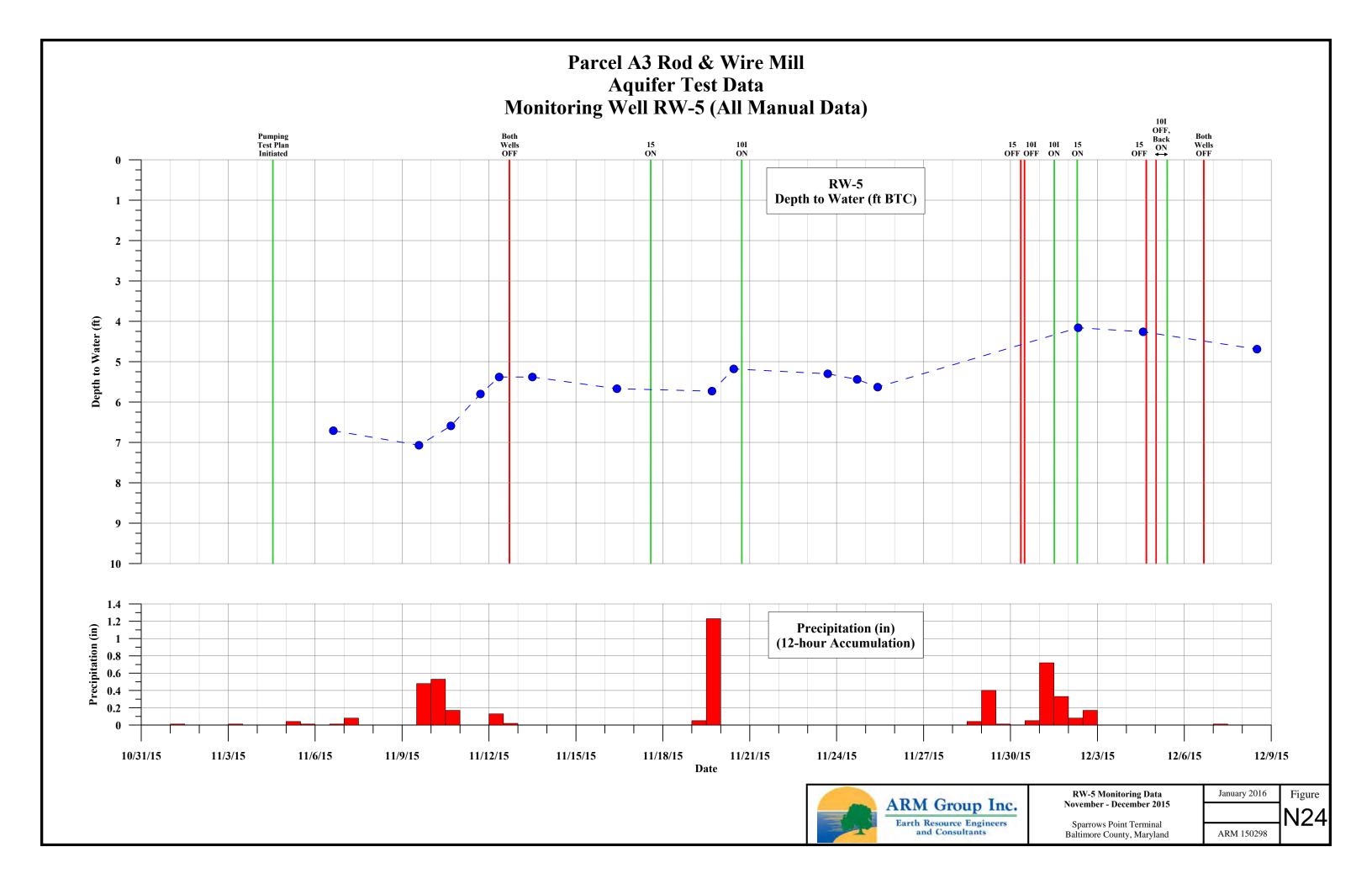


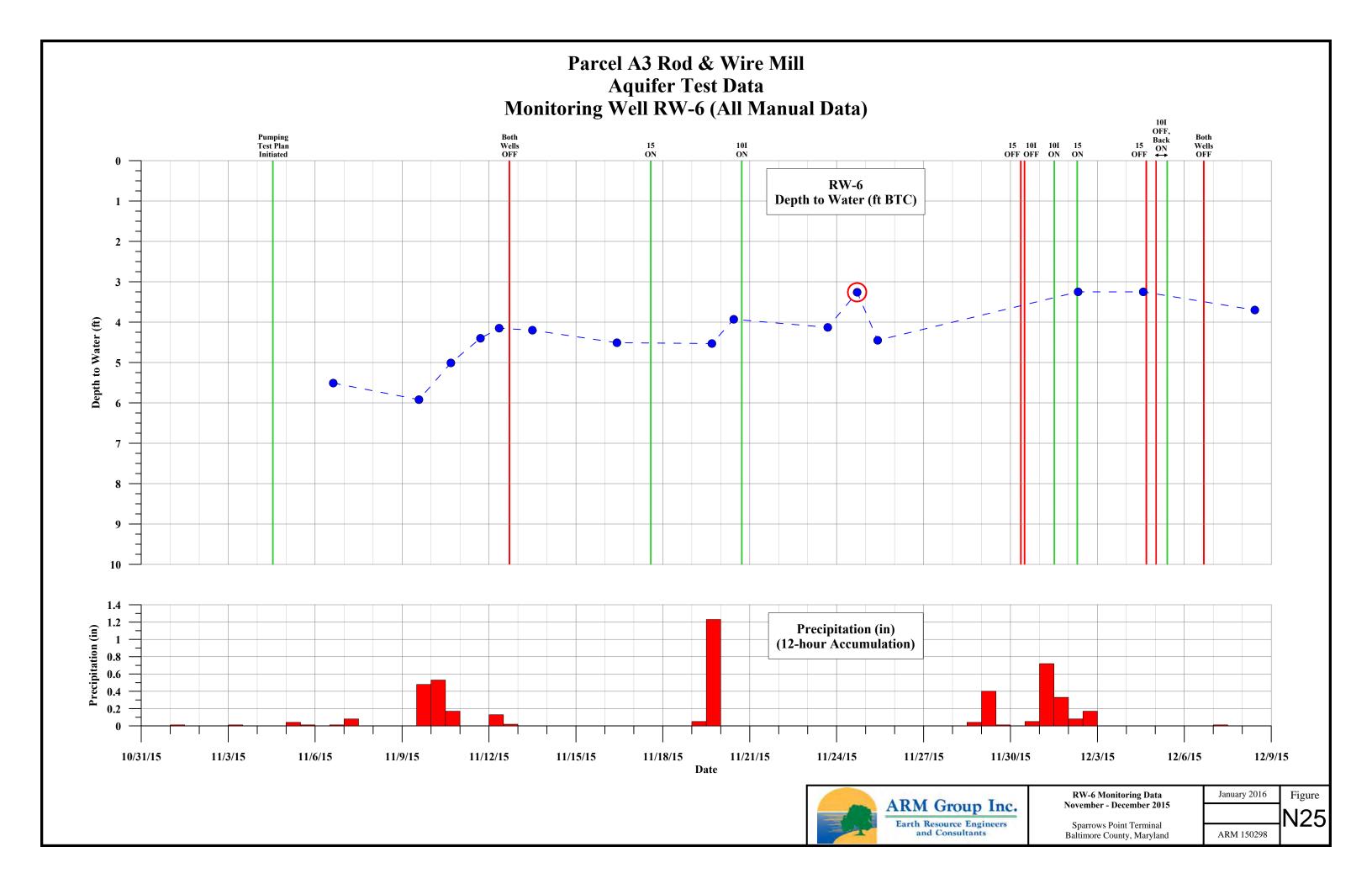


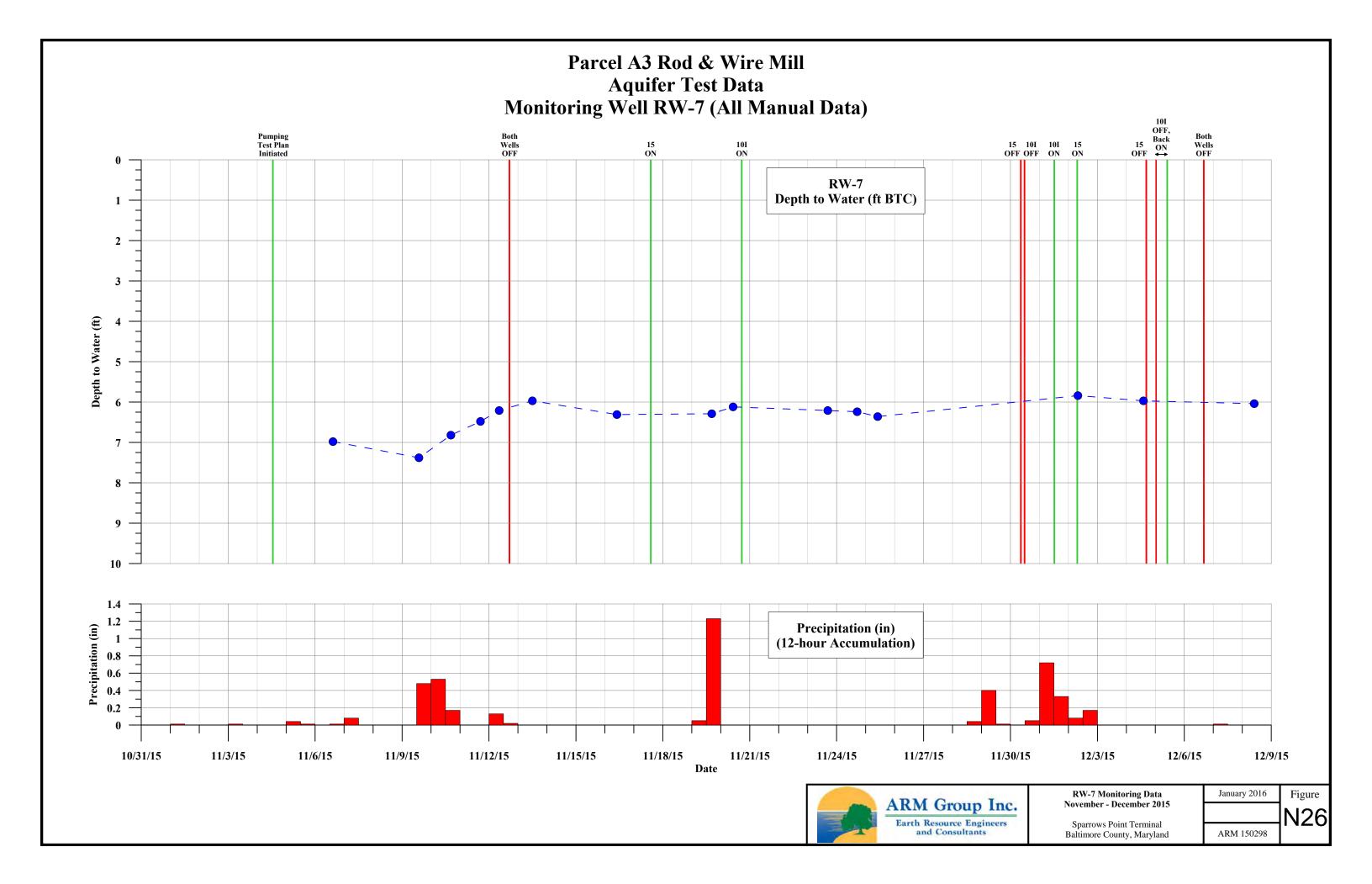


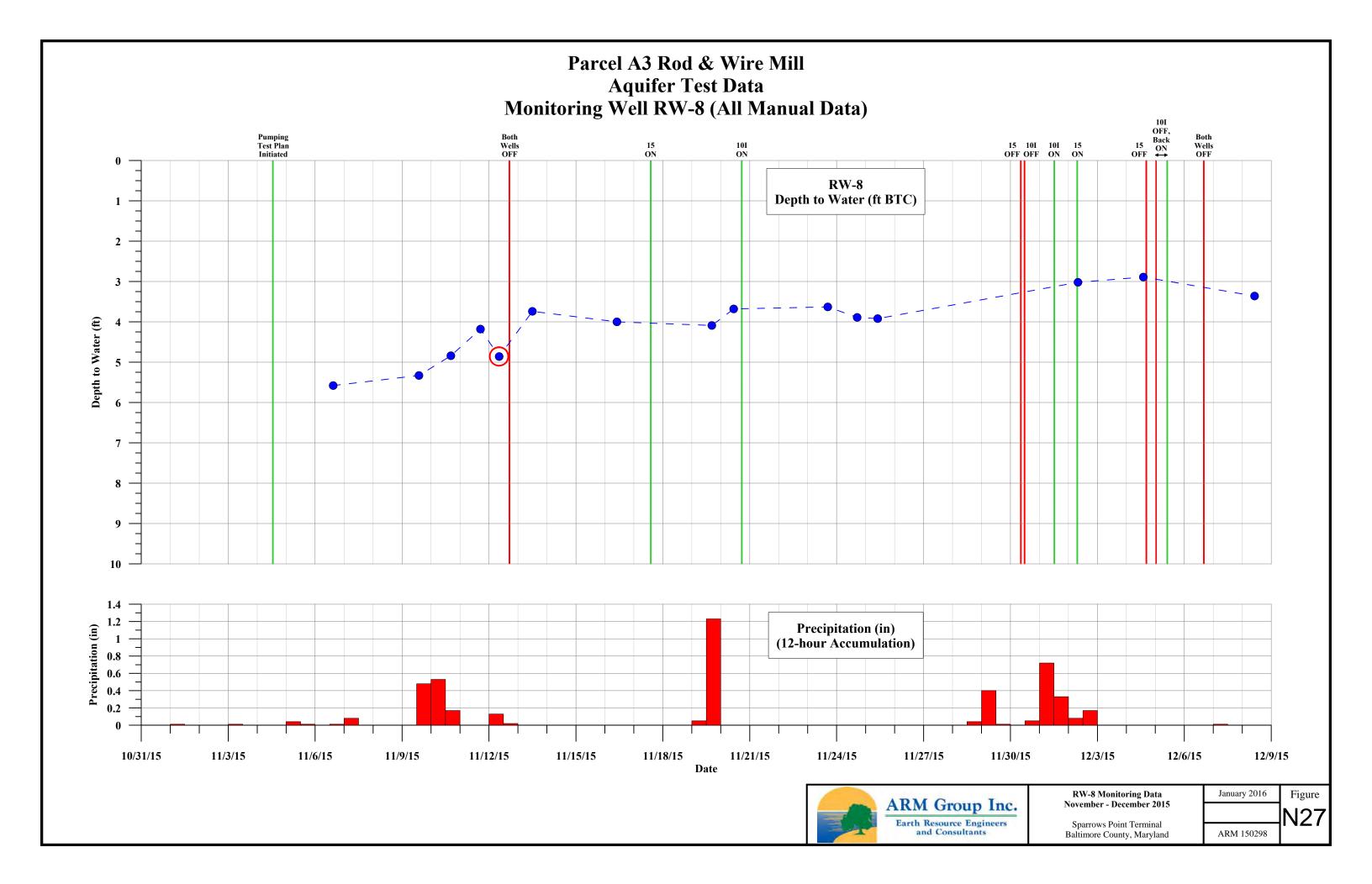


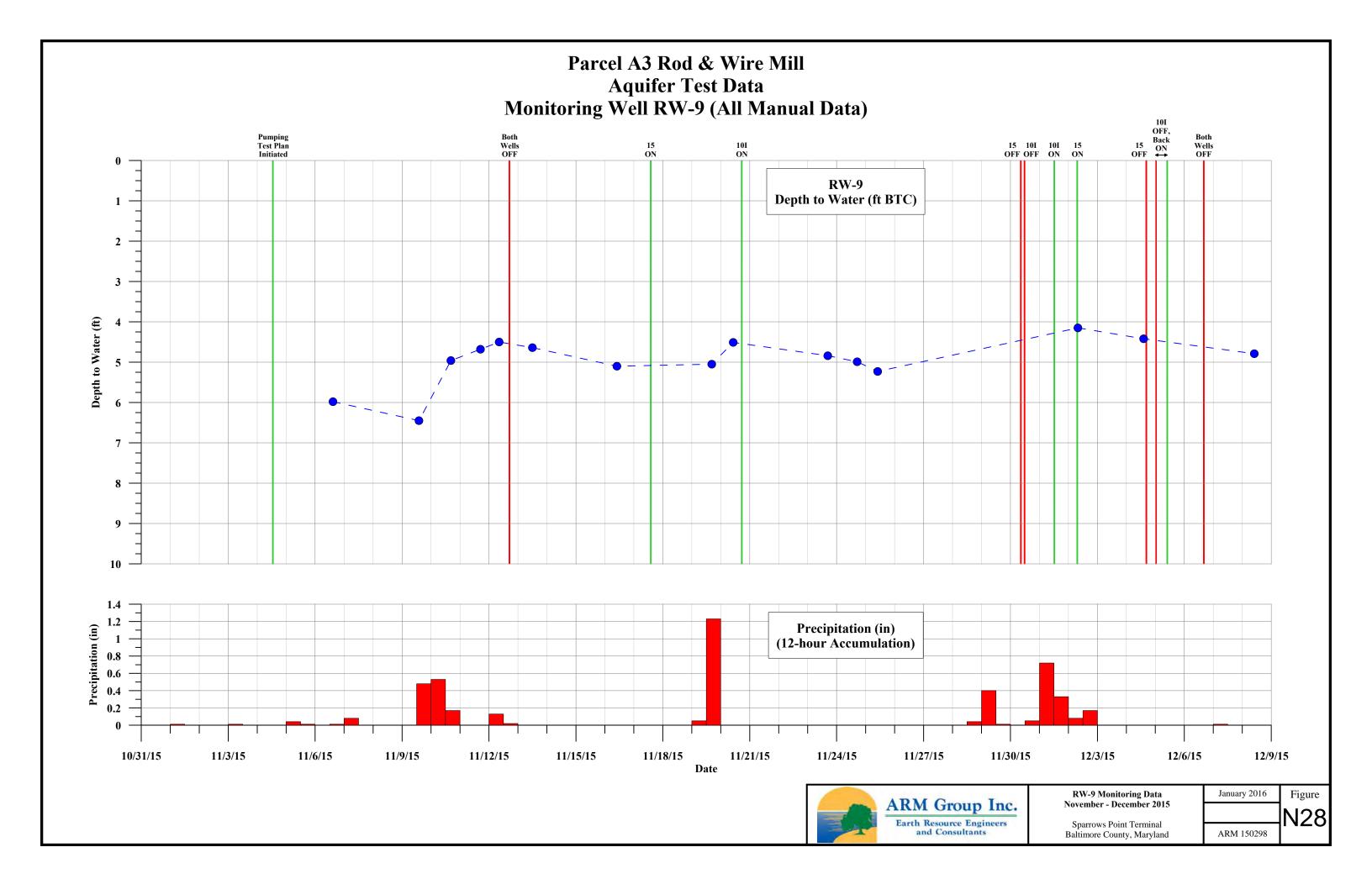


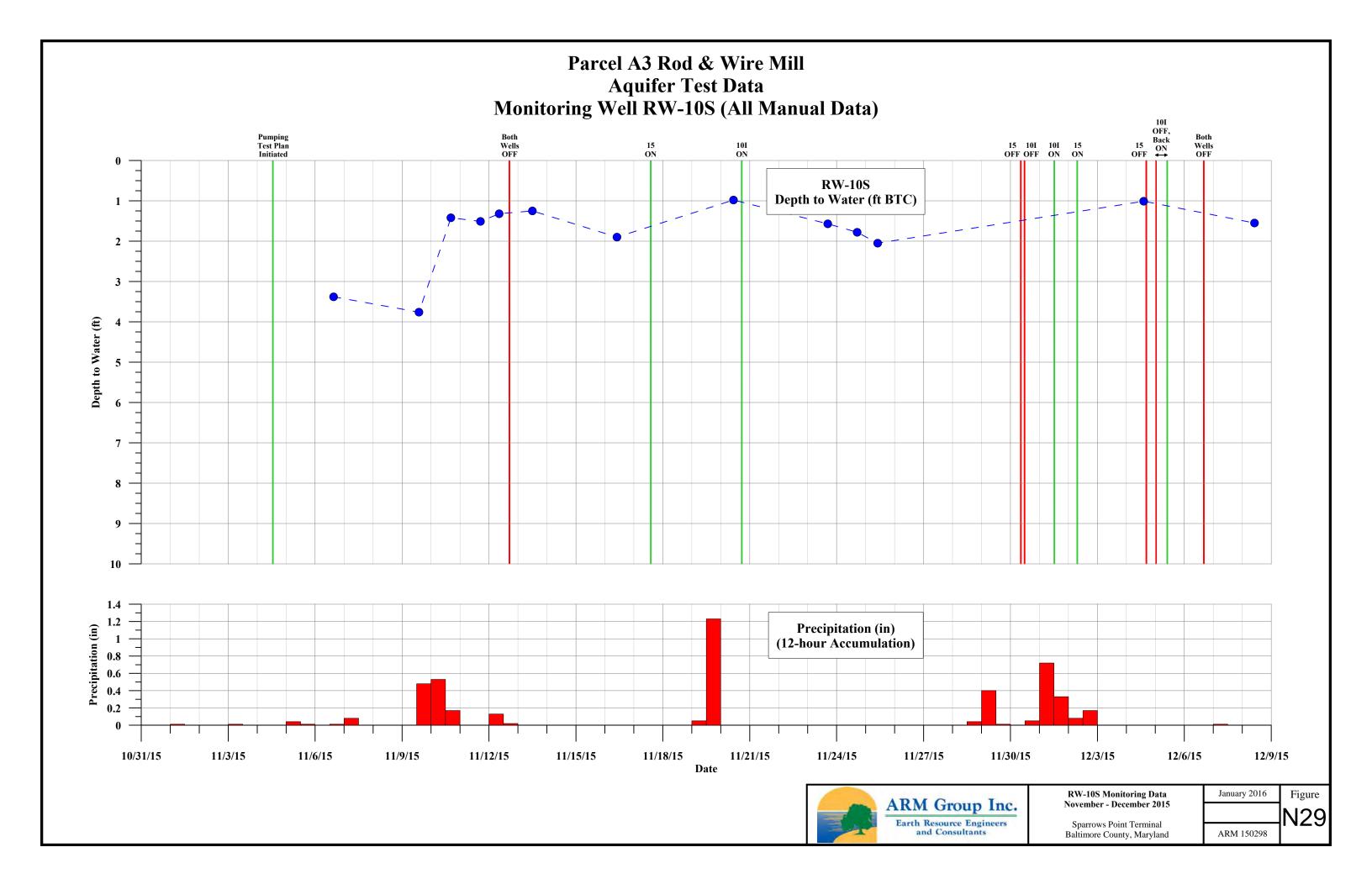


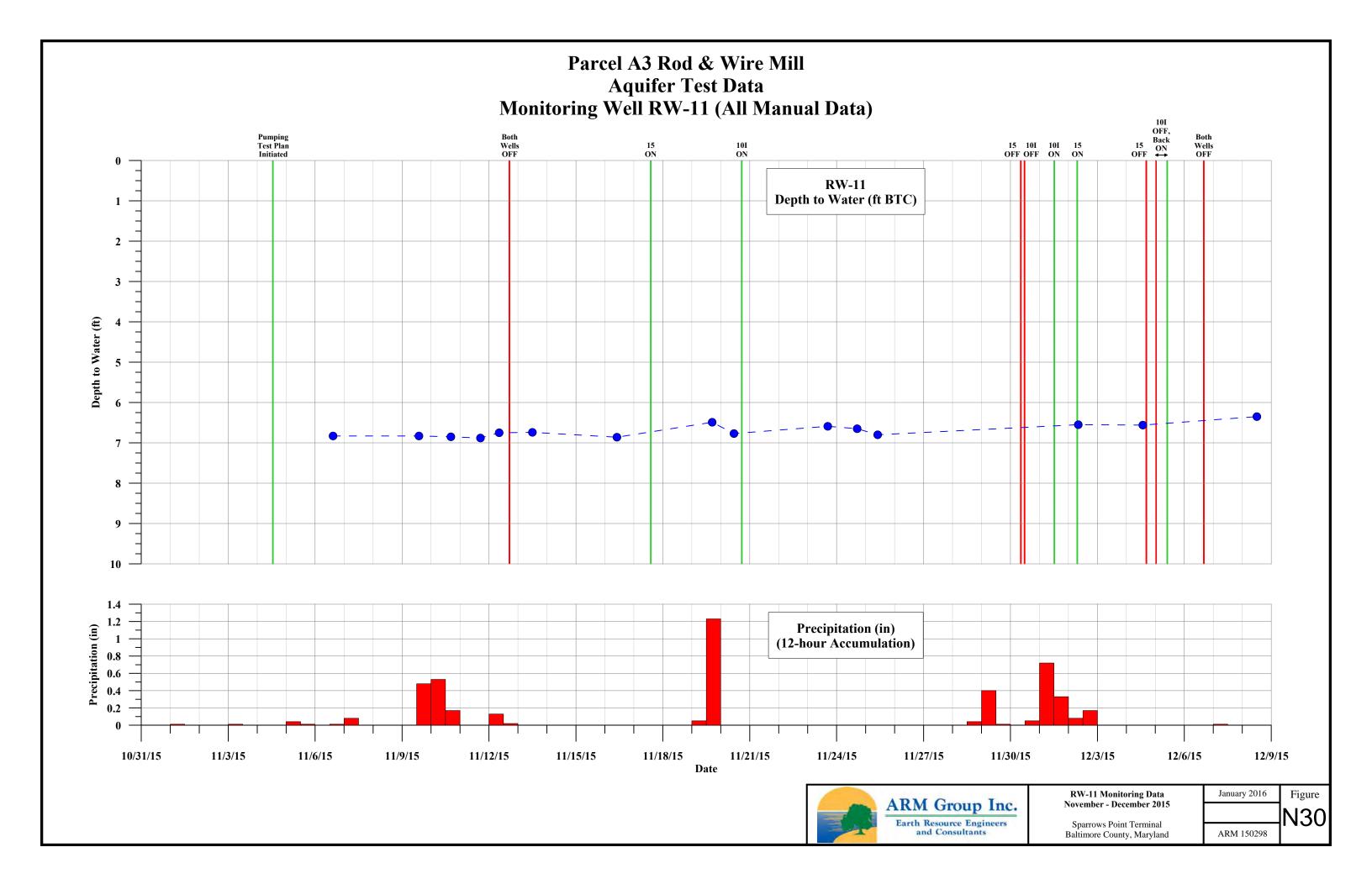


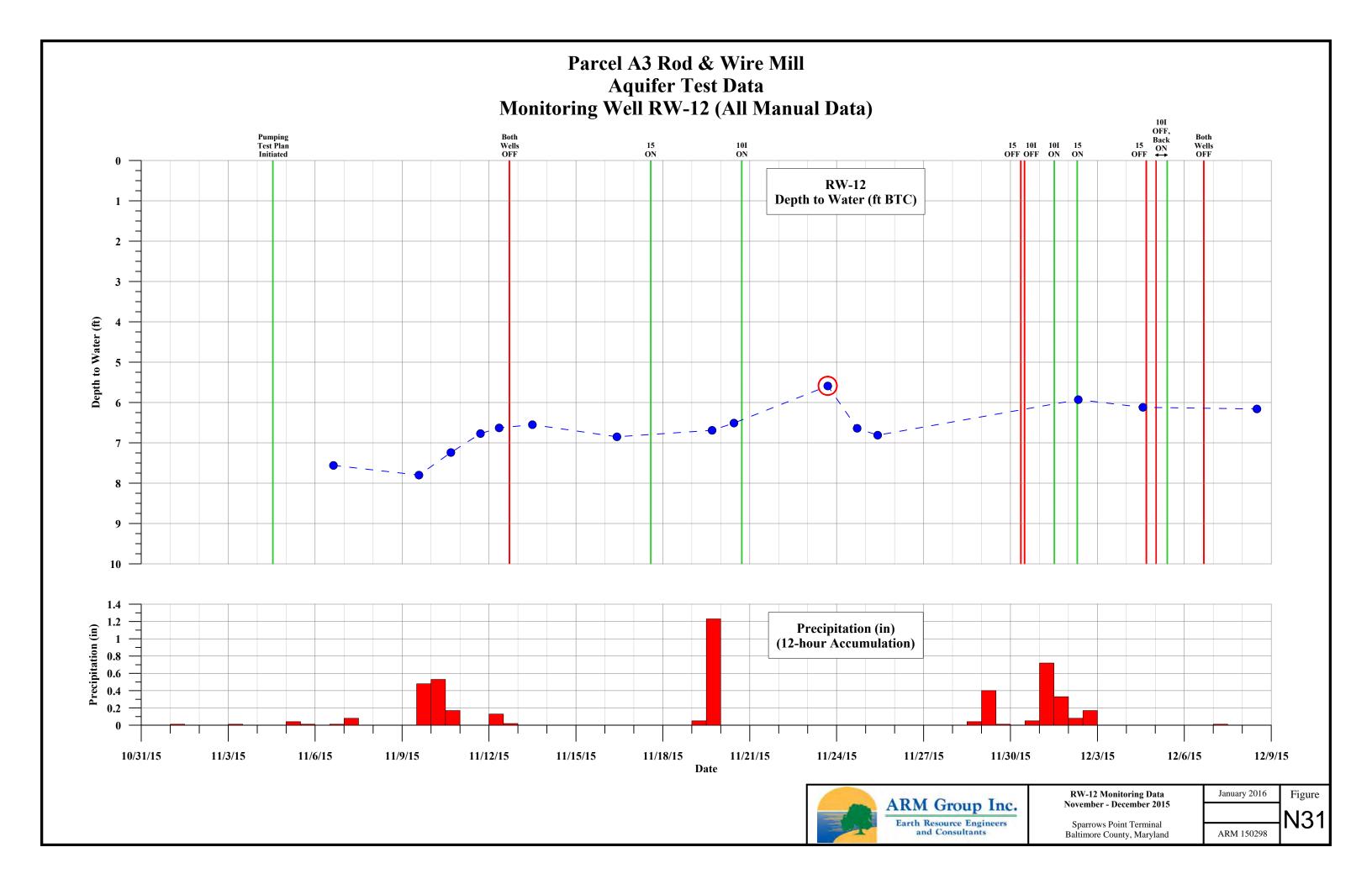


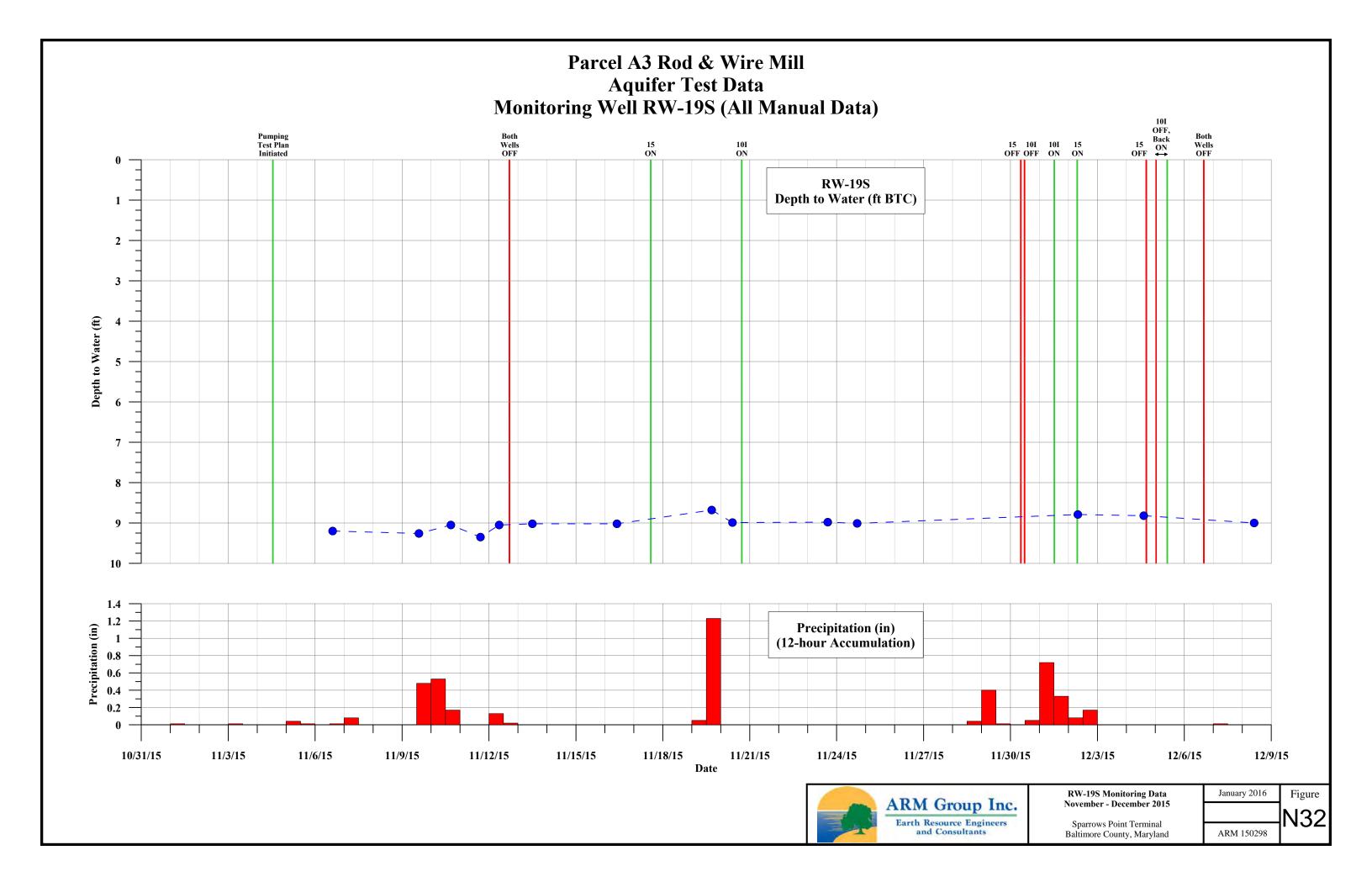


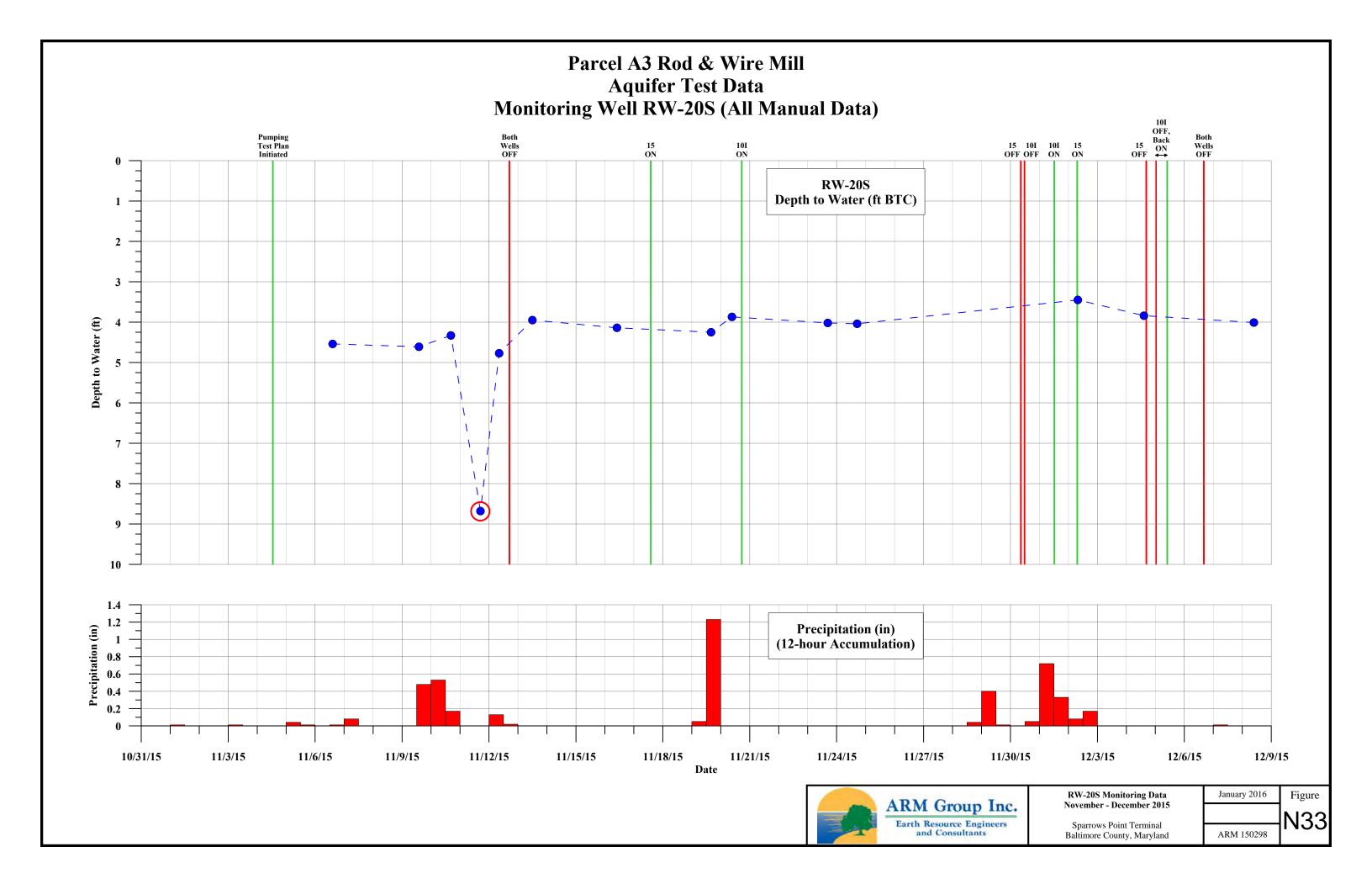


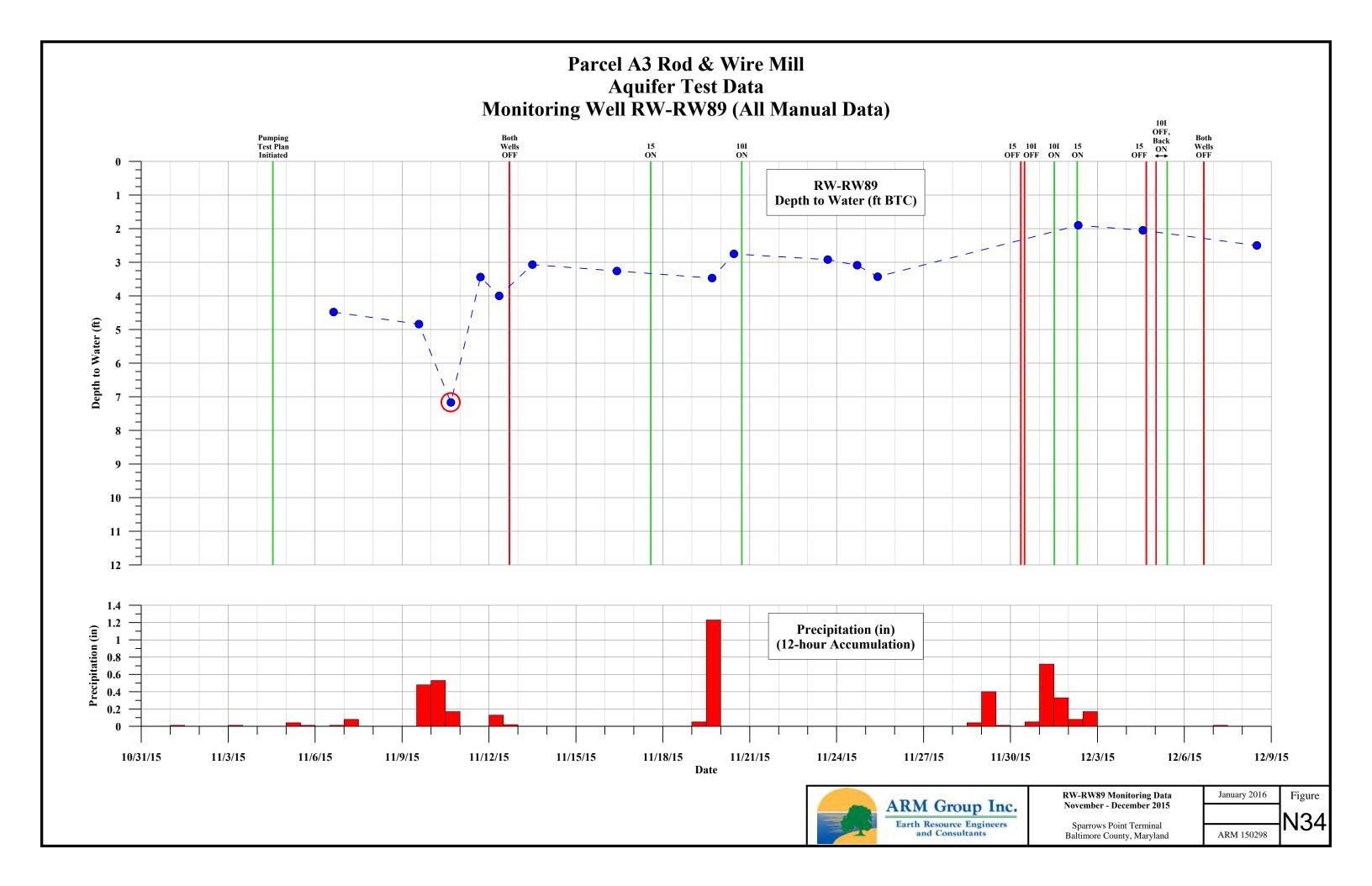


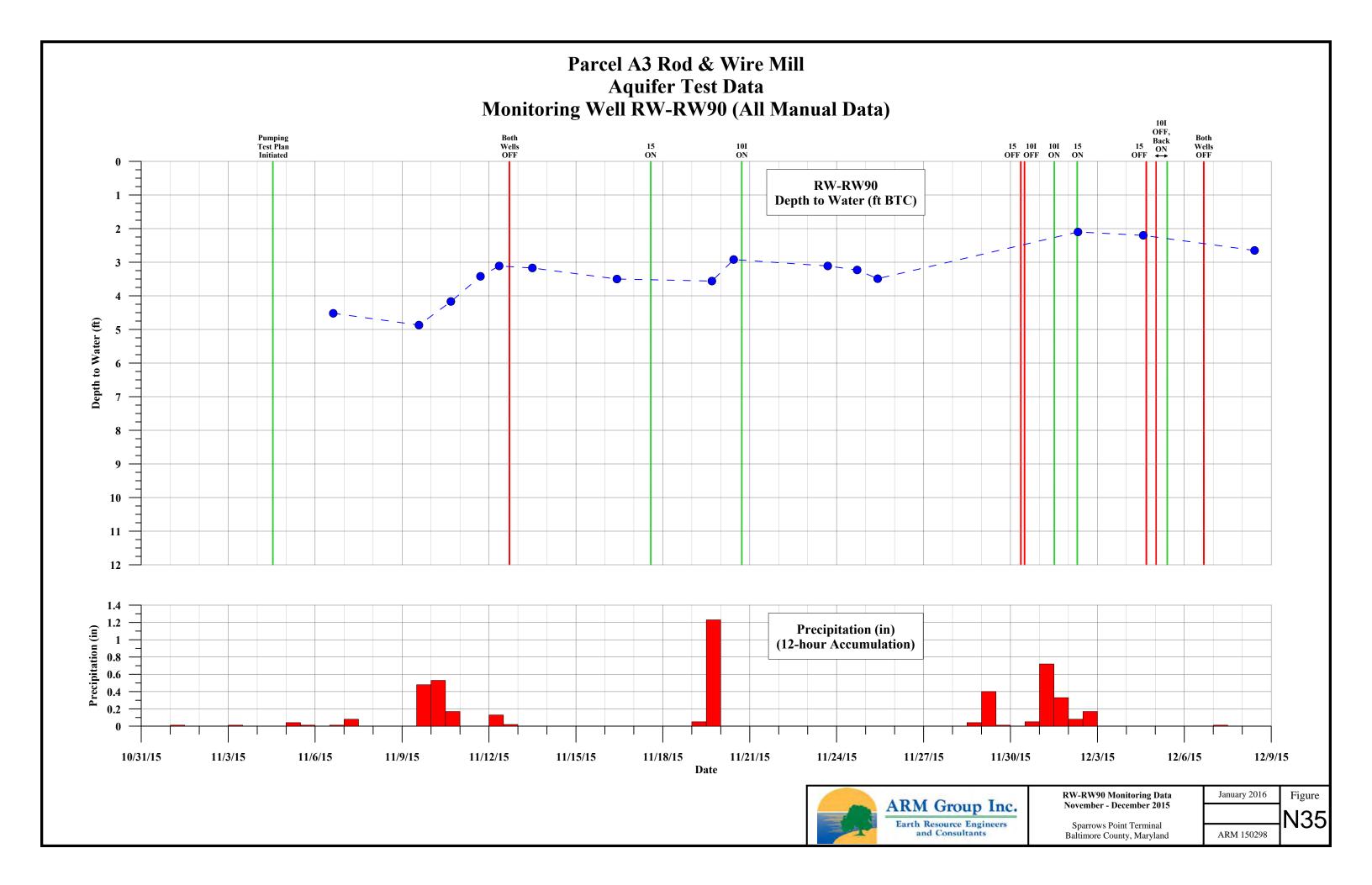


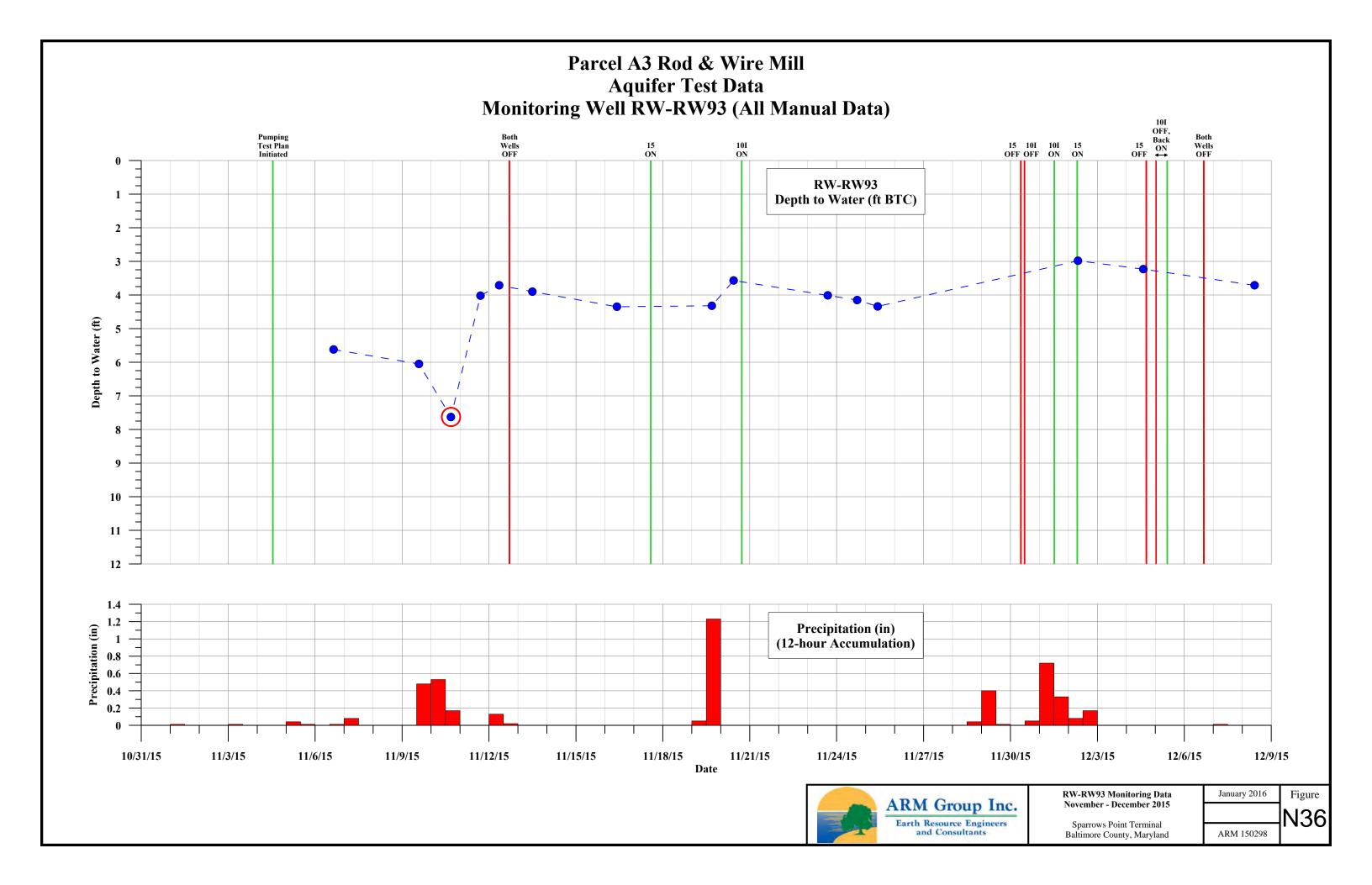


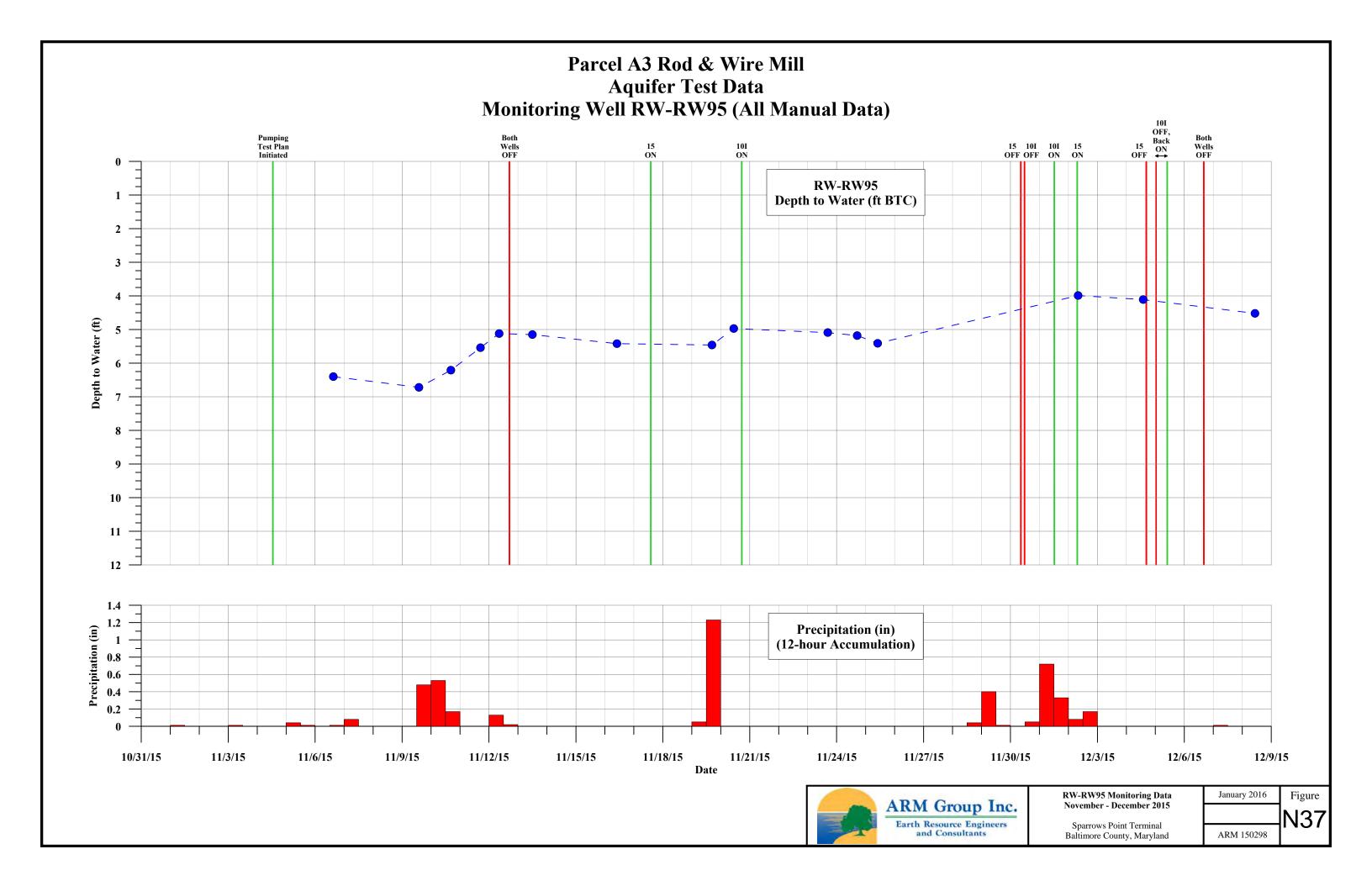


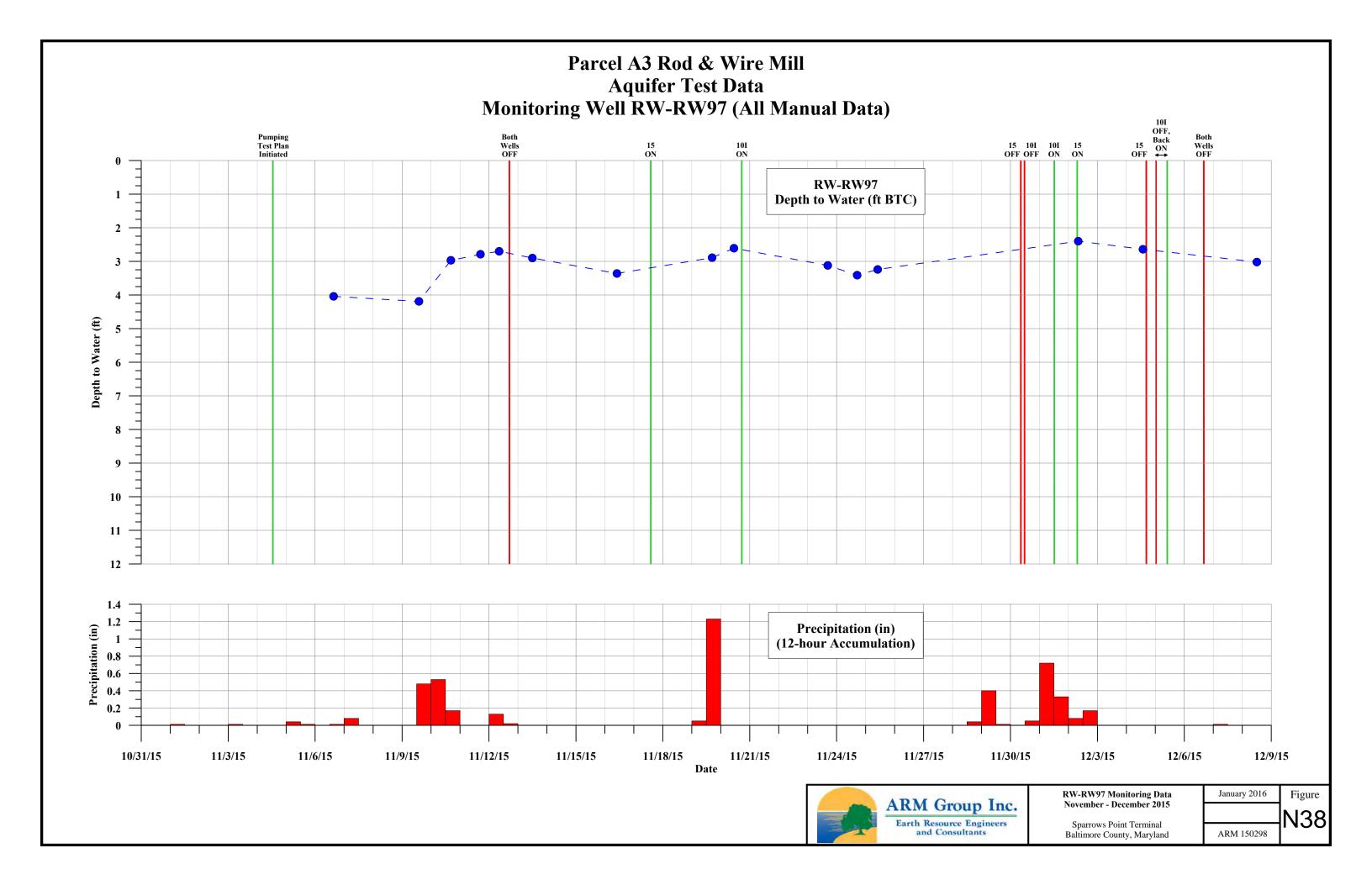


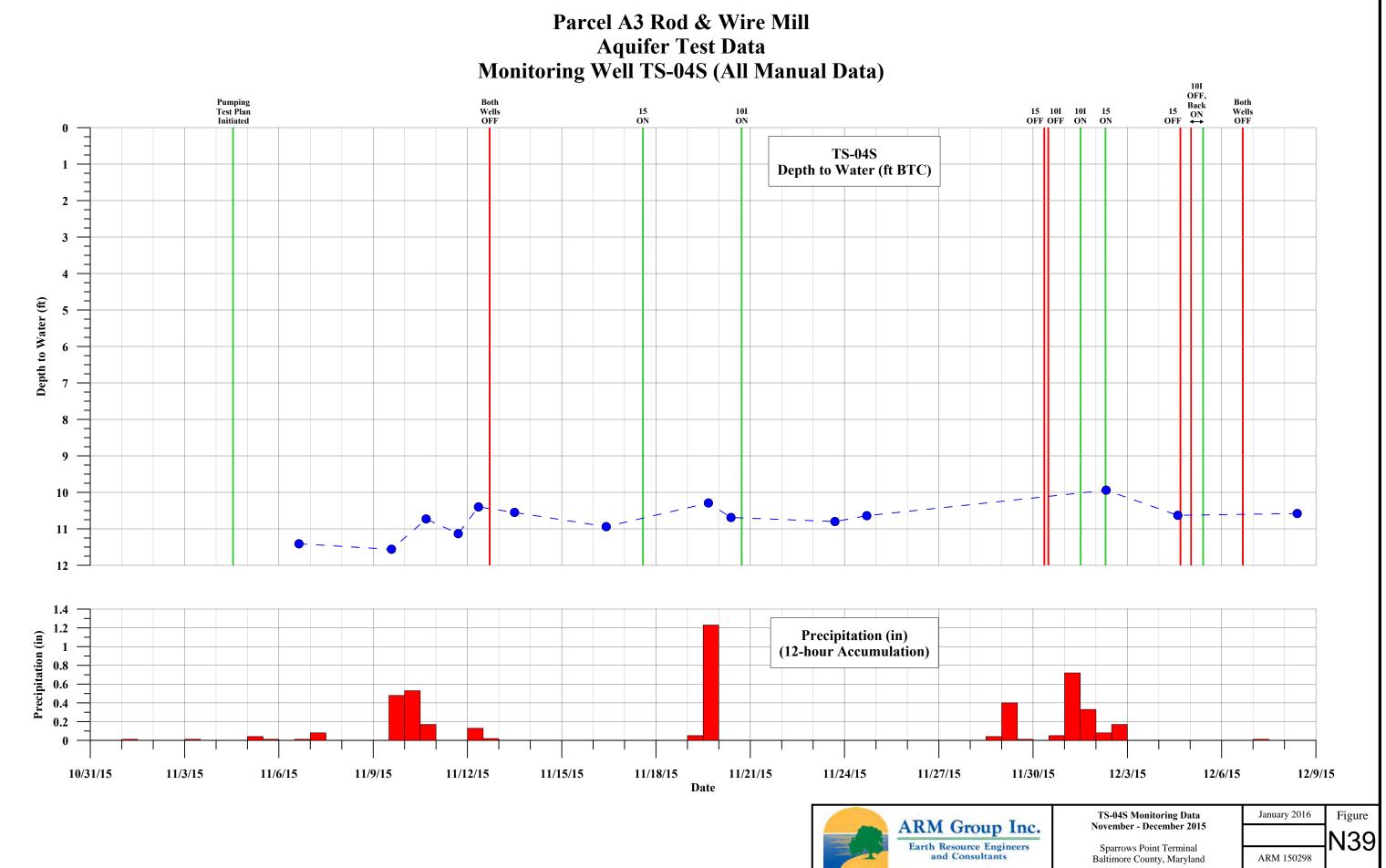


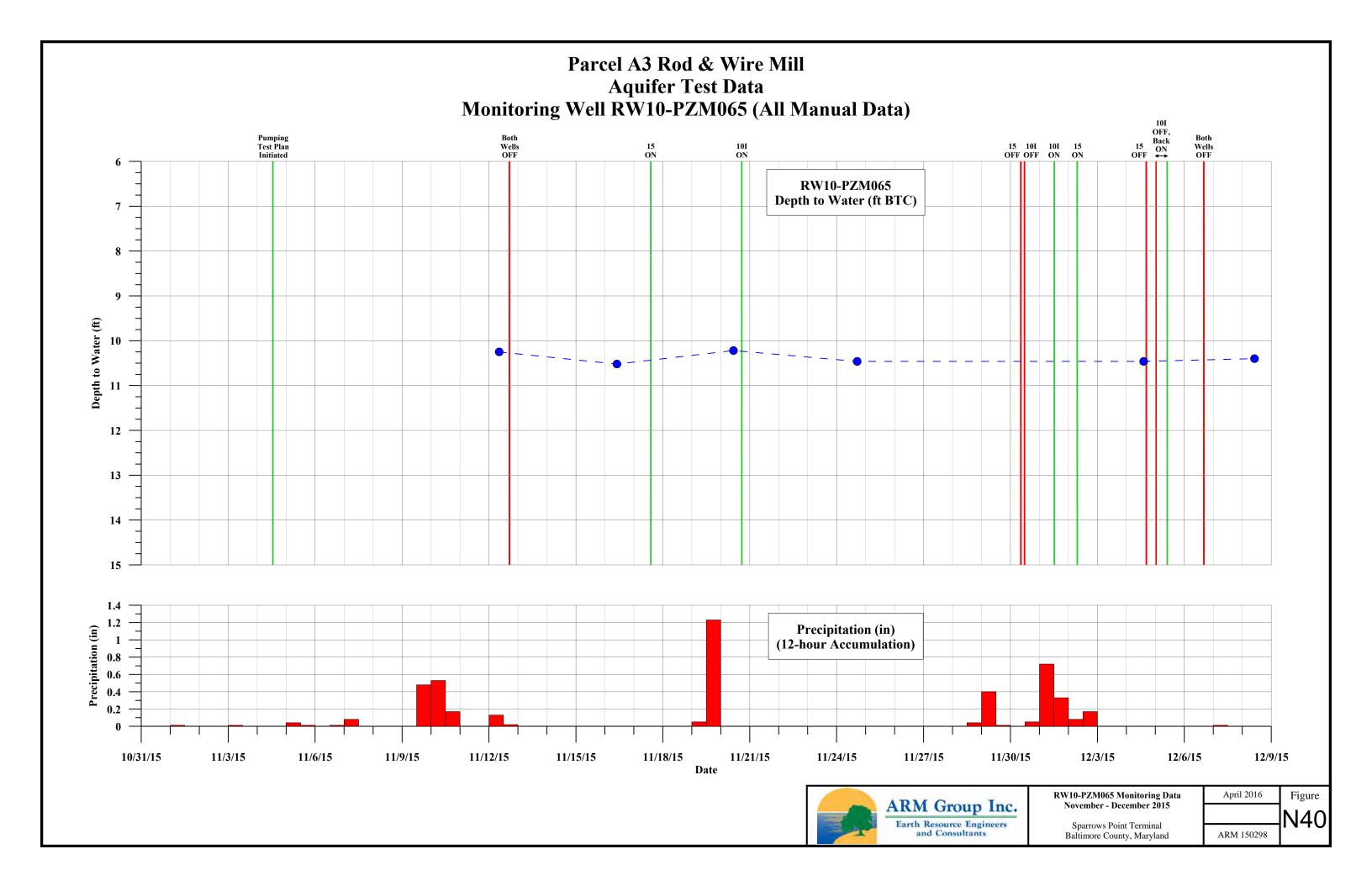


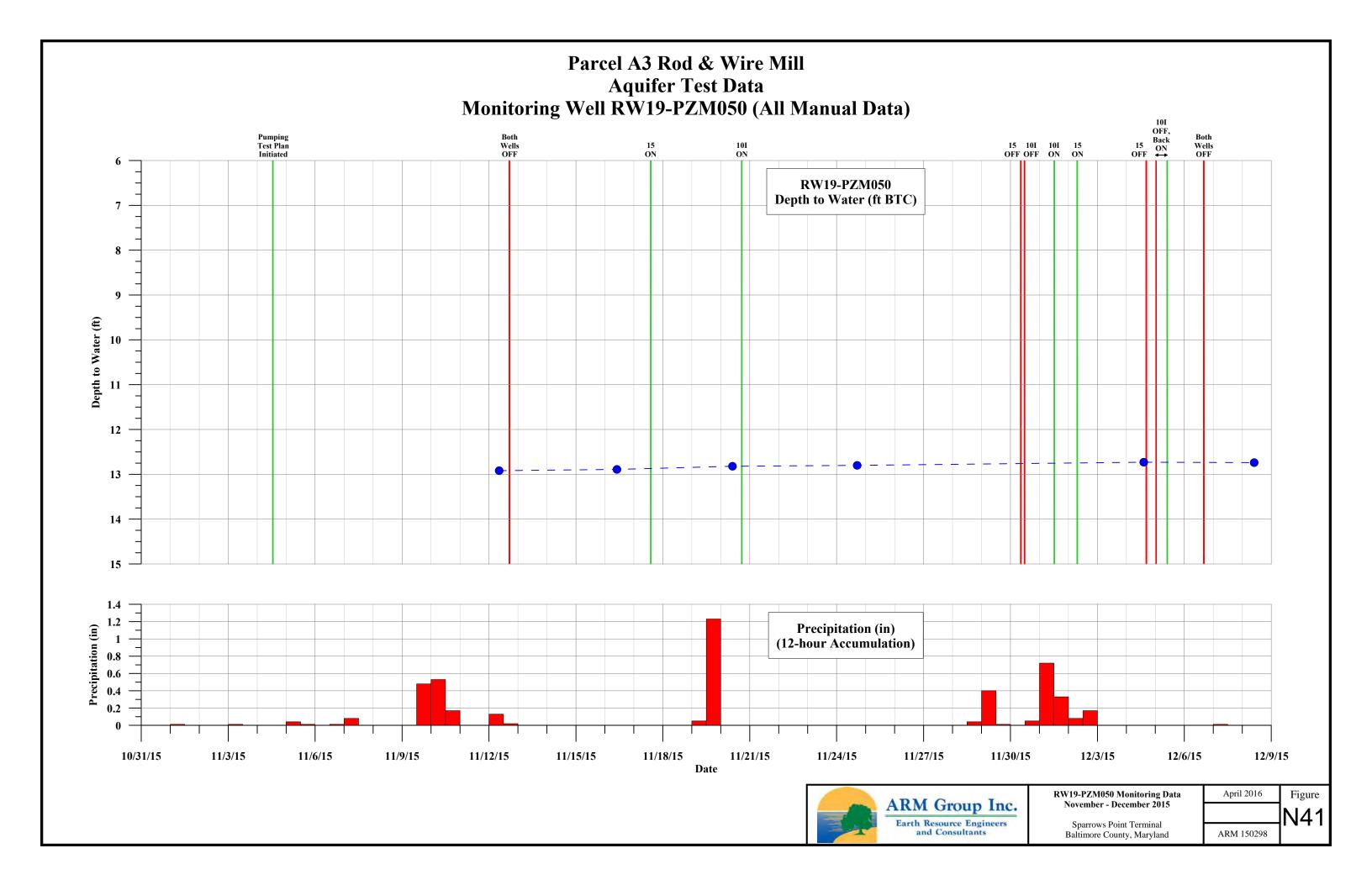


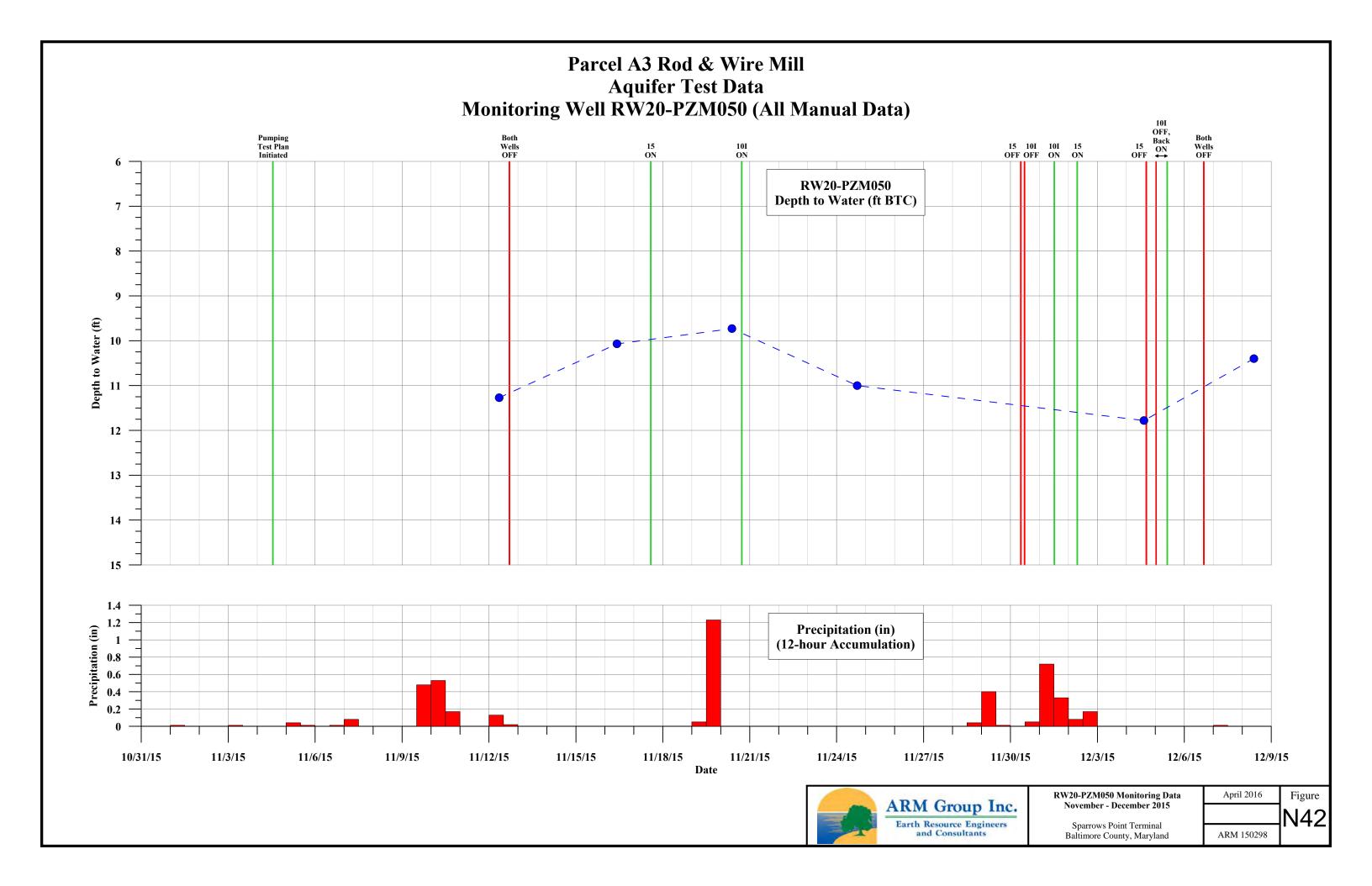












APPENDIX O

Groundwater Model Development Report

1. OBJECTIVES

The objectives of initial groundwater model are:

a) Establish a numerical groundwater flow model that incorporates:

- the surrounding surface water,
- o the shallow, intermediate, and deep aquifer system,
- the influence of the existing pumping system (RW15 and RW10), and
- prediction / control of cadmium and zinc migration, primarily in the intermediate zone (based on flow, not transport).

b) Screen and evaluate potential options for the final remedial approach, to assist in developing a 60% design of the selected remedy, and to identify additional data requirements for the final remedial design.

2. CONCEPTUAL GROUNDWATER MODEL

The subsurface geology at the site is typical of the Maryland coastal plain and consists of layered sedimentary rocks that are un-lithified to partially consolidated materials composed of clay, silt, and sand-sized grains, overlain by variably thick man-made fill materials (including slag).

Boring logs for RW 22-PZM, RW 23-PZM, RW 24-PZM, RW-GB-01, RW-GB-02, RW-GB-03, and RW-GB-04 were evaluated for layer lithologies and thicknesses, and compared with video log results (length and depth of screened intervals) from the older monitoring wells at the site. From this information the geologic framework was constructed for the groundwater model (**Figure 18**). Estimates of hydraulic conductivity for the aquifer model layers were initially obtained from the slug test data. Aquitard hydraulic conductivities were estimated from published information (Freese and Cherry, 1979).

Inspection of the pumping test hydrographs (**Appendix N**) reveal that the Shallow Aquifer and Deep Aquifer were not measurably impacted by pumping of RW10 and RW15 during the pumping test; which are screened in the Intermediate Aquifer. As such, the groundwater model included aquitards above and below the Intermediate Aquifer in the model domain. Recharge is assumed to enter the Intermediate Aquifer in areas outside of the model domain where overlying materials are more transmissive to the downward vertical movement of fluids.

3. HYDROSTRATIGRAPHIC UNITS

3.1. Shallow Aquifer

The Shallow Aquifer is an unconfined water table aquifer occurring at depths ranging from the earth surface to -2 ft elevation (msl) in the uppermost fill and alluvium in the model area. In general, the water table elevation increases from west (Patapsco River) towards the east across



the model area. The saturated thickness of the Shallow aquifer is defined as the depth from the top of the water table to the upper surface of the Layer 2 Aquitard and ranges from approximately 2 feet thick (beneath the Patapsco River) to 14 feet thick (eastern portion of the site area). The Shallow Aquifer was assigned a hydraulic conductivity of 2.5 feet / day; representative of silty sand (Freese and Cherry 1979). Evaluation of the pumping test results indicates that the Shallow Aquifer is hydraulically separated from the Intermediate Aquifer as indicated by the pumping test results (i.e., drawdown in the Intermediate Aquifer caused by the pumping of RW10 and RW15 did not impact water levels in any monitoring points that are completed in the Shallow Aquifer). In addition, fluid conductivity (specific conductance) measurements of samples taken from monitoring wells do not suggest direct hydraulic communication between the Shallow and Intermediate Aquifers (**Figure 19** and **Figure 20**).

As such, the hydraulic heads in the shallow aquifer were assigned as general head boundaries based on water level elevations that were recorded during the pumping test.

3.2. Layer 2 & 3 Aquitards

Information from the boring logs, pumping test results, and previous studies indicated the presence of one or more aquitards between the Shallow Aquifer and the Intermediate Aquifer. In particular, the lack of drawdown or recovery in the Shallow Aquifer associated with pump ON / OFF events during the aquifer pumping test supports the presence of aquitard(s) between the Shallow and Intermediate Aquifers. As such, two aquitards were included in the Groundwater Model; Layer 2 configured as a constant one-foot in thickness and hydraulic conductivity of 1e-5 feet per day (represents a clay material), and Layer 3 with variable thickness between Layer 2 and the top of Layer 4, and hydraulic conductivity of 1e-5 feet per day (represents a clay material). The hydraulic conductivities of Layers 2 & 3 were not changed during the modeling process.

3.3. Intermediate Aquifer (Primary Modeled Aquifer)

The Intermediate Aquifer is a confined aquifer occurring at depths ranging from approximately -5 feet to -25 ft elevation (msl) in the model area. In general, the elevation of the hydraulic head in the Intermediate Aquifer increases from west (Patapsco River) towards the east across the model area.

The saturated thickness of the Intermediate Aquifer is defined as the depth from the base of the Layer 3 Aquitard to the upper surface of the Layer 5 Aquitard, and ranges from approximately 5 feet thick (north, south, east, and west sides of the model domain) to 22 feet thick (central portion of the model domain). The Intermediate Aquifer was assigned a range of hydraulic conductivities from approximately 4 feet / day to 10,000 feet / day representative of clean sand to gravel.

Pumping wells RW10 and RW15 are completed in the Intermediate Aquifer. Drawdowns during the pumping test were only experienced in the monitoring wells completed in the Intermediate Aquifer.



3.4. Layer 5 Aquitard

Information from the boring logs, pumping test results, and previous studies indicated the presence of one or more aquitards between the Intermediate Aquifer and the Deep Aquifer. For the purposes of this report, a single aquitard was included between Layer 4 and Layer 6 with a variable thickness and hydraulic conductivity of 1e-3 feet per day (represents a silty material). The hydraulic conductivity of Layer 5 was not changed during the modeling process.

3.5. Deep Aquifer

The Deep Aquifer is a confined aquifer occurring at depths ranging from approximately -37 feet to -70 feet elevation (msl) in the model area, and was encountered during the installation of the four deep monitoring wells (RW10-PZM065, RW18-PZM047, RW19-PZM050 and RW20-ZM050). The depth of the Deep Aquifer increases from west to east across the model domain.

The saturated thickness of the Deep Aquifer is defined with a constant thickness of 5 feet across the model domain. The Deep Aquifer was assigned a hydraulic conductivity 0.2 feet / day; which is representative of silt to silty sand.

There is no indication that the deep aquifer was impacted by the pumping of RW10 and RW15 (screened in the Intermediate Aquifer) during the pumping test. As such, the hydraulic conductivity of the aquitard that separates the Deep Aquifer from the Intermediate Aquifer was adjusted to eliminate modeled impacts associated with RW10 and RW15 pumping.

3.6. Model Uncertainty

General-head Boundaries and Input Model Water Levels

The uncertainty in the elevation of the general-head boundaries along the north and southeast margins of the Intermediate Aquifer (Layer 4) is relatively low. The elevations of these general-head boundaries were set by extrapolating groundwater elevations from the nearby monitoring wells to the boundaries. The elevation of Layer 1 (Shallow Aquifer / Patapsco River) and the water levels within the Intermediate Aquifer are also relatively certain because of the measured elevations in these features.

3.7. Hydraulic Conductivities

The uncertainty in the hydraulic conductivities in the model is moderate to low. The slug test and pumping test data provided a significant number of hydraulic conductivity measurements that corresponded with visual inspection of split-spoon lithologic samples collected from the borings. The lack of influence on the shallow and deep aquifers during the Intermediate Aquifer (RW10 and RW15) pumping tests supports the presence of aquitards between these layers. The estimated hydraulic conductivities used for this investigation are based upon steady-state modeling and represent approximate conditions in the aquifer. This is an appropriate first step prior to groundwater modeling that involves transient conditions with storage coefficients, recharge, leakance, and other factors used to estimate transport of contaminants.



4. CALIBRATION PROCEDURE

Groundwater modeling was only conducted on the Intermediate Aquifer for this task. The intermediate groundwater flow model was calibrated to the groundwater elevations associated with the pumping test data collected in November and December 2015 (Figure 21). The groundwater flow model was calibrated by specifying initial estimates of general head boundary conditions and hydraulic conductivity within the Intermediate Aquifer, and solving the model for steady-state flow conditions. These estimated input parameters were then varied in successive simulations until the steady state head solution most closely matched the pumping test calibration target water levels and the general geometry of the contoured pumping test measurements. Calibration statistics are shown in Figure 22.

5. SENSITIVITY OF MODEL TO INPUT PARAMETERS

The sensitivity of the calibrated model to variations in hydraulic conductivity is show in **Figure 23**. Hydraulic conductivity zones coupled with general head boundaries are the primary variables used in this steady state model. The general head boundaries are relatively straightforward to specify in this model; however, the distribution of hydraulic conductivity is only partially known from the slug test data and an understanding of the local hydrogeology. The hydraulic conductivity zone values used in the calibrated model are represented by the Calibrated Zone Multiplier of "1" on the X axis in **Figure 23**. Note that the sum of squares residual model values increase rapidly in conductivity zones 2 through 5 when the model input hydraulic conductivity parameter is increased or decreased from the calibrated model values. The Zone 1 value is sensitive to decreases in hydraulic conductivity but not as sensitive to increases in hydraulic conductivity.

6. TIDAL INFLUENCE

Monitoring data obtained from several wells during the aquifer testing show evidence of a potential tidal influence via low-amplitude cyclic patterns that appear to be superimposed on the hydrographs in the intermediate flow regime.

Tides are a manifestation of the gravitational forces of the sun and moon acting on the earth, and are most easily recognized as the upward and downward motion of the water in the oceans. As an incoming tide rises, the force exerted by the increased volume of offshore water compresses the materials overlying adjacent coastal aquifers, causing a rise in the water levels in any wells screened in such an aquifer. The water levels fall when the tide recedes, causing a sinusoidal wave signature in time-series water level data that mimics the offshore tidal pattern, with a time lag and decreased amplitude. This effect can be observed in the hydrographs of several Parcel A3 wells, shown in **Appendix N**.

Tidal signatures may be filtered from water level data, resulting in an approximation of the water levels as they would have occurred without a tidal influence. In order to apply such a filter, the tidal data must also be measured throughout the monitoring period. The National Oceanic and



Atmospheric Administration (NOAA) maintains a tidal monitoring station at Fort McHenry, Baltimore, MD (Station #8574680) which is 5 miles upstream of Sparrows Point on the Patapsco River. Data is publicly available from this station at 6-minute intervals.

A tidal filter requires two data sets, the water levels in the well of interest and the tidal measurements (NOAA station data), that have been time-synchronized and aligned to the same elevation datum. The filtered water level data can be calculated using the following equation (Smith, 1994):

 $hF(t) = h(t) - E[T(t - t_{lag}) - \overline{T}],$

where:

hF(t) = filtered water level at time t

h(t) = observed water level at time t

E = tidal efficiency of the aquifer surrounding the well

 t_{lag} = time lag coefficient

T(t) = observed tidal level at time t

 \overline{T} = mean tidal elevation over the entire monitoring period

The time lag coefficient is estimated by averaging the time difference between several tidal peaks and the corresponding well level peaks. The tidal efficiency reflects the degree to which the materials overlying the aquifer resist the pressure changes induced by tidal oscillation. Factors influencing the tidal efficiency of an aquifer include its transmissivity and storage, the frequency of tidal oscillations, and the monitoring well's distance from the shoreline.

The water level data from RW01-PZM020 was filtered as an example of the results of this method. A time lag of 1.7 hours was calculated by averaging the delay between the peaks observed from November 25-29, 2015; which was a period of relative groundwater level stability without precipitation. A tidal efficiency of approximately 0.18 was estimated by minimizing the sum of the squared residuals relative to the mean of the filtered data from four complete tidal cycles from November 26-28, 2015. This method was chosen in order to arrive at the tidal efficiency that provided the greatest degree of tidal waveform suppression across this time range, during which water levels remained relatively constant, tidal oscillations notwithstanding. As provided in **Appendix N**, **Figure N19** and **Figure N20** show the original and filtered hydrographs for RW01-PZM020, respectively.

Tidal fluctuations appear to influence the groundwater levels in the intermediate zone at Parcel A3. Monitoring data from RW23-PZM (**Appendix N**, **Figure N17**; completed in the shallow zone) shows evidence of tidal influence on the water level changes in the shallow flow regime, albeit to a lesser magnitude. Water levels in RW01-PZM020 appear to fluctuate by as much as



3-4 inches per tidal cycle. However, Smith (1994) noted that tidal influences did not influence the direction of groundwater flow, especially in the areas closest to large surface water bodies.

For this report (including the steady state groundwater modeling), representative average groundwater level measurements for pump-on and pump-off conditions were taken from hydrographs that included tidal influence. Future modeling efforts involving transient flow and transport modeling may include tidal effects as part of the boundary conditions, as the cyclic movement of groundwater may impact the distribution of modeled transport parameters in the aquifer.

7. REFERENCES

Freese and Cherry, 1979, *Groundwater*, Prentice-Hall, Inc., Englewood Cliffs, New Jersey, 604 p

Smith, T.E., 1994, Analysis of Tidal Fluctuation Effects on a Confined and Unconfined Aquifer, *Proceedings of the FOCUS Conference on Eastern Regional Groundwater Issues*, October 3-5, 1994, Burlington, VT, p. 757-771.



APPENDIX P

Space Reserved for PeroxyChem Report (Batch Testing of Bulk Soil Samples)