



**Engineers and Scientists** 

December 10, 2019

Ms. Barbara Brown Project Coordinator Maryland Department of the Environment 1800 Washington Boulevard Baltimore, MD 21230

> Re: Pre-Design Investigation Work Plan (Revision 1) Parcel B14: Humphrey Impoundment Tradepoint Atlantic Sparrows Point, MD 21219

Dear Ms. Brown:

ARM Group Inc. (ARM), on behalf of EnviroAnalytics Group (EAG), has prepared this Pre-Design Investigation (PDI) Work Plan for a portion of the Tradepoint Atlantic property (formerly Sparrows Point Terminal, LLC) that has been designated as Area B: Parcel B14 (the Site). Parcel B14 is comprised of 60.3 acres of the approximately 3,100-acre former steel making facility (**Figure 1**). The majority of Parcel B14 is occupied by the Humphrey Impoundment, which is approximately 43 acres in size. The Site is bounded to the west by the Humphrey Creek Waste Water Treatment Plant (HCWWTP) and Emergency Detention Basin (within Parcel B24), to the north by the Billet Building (within Parcel B8) and the New Cold Mill Complex (NCMC; within Parcel A4), and to the east and south by the Tin Mill Canal (TMC; within Parcel B16). The proposed activities presented in this PDI Work Plan are based on the findings and recommendations from the Phase II Investigation Report for Area B: Parcel B14 (Revision 0 dated March 27, 2018) and communications with the Maryland Department of the Environment (MDE) during a project meeting on June 5, 2018 regarding the conceptual response action plan for Parcel B14.

#### **1.0 BACKGROUND**

During the Phase II Investigation, 33 soil borings were initially completed across Parcel B14 to provide for the characterization of the materials that had been placed within Humphrey Impoundment during its operation. Several of these soil boring locations exhibited elevated detections of TPH/Oil & Grease and/or had physical evidence of non-aqueous phase liquid (NAPL) in the associated soil cores. Temporary screening piezometers were installed at 14 of these locations (i.e., B14-002-SB, B14-006-SB, B14-007-SB, B14-008-SB, B14-010-SB, B14- 011-SB, B14-012-SB, B14-013-SB, B14-015-SB, B14-017-SB, B14-021-SB, B14-022-SB, B14- 028-SB, and B14-034-SB) to help delineate the extent and thickness of NAPLs within the

impoundment. Due to the detection of NAPLs within many of these piezometers, nine additional temporary screening piezometers (B14-035-PZ through B14-043-PZ) were subsequently installed at strategic locations to further characterize the extent and thickness of NAPLs across the impoundment. Another four temporary piezometers (B14-044-PZ through B14-047-PZ) were installed immediately to the west of the Parcel B14 boundary. Despite the presence of measurable NAPL in a number of the temporary piezometers, NAPL was not detected in any of the permanent monitoring wells surrounding the impoundment, suggesting that the NAPL is contained within the impoundment. The locations of all piezometers and permanent wells are shown on **Figure 2**. Combined soil borings and piezometer construction logs for borings installed during the Phase II Investigation, including the nine additional piezometers installed due to observations of NAPL, are included in **Appendix A**.

Each screening piezometer was gauged for the presence or absence of NAPL with an oil-water interface probe immediately, 48-hours, and 30-days (or more) after installation. Several of the screening piezometers have since been gauged periodically, depending on accessibility, to monitor the accumulation of NAPL within the piezometer casing. The results of the periodic NAPL gauging events are summarized in **Appendix B**, with the maximum accumulated NAPL thickness in each piezometer summarized in **Appendix C**. During the most recent gauging event completed on November 26 and November 27, 2019, several piezometers could not be located due to dense vegetation or were noted to have been destroyed.

The screening-level risk assessment (SLRA) included in the Phase II Investigation Report for Parcel B14 did not indicate any unacceptable risks for future Composite Workers. However, because the current surface elevation of the impoundment is depressed below the perimeter embankment, any future redevelopment of the parcel is anticipated to include the placement of fill across the surface of the impoundment to promote surface water runoff and reduce infiltration.

# **2.0 PRE-DESIGN INVESTIGATION**

# **2.1 Purpose and Scope**

Due to potential concerns associated with the planned fill placement activities, which include embankment stability, potential NAPL migration, and future constructability, supplemental PDI activities are warranted to support the completion of final design details. The planned PDI activities are discussed in the following subsections of this Work Plan and are summarized in **Table 1**.

# **2.2 Geotechnical Soil Boring Investigation**

A supplemental geotechnical soil boring investigation will be completed to support the characterization of surface and subsurface conditions, and to facilitate the collection of samples for laboratory testing. The soil boring investigation will be performed by a drill rig that is suitable for the site conditions and proposed work. This includes the ability to drive split-spoon samples for Standard Penetration Testing (SPT) in accordance with ASTM D1586, reach the targeted





depths of 25 to 30 feet, and create a borehole of large enough diameter to support in-field permeability testing. The assessments to be completed as part of the supplemental investigation are discussed in the following subsections.

### *2.2.1 Geotechnical Assessment of Embankment*

Soil borings will be completed at selected locations along the embankment of the impoundment to support the evaluation of its construction and stability. The boring locations, consisting of borings B14-001-PDI, B14-005-PDI, B14-007-PDI, B14-008-PDI, B14-009-PDI, B14-010-PDI, and B14- 011-PDI, are shown on **Figure 3**. These locations were selected to assess portions of the embankment that have not previously been investigated under a geotechnical investigation performed along the eastern side of the embankment by Hillis Carnes Engineering Associates (HCEA). The locations of the geotechnical borings completed by HCEA are shown on **Figure 3**, with boring logs included in **Appendix D**. The proposed supplemental locations were also selected to assess portions of the embankment where NAPL migration to adjacent areas is a potential concern. These borings will extend to a depth of approximately 25 to 30 feet below the existing grade with the intention of extending through the embankment materials and at least five feet into the underling native materials. Continuous split-spoon sampling with SPT testing will be conducted from the ground surface to a depth of 15 feet, and then one more split-spoon and SPT test for every five feet thereafter.

During drilling, soils and subsurface lithologies will be logged by the attending scientist or engineer with respect to material type, color, particle size, odors, and any other relevant properties. Representative materials from each boring between a depth of approximately 5 to 15 feet below grade will be collected and subsequently submitted to a geotechnical testing laboratory for sieve analysis (ASTM D422) and Atterberg limits (ASTM D4318).

### *2.2.2 Geotechnical Assessment of Sediments/Sludges*

Concurrent with the embankment soil boring investigation, additional soil borings will be completed within the interior of the impoundment to characterize the physical properties of the impoundment sediments and sludges. Boring locations are shown on **Figure 3** and consist of borings B14-002-PDI, B14-003-PDI, B14-004-PDI, and B14-006-PDI. These locations were selected to characterize the subsurface materials where NAPL was measured and to evaluate the potential for fluid (i.e., water and NAPL) migration. The selection of these locations was also limited by anticipated accessibility for a drill rig within the interior of the impoundment. These borings will be extended to a depth of approximately 15 to 20 feet below the existing grade, with continuous split-spoon sampling and SPT testing conducted from the ground surface to a depth of 15 feet, and then one more split-spoon and SPT test for every five feet thereafter.

During the drilling, soils and subsurface lithologies will be logged by the attending scientist or engineer with respect to material type, color, particle size, odors, and any other relevant properties. Representative materials from each boring between a depth of approximately 5 to 15 feet below



grade will be collected and subsequently submitted to a geotechnical testing laboratory for sieve analysis (ASTM D422) and Atterberg limits (ASTM D4318).

### *2.2.3 Field Permeability Testing*

To further support the evaluation of potential NAPL migration and recoverability, field permeability testing will be conducted at selected locations to help characterize the permeability of the impounded materials. Permeability testing will be conducted at or adjacent to the geotechnical boring locations designated as B14-002-PDI, B14-003-PDI, and B14-006-PDI (**Figure 3**). At each of the permeability test locations, a 2-inch diameter temporary PVC well will be installed such that the bottom of the well will have 10 to 15 feet of slotted well screen, with solid riser pipe up to the ground surface. The total depth of each well will be approximately 15 to 20 feet, with a goal of having 5 to 10 feet of screened interval below the static water level, and 3 to 5 feet of screened interval above the water table. A sand pack will be placed in the annular space around the screened interval and to an elevation of 1 or 2 feet above the screened interval, and the sand pack will be sealed with 1 to 2 feet of hydrated bentonite and then soil fill up to the ground surface to prevent surface water intrusion. The permeability tests will be conducted as falling head and/or rising head 'slug' tests, where water is added or removed from the wells and the subsequent rise or drop in water level is recorded over time until the water level largely recovers to its initial condition. Alternatively, or in addition to the slug testing, if a constant rate of water addition or withdrawal can be maintained at a relatively constant water level in the well, the associated flow rate and water level will be recorded (i.e. a constant head test). Following data collection, the resulting field measurements will be used to estimate the saturated permeability at each test location using an appropriate analysis method for the field testing conducted (e.g., Bouwer and Rice, Hvorslev, Dagan, and/or other methods as appropriate for partially penetrated unconfined aquifers). The permeability results will be used to support the evaluation of potential dewatering and settlement rates and the design of a NAPL recovery or control system if warranted.

#### **2.3 NAPL Assessment**

Additional testing is planned to support the evaluation of the nature, extent, and potential mobility and recoverability of the observed NAPLs within the impoundment. This additional testing will consist of NAPL bail-down recovery testing, and the collection of NAPL samples for selected physical and chemical property testing as described in the following subsections. Prior to the selection of locations for NAPL bail-down transmissivity testing, an inclusive round of NAPL gauging will be completed on each existing 1-inch diameter piezometer in Parcel B14. Although piezometers B14-044-PZ through B14-047-PZ will be gauged during this event, these four piezometers will not be considered for transmissivity testing as they are located outside the Parcel B14 boundary.

#### *2.3.1 NAPL Bail-Down Transmissivity Testing*

NAPL bail-down transmissivity testing will be completed in accordance with the ASTM E2856- 13 (Estimation of LNAPL Transmissivity): Bail-down/Slug Testing Field Methods.





NAPL bail-down transmissivity testing will be conducted at selected monitoring well locations to support the assessment of potential NAPL migration and recoverability. If such studies indicate that NAPL migration beyond the impoundment embankment is a potential concern during or following the planned fill placement activities, some type of NAPL monitoring and recovery/control will likely be proposed as part of the Response Action Plan for the parcel.

A NAPL bail-down transmissivity test will be completed at three select locations, which will be selected following the completion of an inclusive round of NAPL gauging for existing 1-inch wells. The three locations with the greatest thickness of product recorded during this gauging event will be selected, but no location with less than 0.25 ft on NAPL will be selected. Based on the gauging data included in **Appendix C**, it is anticipated that all 3 locations will have at least one foot of NAPL thickness present. Once the three locations have been determined, a 2-inch monitoring well will be installed at each location for the purpose of completing the bail-down transmissivity testing. Following installation, the monitoring wells will be developed to ensure the transmissivity values collected from the tests are representative of the impoundment area. Each test consists of a single NAPL removal event in which the accumulated NAPL is removed from the monitoring well, followed by continuous NAPL gauging. The minimum NAPL gauging frequency recommended by ASTM E2856-13 corresponds to a 5% or 0.05 feet change in NAPL thickness, whichever is less, for the first 100 minutes. As stated in ASTM E2856-13, the minimum practical time for measuring the fluid levels with a single interface probe is at 1-minute intervals. After the first 100 minutes, the frequency of NAPL measurements will be dependent on the NAPL recovery rate, and an estimated schedule will be implemented based on a preliminary review of the data from the first 100 minutes of testing. A slow recovery rate is predicted due to the NAPL observed in the on-site piezometers; therefore, the test may take days, weeks, or months to complete. The test is considered complete when the NAPL thickness has stabilized, i.e. when the NAPL thickness reaches a plateau with at least three measurements of LNAPL thickness over a period of at least one quarter of a log cycle when plotted on a semi-log scale. A definition of equilibrium as 3 readings within 10% of each other is proposed.

Prior to starting the bail-down transmissivity test, an oil-water interface probe will be used to gauge the three 2-inch monitoring wells. All gauging data, NAPL thicknesses, and visual product observations (color/viscosity) will be recorded on appropriate field log sheets (**Appendix E**). NAPL will be removed with a peristaltic or Xitech pump until all visible free product has been removed or until only trace levels of NAPL remain in the casing; the recovery of water and impacts on the water level will be minimized to the extent practical. The volume of NAPL that is recovered from each monitoring well will be recorded on the field log, as will the new depth to water and depth to product. The NAPL removal and 0-minute gauging event will start the clock for the baildown transmissivity test. The data will be recorded in the American Petroleum Institute (API) field worksheets included in the *API LNAPL Transmissivity Workbook: A Tool for Bail-down Test Analysis* dated June 2012 (**Appendix E**). The test will be continued until the NAPL thickness has stabilized as discussed above.

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The API worksheets are designed to calculate NAPL transmissivity with three different models: Bouwer and Rice (1976), Cooper and Jacob (1946), and Cooper, Bredehoeft and Papadopulos (1967). Following the completion of the transmissivity tests, the model that best fits the data will be utilized for the transmissivity value. Final transmissivity values will then be compared to guideline reference values to help make conclusions regarding NAPL recoverability and the need for any NAPL recovery or control measures as part of the Response Action Plan.

#### *2.3.2 NAPL Laboratory Testing*

As part of the NAPL assessment, and in conjunction with the bail-down transmissivity testing, a sample of the NAPL recovered from each of the monitoring wells will be placed into laboratorysupplied bottleware and submitted to Pace Analytical Services, Inc. (PACE) for density and viscosity testing. The results of this testing will support the evaluation of potential NAPL mobility and recoverability and potential treatment or disposal requirements for any recovered NAPL.

#### **2.5 Additional Provisions**

All field protocols will be conducted in accordance with the Standard Operating Procedures (SOPs) and requirements given in the property-wide Quality Assurance Project Plan (QAPP). The investigation will also be conducted under the property-wide Health and Safety Plan (HASP). Any NAPL or water removed from the piezometers and temporary wells will be containerized and subsequently disposed of at an appropriate and permitted disposal facility. The selected disposal facility will be approved by the MDE prior to shipment. Any waste generated during the PDI activities will be placed in designated drums and will be managed in bulk with waste from other investigations and will be appropriately characterized prior to disposal.

#### **3.0 CLOSING**

If you have any questions, or if we can provide any additional information at this time, please do not hesitate to contact ARM Group Inc. at 410-290-7775.

ARM Group Inc.

Respectfully submitted, ARM Group Inc.

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Stewart Kabis, G.I.T. T. Neil Peters, P.E.

 $N/L$   $R+$ 

Project Geologist Senior Vice President



#### Attachments:

#### Figures

Figure 1 – Site Location Map

Figure 2 – Piezometer and Well Locations

Figure 3 – Geotechnical Boring Locations

#### Tables

Table 1 – Parcel B14: Pre-Design Investigation Summary

#### Appendices

Appendix A – Soil Boring and Piezometer Construction Logs Appendix B – NAPL Gauging Summary Tables Appendix C – Maximum NAPL Thickness Data Appendix D – HCEA Geotechnical Boring Logs Appendix E – Field Forms



# **FIGURES**







# **TABLES**

#### Table 1 Parcel B14: Pre-Design Investigation Summary Former Sparrows Point Steel Mill Sparrows Point, Maryland



Notes:

1. SPT = Standard Penetration Test

2. TPD = To Be Determined

# **APPENDIX A**






















































# **APPENDIX B**



NA = Not Applicable

NM = Not Measured

**SHADED** = NAPL Detection

NA = Not Applicable

NM = Not Measured

**SHADED** = NAPL Detection



NA = Not Applicable

NM = Not Measured

**SHADED** = NAPL Detection



NA = Not Applicable

NM = Not Measured

**SHADER** = 
$$
NAPL
$$
 Detection



NA = Not Applicable

NM = Not Measured

**SHADED** = 
$$
NAPL
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 Detection



# **APPENDIX C**

# **Table 1 NAPL Piezometer Construction Details and Product Thickness Parcel B14 Tradepoint Atlantic Sparrows Point, Maryland**



NP: No Product NA: Not Applicable

# **APPENDIX D**

**Boring Location Plan 2** *Legend* **Legend Legend Legend Legend Boring 208** 

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Boring 218 Boring 219

**HILLIS-CARNES** Engineering Associates, Inc. 417 Maryland Avenue, Delmar, MD 21875**ENGINEERING ASSOCIATES** http://www.hcea.com

#### **Project: S18032 Fitzell Substation In Situ**

**Sparrows Point, MarylandLocation:**



#### **SBTn legend** 1. Sensitive fine grained4. Clayey silt to silty clay7. Gravely sand to sand Ħ 5. Silty sand to sandy siltП 8. Very stiff sand to clayey sand2. Organic materialn. 9. Very stiff fine grained 3. Clay to silty clay6. Clean sand to silty sand

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#### **CPT: Fitzell Project B-214**

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#### **Project: S18032 Fitzell Substation In Situ**

**Sparrows Point, MarylandLocation:**



## **Mod. SBTn legend**



#### **CPT: Fitzell Project B-214**

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#### **Project: S18032 Fitzell Substation In Situ**

**Sparrows Point, MarylandLocation:**



#### **Calculation parameters**

Permeability: Based on SBT<sub>n</sub> SPT  $N_{60}$ : Based on  $I_c$  and  $q_t$ 

Young's modulus: Based on variable alpha using  $I_c$  (Robertson, 2009)

Relative desnisty constant,  $C_{Dr}$ : 350.0 Phi: Based on Kulhawy & Mayne (1990)User defined estimation data

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#### **Project: S18032 Fitzell Substation In Situ**

**Sparrows Point, MarylandLocation:**



#### **Calculation parameters**



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## **CPT: Fitzell Project B-214**

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#### **Project: S18032 Fitzell Substation In Situ**

**Sparrows Point, MarylandLocation:**



#### **Calculation parameters**

Soil Sensitivity factor,  $N_S$ : 7.00

User defined estimation data

#### **CPT: Fitzell Project B-214**

$$
c_h = \frac{T \times r^2 \times I_r^{0.5}}{t_{50}}
$$

where:

T: time factor given by Houlsby and Teh's (1988) theory corresponding to the porepressure position r: piezocone radius

I<sub>r</sub>: stiffness index, equal to shear modulus G divided by the undrained strength of clay (S<sub>u</sub>).

 $t_{50}$ : time corresponding to 50% consolidation

## **Permeability estimates based on dissipation test**

The dissipation of pore pressures during a CPTu dissipation test is controlled by the coefficient of consolidation in the horizontal direction (c<sub>h</sub>) which is influenced by a combination of the soil permeability (k<sub>h</sub>) and compressibility (M), as defined by the following:

$$
k_h = c_h \times \gamma_w / M
$$

where: M is the 1-D constrained modulus and  $y_w$  is the unit weight of water, in compatible units.



**Project: S18032 Fitzell Substation In Situ Sparrows Point, Maryland Location:**

## **Dissipation Tests Results**

## **Dissipation tests**

Dissipation tests consists of stopping the piezocone penetration and observing porepressures (u) with elapsed time (t). The data are automatic recorded by the field computer and should take place until a minimum of 50% dissipation.

The porepressures are plotted as a function of square root of (t). The graphical technique suggested by Robertson and Campanella (1989), yields a value for  $t_{50}$ , which corresponds to the time for 50% consolidation.

The value of the coefficient of consolidation in the radial or horizontal direction  $c_h$  was then calculated by Houlsby and

Coords: X:0.00, Y:0.00 Cone Type: NOVA U2 Cone Operator: R. Harman





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#### **Project: S18032 Fitzell Substation In Situ**

**Sparrows Point, MarylandLocation:**



## **CPT: Fitzell Project B-215 offset**

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#### **Project: S18032 Fitzell Substation In Situ**

**Sparrows Point, MarylandLocation:**





## **CPT: Fitzell Project B-215 offset**

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#### **Project: S18032 Fitzell Substation In Situ**

**Sparrows Point, MarylandLocation:**



#### **Calculation parameters**

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## **CPT: Fitzell Project B-215 offset**

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#### **Project: S18032 Fitzell Substation In Situ**

**Sparrows Point, MarylandLocation:**



#### **Calculation parameters**



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## **CPT: Fitzell Project B-215 offset**

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#### **Project: S18032 Fitzell Substation In Situ**

**Sparrows Point, MarylandLocation:**



#### **Calculation parameters**

Soil Sensitivity factor,  $N_S$ : 7.00

User defined estimation data

## **CPT: Fitzell Project B-215 offset**

horizontal defined by

$$
k_h = c_h \times \gamma_w / M
$$

where: M is the 1-D constrained modulus and  $y_w$  is the unit weight of water, in compatible units.



## **HILLIS-CARNES S** Engineering Associates, Inc. 417 Maryland Avenue, Delmar, MD 21875 ENGINEERING ASSOCIATES The Principle interval and the second

**Project: S18032 Fitzell Substation In Situ Sparrows Point, Maryland Location:**

# **Dissipation Tests Results**

# **Dissipation tests**

Dissipation tests consists of stopping the piezocone penetration and observing porepressures (u) with elapsed time (t). The data are automatic recorded by the field computer and should take place until a minimum of 50% dissipation.

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$$
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$$
(c_h)
$$
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#### **Project: S18032 Fitzell Substation In Situ**

**Sparrows Point, MarylandLocation:**



3. Clay to silty clay

6. Clean sand to silty sand

H

## **CPT: Fitzell Project B-215**

Total depth: 17.39 ft, Date: 3/8/2018 Surface Elevation: 7.00 ftCoords: X:0.00, Y:0.00 Cone Type: NOVA U2Cone Operator: R. Harman

9. Very stiff fine grained

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#### **Project: S18032 Fitzell Substation In Situ**

**Sparrows Point, MarylandLocation:**



## **Mod. SBTn legend**



## **CPT: Fitzell Project B-215**

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#### **Project: S18032 Fitzell Substation In Situ**

**Sparrows Point, MarylandLocation:**



#### **Calculation parameters**

Permeability: Based on SBT<sub>n</sub> SPT  $N_{60}$ : Based on  $I_c$  and  $q_t$ 

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Relative desnisty constant,  $C_{Dr}$ : 350.0 Phi: Based on Kulhawy & Mayne (1990)User defined estimation data $\overline{\phantom{a}}$ 

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**CPT: Fitzell Project B-215**

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#### **Project: S18032 Fitzell Substation In Situ**

**Sparrows Point, MarylandLocation:**



#### **Calculation parameters**



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## **CPT: Fitzell Project B-215**

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#### **Project: S18032 Fitzell Substation In Situ**

**Sparrows Point, MarylandLocation:**



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#### **CPT: Fitzell Project B-215**

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#### **Project: S18032 Fitzell Substation In Situ**

**Sparrows Point, MarylandLocation:**



CPeT-IT v.2.0.2.5 - CPTU data presentation & interpretation software - Report created on: 3/9/2018, 3:48:00 PMProject file: C:\Users\fernando\_garcia\Desktop\Fitzell Project\Fitzell Project CPT Analyses.cpt

## **CPT: Fitzell Project B-216**
**HILLIS-CARNES** Engineering Associates, Inc. 417 Maryland Avenue, Delmar, MD 21875**ENGINEERING ASSOCIATES** http://www.hcea.com

#### **Project: S18032 Fitzell Substation In Situ**

**Sparrows Point, MarylandLocation:**



#### 1. CCS: ClayLike - Contractive, Sensitive4. TC: Transitional - Contractive7. SD: Sand-like - Dilative 5. TD: Transitional - Dilative2. CC: Clay-like - ContractiveТ. 6. SC: Sand-like - Contractive3. CD: Clay-Like: Dilative

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## Surface Elevation: 12.00 ft

Coords: X:0.00, Y:0.00Cone Type: NOVA U2

Cone Operator: R. Harman

#### **CPT: Fitzell Project B-216**

Total depth: 55.51 ft, Date: 3/8/2018

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#### **Project: S18032 Fitzell Substation In Situ**

**Sparrows Point, MarylandLocation:**



#### **Calculation parameters**

Permeability: Based on SBT<sub>n</sub> SPT  $N_{60}$ : Based on  $I_c$  and  $q_t$ 

Young's modulus: Based on variable alpha using  $I_c$  (Robertson, 2009)

Relative desnisty constant,  $C_{Dr}$ : 350.0 Phi: Based on Kulhawy & Mayne (1990)User defined estimation data

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**Sparrows Point, MarylandLocation:**



#### **Calculation parameters**



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#### **Project: S18032 Fitzell Substation In Situ**

**Sparrows Point, MarylandLocation:**



#### **Calculation parameters**

Soil Sensitivity factor,  $N_S$ : 7.00

User defined estimation data

#### **CPT: Fitzell Project B-216**

where: M is the 1-D constrained modulus and  $y_w$  is the unit weight of water, in compatible units.



## **Dissipation Tests Results**

**Sparrows Point, Maryland Location:**

**Project: S18032 Fitzell Substation In Situ**

## **Dissipation tests**

Dissipation tests consists of stopping the piezocone penetration and observing porepressures (u) with elapsed time (t). The data are automatic recorded by the field computer and should take place until a minimum of 50% dissipation.

The porepressures are plotted as a function of square root of (t). The graphical technique suggested by Robertson and Campanella (1989), yields a value for  $t_{50}$ , which corresponds to the time for 50% consolidation.

The value of the coefficient of consolidation in the radial or horizontal direction  $c_h$  was then calculated by Houlsby and Teh's (1988) theory using the following equation:

50 5.0  $2 \times I_r$  $h = \frac{}{}$  $c_h = \frac{T \times r^2 \times I}{I}$  $=\frac{T\times r^2\times r^2}{r^2}$ 

where:

T: time factor given by Houlsby and Teh's (1988) theory corresponding to the porepressure position r: piezocone radius

I<sub>r</sub>: stiffness index, equal to shear modulus G divided by the undrained strength of clay (S<sub>u</sub>).

 $t_{50}$ : time corresponding to 50% consolidation

## **Permeability estimates based on dissipation test**

The dissipation of pore pressures during a CPTu dissipation test is controlled by the coefficient of consolidation in the horizontal direction (c<sub>h</sub>) which is influenced by a combination of the soil permeability (k<sub>h</sub>) and compressibility (M), as

$$
k_h = c_h \times \gamma_w / M
$$

$$
x_1 \in \mathcal{X}_1 \cup \mathcal{X}_2
$$





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#### **Project: S18032 Fitzell Substation In Situ**

**Sparrows Point, MarylandLocation:**



#### **CPT: Fitzell Project B-217**

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#### **Project: S18032 Fitzell Substation In Situ**

**Sparrows Point, MarylandLocation:**



3. CD: Clay-Like: Dilative

6. SC: Sand-like - Contractive

Т.

#### **CPT: Fitzell Project B-217**

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#### **Project: S18032 Fitzell Substation In Situ**

**Sparrows Point, MarylandLocation:**



#### **Calculation parameters**

Permeability: Based on SBT<sub>n</sub> SPT  $N_{60}$ : Based on  $I_c$  and  $q_t$ Young's modulus: Based on variable alpha using  $I_c$  (Robertson, 2009) Relative desnisty constant,  $C_{Dr}$ : 350.0 Phi: Based on Kulhawy & Mayne (1990)User defined estimation data

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**CPT: Fitzell Project B-217**

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#### **Project: S18032 Fitzell Substation In Situ**

**Sparrows Point, MarylandLocation:**



#### **Calculation parameters**



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## **CPT: Fitzell Project B-217**

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#### **Project: S18032 Fitzell Substation In Situ**

**Sparrows Point, MarylandLocation:**



#### **Calculation parameters**

Soil Sensitivity factor,  $N_S$ : 7.00

User defined estimation data

#### **CPT: Fitzell Project B-217**

**HILLIS-CARNES Engineering Associates, Inc.** 

417 Maryland Avenue, Delmar, MD 21875

**Project: S18032 Fitzell Substation In Situ**

**Sparrows Point, Maryland Location:**

ENGINEERING ASSOCIATES The Principle interval and the second

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c_h=\frac{T\!\times\!r^2\!\times\! I_r^{\,0.5}}{t_{50}}
$$

where:

T: time factor given by Houlsby and Teh's (1988) theory corresponding to the porepressure position r: piezocone radius

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$$
k_h = c_h \times \gamma_w / M
$$

where: M is the 1-D constrained modulus and  $y_w$  is the unit weight of water, in compatible units.



Cone Operator: R. Harman









# **APPENDIX E**



