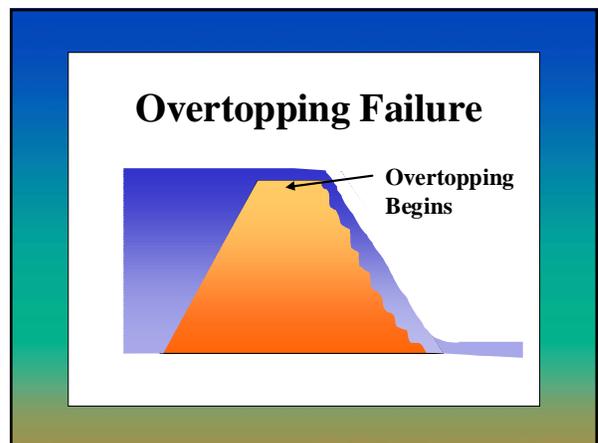
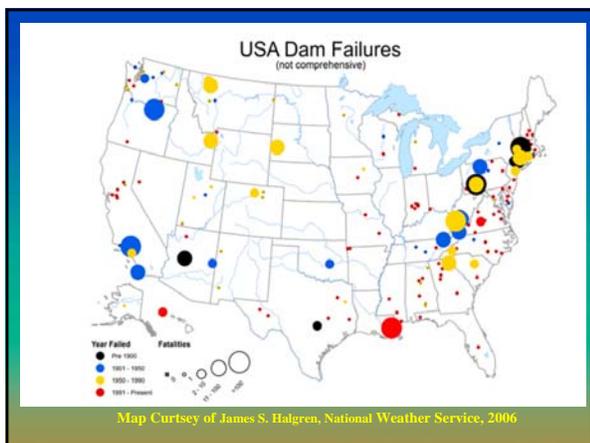
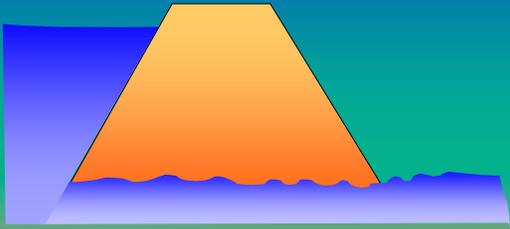


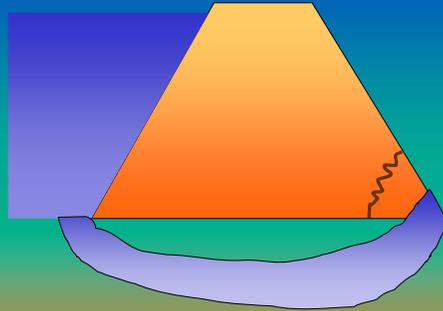
- Other Causes of Dam Failures**
- Structural Failures
 - Earthquake
 - Trees
 - Animal Burrows
 - Poor Design
 - Poor Construction
 - Neglect / Lack of Maintenance
 - Lightning



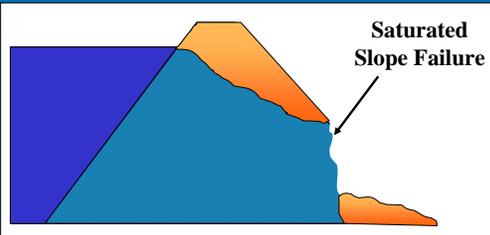
Piping Failure for Earth Dam



Foundation Failure



Slope Failure



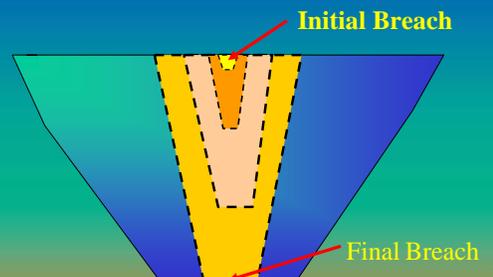
Embankment Dam Schematic

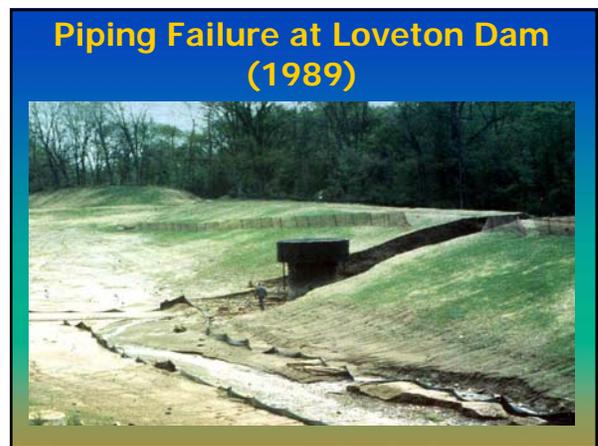
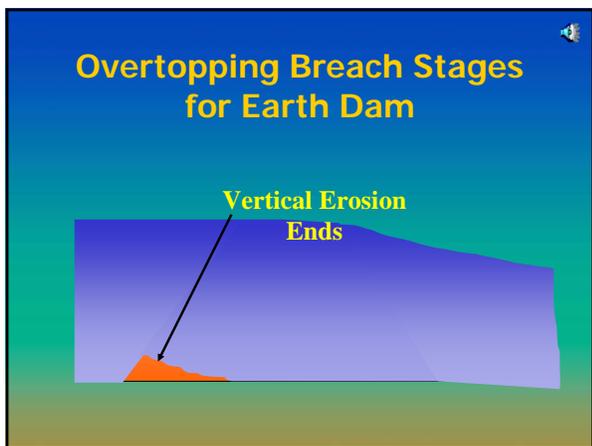
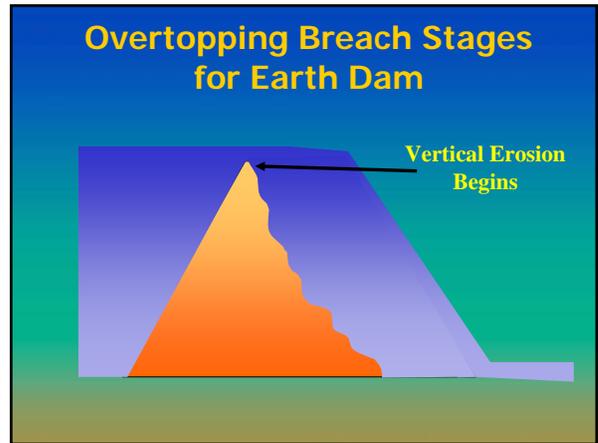
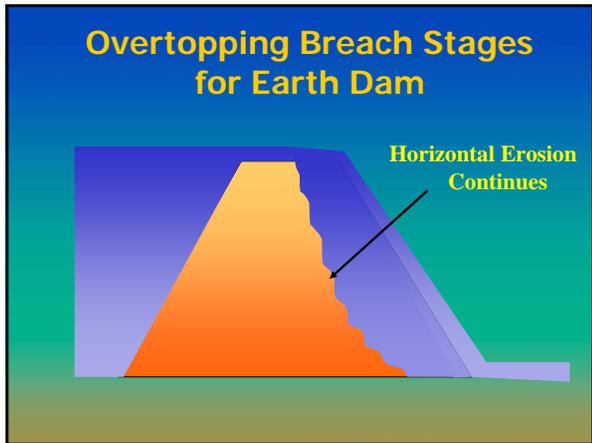
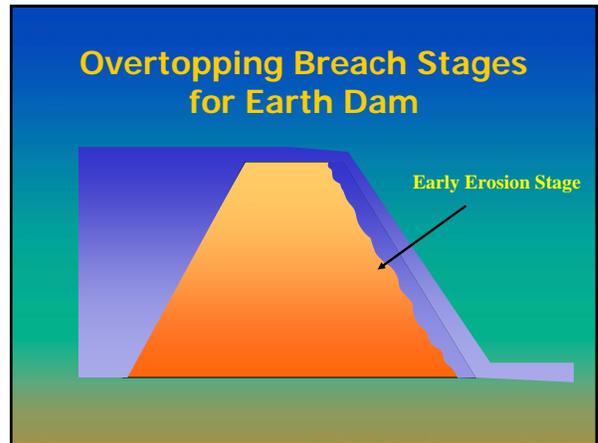
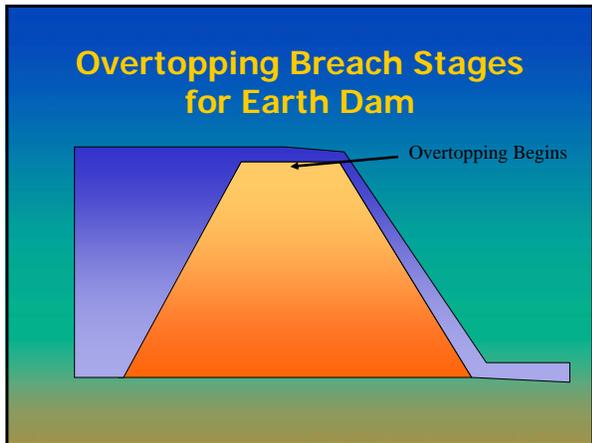


Dam Overtopping Photo



Overtopping Breach of Earth Dam





Loveton Dam Failure (1989)



Loveton Failure Viewed from Downstream



Medford Quarry Wash Pond Piping Failure



Piping Failure

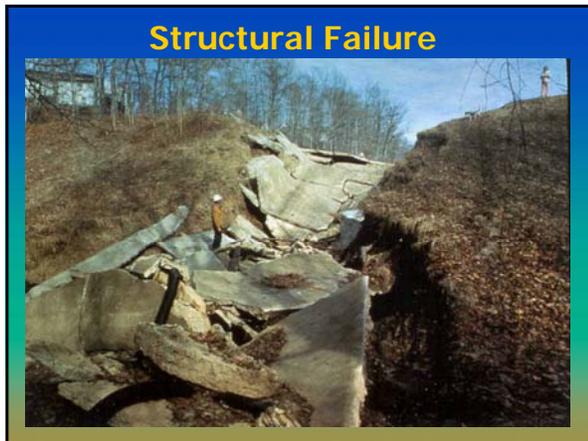


Annap. Mall Piping Failure



Sinkhole in Dam Crest





Dam Hazard Classifications

- Low Hazard = Class "a"
- Significant Hazard = Class "b"
- High Hazard = Class "c"

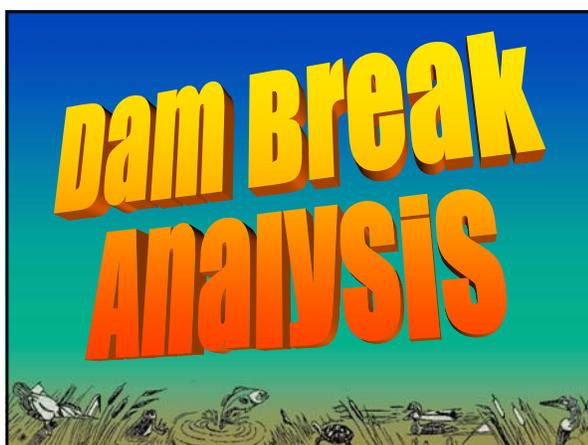
MDE Dam Hazard Classifications

- Low Hazard - Potential loss of life is very unlikely due to low danger flood depths.
- Significant Hazard - Potential loss of life is possible with no more than 6 lives in jeopardy and flooding to no more than two isolated houses and downstream roads.
- High Hazard - Potential loss of life is very likely with more than 6 lives in jeopardy, and serious damage to residential, commercial, or industrial buildings, and downstream roads.

Loss of Life from Dam Failure Varies with Warning Time

Warning time < 15",	Loss of Life = .5(PAR)
Warning time 15" to 90",	Loss of Life = PAR ⁶
Warning time > 90",	Loss of Life = .0002(PAR)

Source: "A Procedure for Estimating Loss of Life Caused by Dam Failure", USBR, Wayne Graham, 1999



Incremental Flood Analysis

Flood Conditions without & with Dam Failure

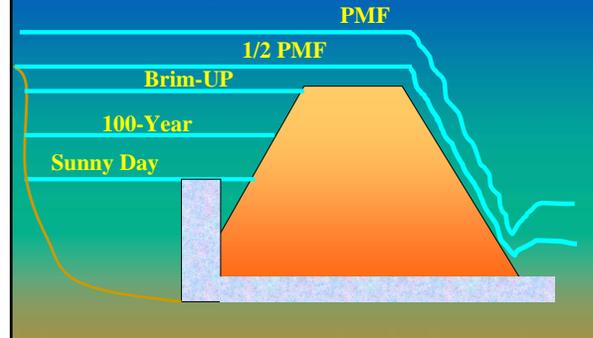
Storms to Evaluate

- Sunny Day (Normal Pool)
- 100-Year Storm
- Brim-up Storm (fill reservoir to top of dam)
- 1/2 of Probable Maximum Flood
- Full Probable Maximum Flood

Probable Maximum Flood (PMF)

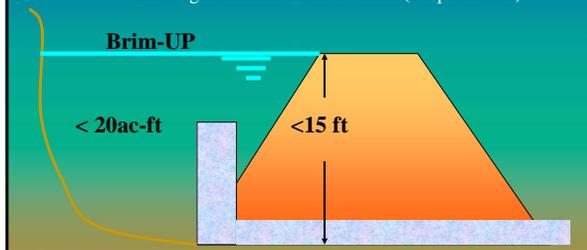
PMF - the largest flood considered possible based on the most severe combination of meteorological and hydrologic conditions that are reasonably possible.

Failure Storms to Analyze

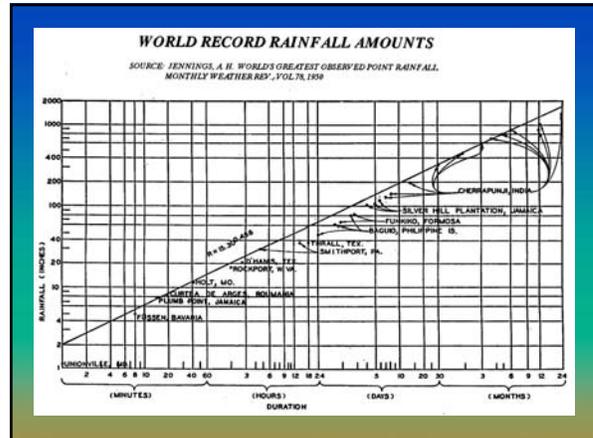
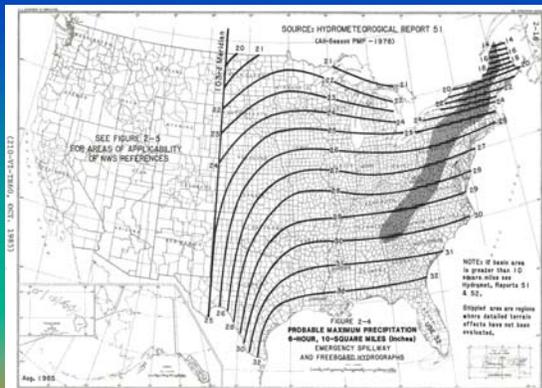
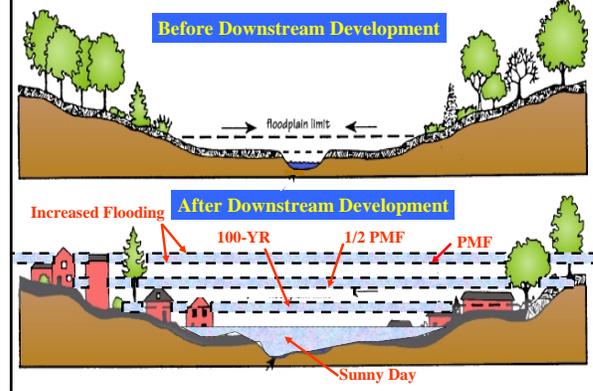


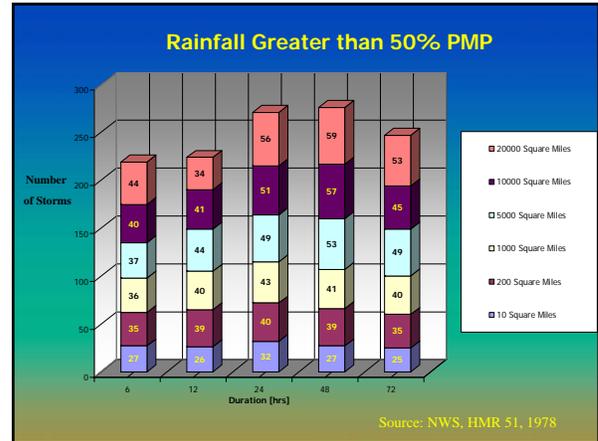
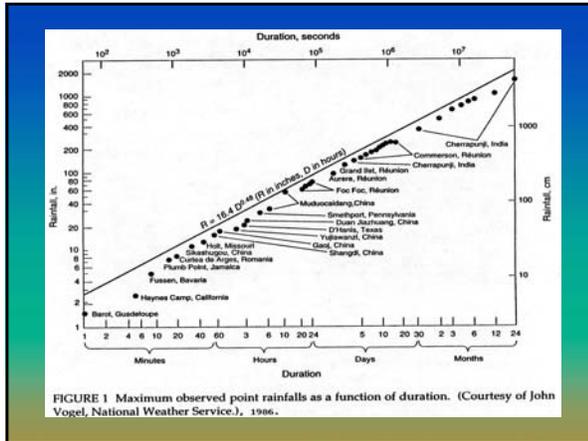
Small Dam or Pond Use NWS Dam Break Equation

- 15 ft or less in height,
- Storage volume less than 20 acre-feet
- Drainage area less than 640 acres (1 square mile)



Increased Flood Risks





Hydrology for Dams

- GISHydro2000 Model > 400 acres
- TR-20 Models
- HEC-1 Model
- HydroCad Model (new dam break added)

Web Sites:

www.gishydro.umd.edu

www.hydrocad.net

Dam Break Models

- HEC-1 Computer Model
- HECRAS Computer
- NWS DAMBRK or FLDWAV
- NWS Simple DAMBRK Equation
- HEC-HMS (New HEC-1 but not recommended)

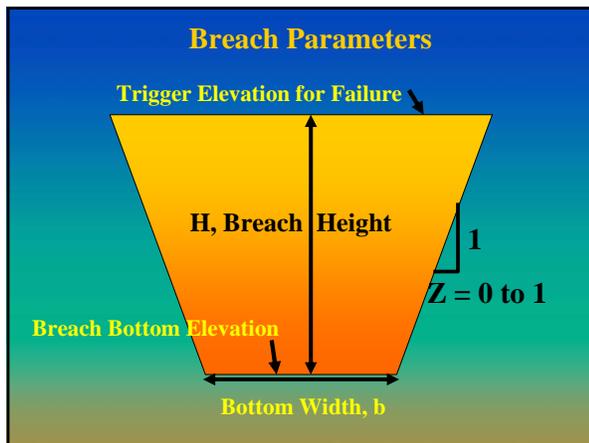
Learn HEC1 Model

```

* ALL DATA IS ENTERED IN TABLES OF 5 WITH THE COLUMN NUMBER INDICATING THE
  USE THESE FORMATS:
* THE FIRST CARD ALLOWS YOU TO USE A FREE FORMAT WHERE YOU DON'T HAVE TO
  WORRY ABOUT COLUMN LOCATIONS. You place a comma between data entries.
*FREE
* THE NEXT CARD TELLS THE COMPUTER TO PRINTOUT A FREE DIAGRAM OF THE
  HYDROLOG
*THE DIAGRAM
* THE NEXT THREE CARDS ARE PROJECT DESCRIPTION CARDS. USE ONE IN EACH OF
  THESE CARDS
IN Your Dam Name, File Name (*.dat)
IN THE YEAR STARTING WITH A W/THOUT YEAR ENDING (DESCRIPTION)
IN HYDROLOGIC DATA BEGINNING FROM 11:15 AND END AT LAST OR ONLY ONE IN
  CARD
* Next card is the time computing indicates 5 minutes interval and 100
  ordinates
IN 5 100
* The next card tells the computer how much to print out, recommend
  minimum = 5
IN 5
* The next card says that there are 3 lake (without failure) & with
  failure!
IN 3
  
```

Breach Parameters for HEC-1 Model

- Breach Bottom Elevation
- Breach Top Elevation (Trigger Elevation)
- Bottom Breach Width
- Breach Side Slope
- Time of Failure



Suggested Breach Parameters for Earth Dams

Source	Average Breach Width (ft)	Breach Side Slope (1V:ZH)	Breach Failure Time (hrs)
NWS (1988)	1H to 5H	Z = 0 to 1	0.1 to 2.0
COE (1980)	0.5H to 4H	Z = 0 to 1	0.5 to 4
FERC (1991)	1H to 5H	Z = 0 to 1	0.1 to 1.0
USBR (1982)	3H	N/A	0.00333b
Boss Dambrk (1988)	0.5 to 4H	Z = 0 to 1	0.5 to 4
Harrington (1999)	1H to 8H	Z = 0 to 1	H/120 to H/180

Froelich Breach Predictor Equations

$$b = 9.5 K_0 (V_s H)^{0.25}$$

$$T_f = 0.59 (V_s^{0.47}) / H^{0.91}$$

b = Average Breach Width (ft),
T_f = Time of Failure (hrs)

K₀ = 0.7 for Piping & 1.0 for Overtopping Failure
V_s = Storage Volume (ac-ft)
H = Selected Failure Depth (ft) above Breach Bottom
T_f = Time of Failure (hrs, ~H/120 or Minimum of 10 Min)

Dam Break Models

NWS Simple Dam Break Equation

$$Q_b = Q_0 + 3.1 B_r (C / (T_f + C / \sqrt{H}))^3$$

Q_b = Breach + Non-Breach Flow (cfs)
Q₀ = Non-Breach Flow (cfs)
B_r = Final Average Breach Width (ft, ~ 1H to 5H)
C = 23.4 A_s/B_r
A_s = Reservoir Surface Area (ac) at Failure Elevation
H = Selected Failure Depth (ft) above Final Breach Elevation
T_f = Time of Failure (hrs, ~H/120 or Minimum of 10 Min)

Dam Break Models

- SCS (NRCS) Breach Formula

$$Q_b = 3.2 H^{5/2}$$
 - Usually Conservative Estimate of Breach Flow but not Always
 - Storage Volume not included in Formula
 - Similar to a V-Notch Weir Formula

COMPARISON OF DAM BREACH EQUATIONS
NWS SIMPLE DAMBRK vs NRCS BREACH EQUATIONS

NWS SIMPLE DAMBRK EQUATION: $Q_{NWS} = 3.1B_s(C/T_f + C/\sqrt{H})^3$

NRCS MD-378 EQUATION: $Q_{NRCS} = 3.2H^{2.5}$

Br = 3H (Breach Width, ft)
H = Height of Water at failure, ft
C = 23.4As/Br = 7.6As/H
As = Surface Area at Failure (acres)
T_f = H/120 (Failure Time, hrs)
= Minimum Time of 10 min = 0.17 hrs

H (ft)	As (ac)	T _f (hrs)	C	Q _{NWS} (cfs)	Q _{NRCS} (cfs)
5.0	0.5	0.17	0.47	88	179
5.0	1.0	0.17	1.56	270	179
5.0	5.0	0.17	7.80	451	179
10.0	0.5	0.17	0.23	79	1012
10.0	1.0	0.17	0.78	610	1012
10.0	5.0	0.17	3.90	1996	1012
15.0	0.5	0.17	0.26	184	2789
15.0	1.0	0.17	0.52	696	2789
15.0	5.0	0.17	2.40	4117	2789
20.0	1.0	0.17	0.39	648	5724
20.0	3.0	0.17	1.17	3705	5724
20.0	10.0	0.17	3.90	9750	5724
40.0	10.0	0.33	1.95	10803	32382
40.0	20.0	0.33	3.90	26012	32382
40.0	40.0	0.33	7.80	46207	32382

Dam Break Models

- NWS Simple Dam Break Equation
 - Developed from NWS Full Dam Break Model
 - Based on Falling Head Weir Flow
 - Input Non-Breach Flow, Surface Area, Selected Failure Depth, & Time of Failure

Dam Break Models

- NWS Full Dam Break Model (DAMBRK)
 - Very Difficult to Learn & Temperamental
 - Uses Unsteady State Dynamic Routing by a Finite Difference Technique
 - Includes Pressure & Acceleration Effects
 - A Hydrograph must be Inputted
 - Has Been Replaced by NWS Flood Wave Model (FLDWAV), Free Download at: <http://hsp.nws.noaa.gov/oh/hrl/rvrmech/rvrmain.htm>

Recommended Dam Failure Methods for Small Dams 15 feet or less in height

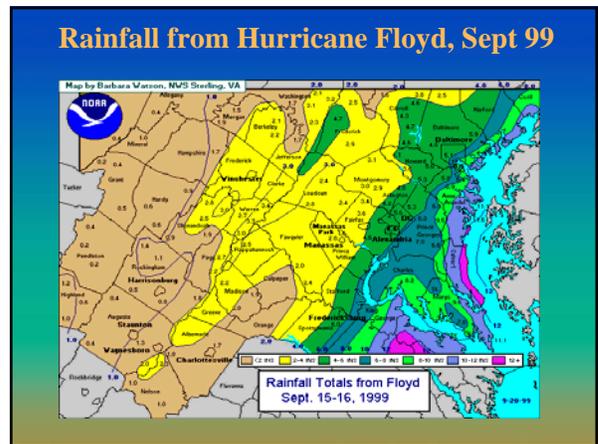
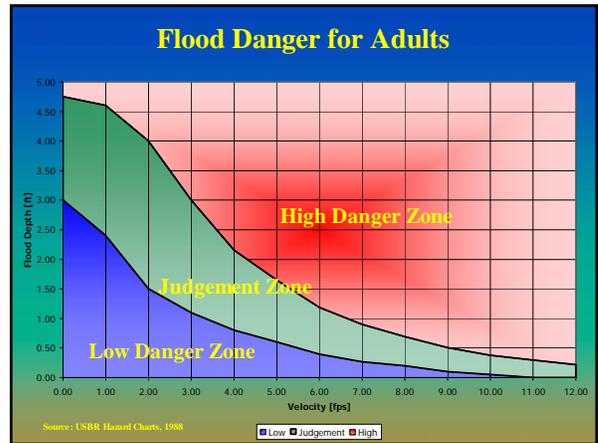
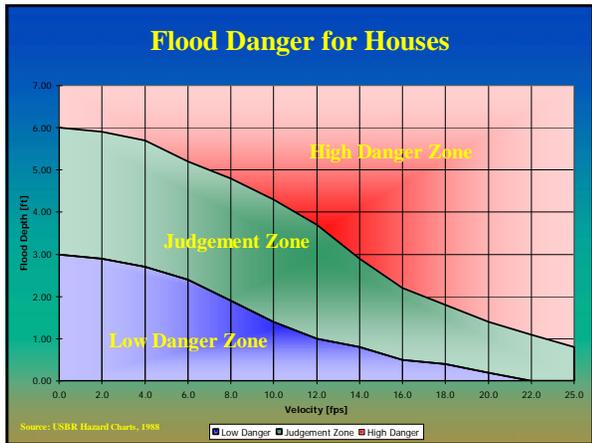
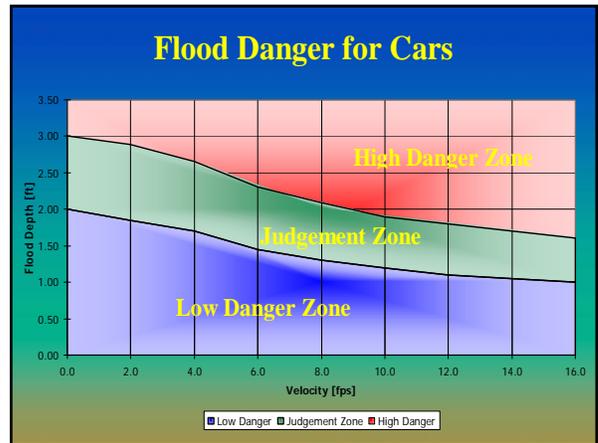
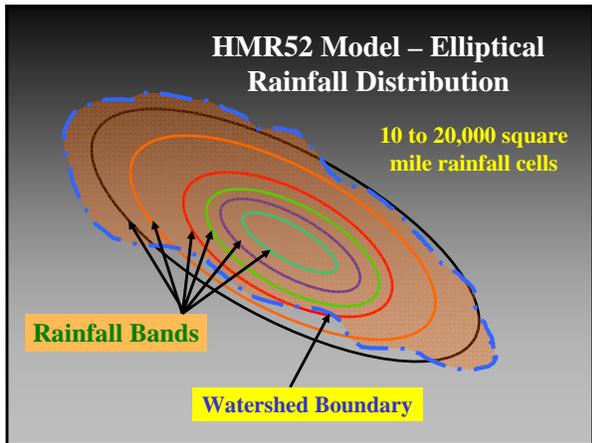
- Use NWS SMPDBK Equation to determine Breach Flows
- Use HECRAS Model to determine Downstream Flood Depths
- Stop Danger Reach when roads flood < 1.5 feet, and Flooding to Houses & Buildings < 6 inches

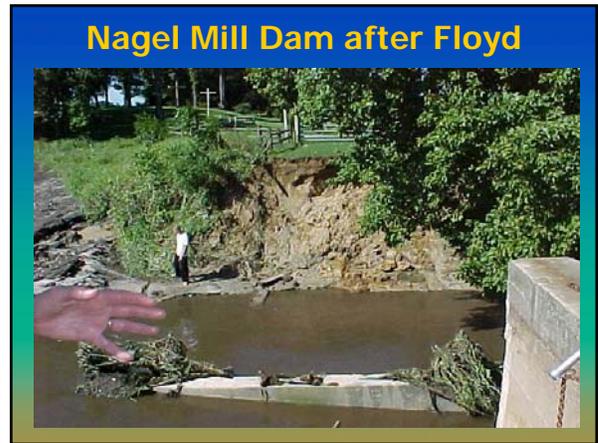
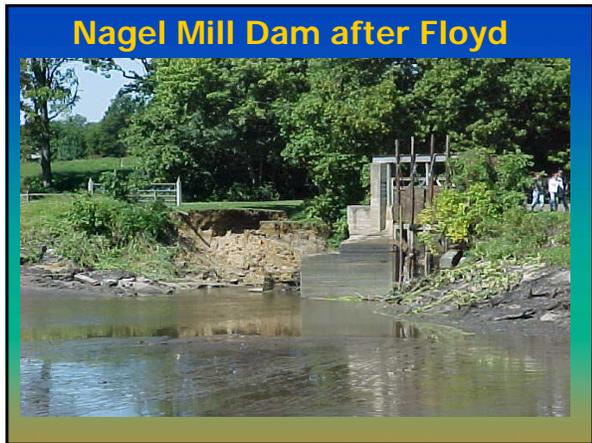
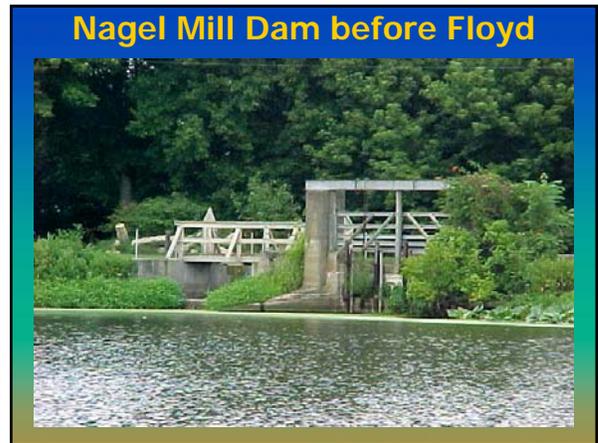
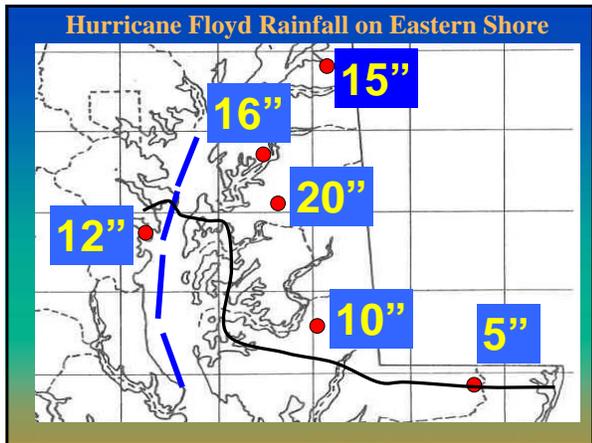
Recommended Dam Failure Methods for Dams > 15 & < 75 feet high

- Use Hec-1 Model for Breach Flows
- Use HECRAS Model to determine Downstream Flood Depths & USBR Hazard Charts to determine Flood Dangers
- Stop Danger Reach when Increased Flooding < 1 foot or no structures flooded

Recommended Dam Failure Methods for Dams > or = 75 feet high

- Use HMR-52 & HEC-1 Model for Hydrology
- Use HECRAS Model for Breach Flow
- Use the Unsteady HECRAS Model if feasible
- May also use DAMBRK , or FLDWAV Models for Breach Flow





Nagels Breach Statistics

Piping Failure
 Breach Width = 60 ft = 4H
 Side Slope Z = 0.4
 Time of Failure < 20 min

Foreman Branch Dam before Floyd



Foreman Branch Dam after Floyd



Foreman Branch Dam after Floyd



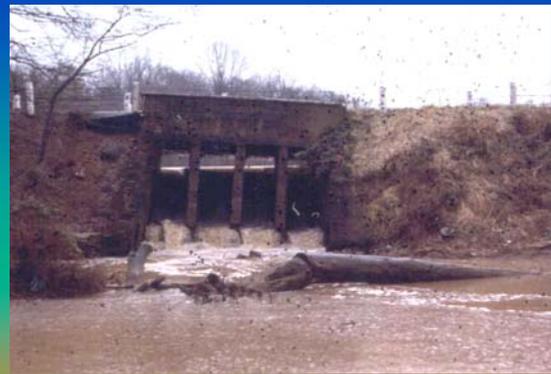
Foreman Branch Dam after Repair



**Foreman Dam Breach
Statistics**

Overtopping Failure
Breach Width = 85 ft = 8H
Side Slope Z = 0.5
Time of Failure < 30 min

Frazer Mill Dam before Floyd



Frazer Mill Dam after Floyd



Frazer Mill Dam after Floyd



Frazer Dam Breach Statistics

Overtopping Failure
Breach Width = 120 ft = 6H
Side Slope Z = 0.6
Time of Failure Unknown

Jones Lake Dam before Floyd



Jones Lake Dam before Floyd



Jones Lake Dam after Floyd



Jones Lake Dam Breach Statistics

Piping Failure
Breach Width = 103 ft = 6H
Side Slope Z = 0.6
Failure Time Unknown

Sassafras Dam before Floyd



Sassafras Dam after Floyd



Sassafras Dam During Floyd



Sassafras Dam after Repair



Sassafras Dam During Repair



Sassafras Dam Breach Statistics

Overtopping Failure
Breach Width = 47 ft = 4H
Side Slope Z = 0.2
Failure Time = 15 Min

Stubbs Dam after Floyd



Stubbs Dam after Floyd



Stubbs Dam after Repair



Stubbs Dam Breach Statistics

Piping Failure
Breach Width = 30 ft = 2.5H
Side Slope Z = 0.2
Failure Time Unknown

Tuckahoe Dam after Floyd



Tuckahoe Breach below Spillway



St Pauls Emergency Spillway during Floyd



Boundary Dam Near Seattle Washington



Hoover Dam One of the "Seven Modern Civil Engineering Wonders"



MDE Dam Break Web Site

Go to www.mde.state.md.us & Search for technical references

- Microsoft Word Documents
 - Hazard Guidelines
 - Model Emergency Action Plans
- Microsoft Excel Spreadsheets
 - NWS Dam Break Equation
 - USBR Hazard Graphs
 - Hydrology Spreadsheets
 - Hydraulic Spreadsheets
- Executable Programs
 - HEC-1 Program
 - NWS Simple Dam Break Program
 - Sample Data for HEC-1 & NWS Simple Dam Break

Any Questions?



Bruce Harrington, MD Dam Safety, 410-713-3687