Total Maximum Daily Load of Sediment in the Jones Falls Watershed, Baltimore City and Baltimore County, Maryland

PUBLIC REVIEW DRAFT

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Table of Contents

List of Figures ii
List of Tables ii
List of Abbreviations iii
EXECUTIVE SUMMARY v
1.0 INTRODUCTION 1
2.0 SETTING AND WATER QUALITY DESCRIPTION 3
2.1 General Setting 3
2.1.1. Land Use 5
2.2 Source Assessment 8
2.2.1 Nonpoint Source Assessment 8
2.2.2 Point Source Assessment 12
2.2.3 Summary of Baseline Loads 13
2.3 Water Quality Characterization 14
2.4 Water Quality Impairment 18
3.0 TARGETED WATER QUALITY GOAL 20
4.0 TOTAL MAXIMUM DAILY LOADS AND SOURCE ALLOCATION 21
4.1 Overview 21
4.2 Analysis Framework 21
4.3 Scenario Descriptions and Results 25
4.4 Critical Condition and Seasonality 26
4.5 TMDL Loading Caps 26
4.6 Load Allocations Between Point and Nonpoint Sources 27
4.7 Margin of Safety 29
4.8 Summary of Total Maximum Daily Loads 30
5.0 ASSURANCE OF IMPLEMENTATION 31
REFERENCES 33
APPENDIX A – Watershed Characterization Data A1
APPENDIX B – MDE Permit Information B1
APPENDIX C – Technical Approach Used to Generate Maximum Daily Loads C1

List of Figures

Figure 1: Location Map of the Jones Falls Watershed in Baltimore City and Baltimore County, Maryland 4
Figure 2: Land Use of the Jones Falls Watershed..... 7
Figure 3: Percent Impervious vs. Percent Erosional Sediment Load Resultant from Streambank Erosion 12
Figure 4: Monitoring Stations in the Jones Falls Watershed 16
Figure 5: Jones Falls Watershed TMDL Segmentation 22
Figure C-1: Histogram of CBP River Segment Daily Simulation Results for the Jones Falls Watershed.....C5

List of Tables

Table ES-1: Jones Falls Baseline Sediment Loads (ton/yr)..... vii
Table ES-2: Jones Falls Average Annual TMDL of Sediment/Total Suspended Solids (ton/yr) vii
Table ES-3: Jones Falls Baseline Load, TMDL, and Total Reduction Percentage viii
Table 1: Land Use Percentage Distribution for the Jones Falls Watershed..... 6
Table 2: Summary of EOF Erosion Rate Calculations 9
Table 3: Jones Falls Baseline Sediment Loads (ton/yr)..... 13
Table 4: Detailed Baseline Sediment Budget Loads Within the Jones Falls Watershed. 13
Table 5: Monitoring Stations in the Jones Falls Watershed 17
Table 6: Jones Falls Core/Trend Data..... 19
Table 7: Jones Falls Baseline Load and TMDL..... 27
Table 8: Jones Falls TMDL Reductions by Source Category..... 28
Table 9: Jones Falls Watershed Average Annual TMDL of Sediment/TSS (ton/yr) 30
Table 10: Jones Falls Maximum Daily Loads of Sediment/TSS (ton/day) 30
Table A-1: Reference Watersheds A1
Table B-1: Permit Summary B1
Table B-2: Individual Municipal Permit Data B2
Table B-3: General Mine Permit Data B3
Table B-4: Stormwater Permits[1] B4

List of Abbreviations

BIBI	Benthic Index of Biotic Integrity
BIP	Buffer Incentive Program
BMP	Best Management Practices
BSID	Biological Stressor Identification
CBP P5	Chesapeake Bay Program Phase 5
CV	Coefficient of Variation
CWA	Clean Water Act
DNR	Maryland Department of Natural Resources
EOF	Edge-of-Field
EOS	Edge-of-Stream
EPA	Environmental Protection Agency
EPT	Ephemeroptera, Plecoptera, and Trichoptera
EPSC	Environmental Permit Service Center
ESD	Environmental Site Design
ETM	Enhanced Thematic Mapper
FDC	Flow Duration Curve
FIBI	Fish Index of Biologic Integrity
GIS	Geographic Information System
HSPF	Hydrological Simulation Program – FORTRAN
IBI	Index of Biotic Integrity
LA	Load Allocation
MAL	Minimum Allowable IBI Limit
MBSS	Maryland Biological Stream Survey
MD 8-Digit	Maryland 8-digit Watershed
MDE	Maryland Department of the Environment
MDL	Maximum Daily Load
MGD	Millions of Gallons per Day
mg/l	Milligrams per liter
MOS	Margin of Safety
MS4	Municipal Separate Storm Sewer System

NPDES	National Pollutant Discharge Elimination System
NRCS	Natural Resource Conservation Service
NRI	Natural Resources Inventory
PCBs	Polychlorinated Biphenyls
PSU	Primary Sampling Unit
RESAC	Regional Earth Science Applications Center
TMDL	Total Maximum Daily Load
Ton/yr	Tons per Year
TSD	Technical Support Document
TSS	Total Suspended Solids
TM	Thematic Mapper
USGS	United Stated Geological Survey
WLA	Waste Load Allocation
WQA	Water Quality Analysis
WQIA	Water Quality Improvement Act
WQLS	Water Quality Limited Segment
WWTP	Wastewater Treatment Plant

EXECUTIVE SUMMARY

This document, upon approval by the U.S. Environmental Protection Agency (EPA), establishes a Total Maximum Daily Load (TMDL) for sediment in the Jones Falls watershed (basin number 02131904) (2008 *Integrated Report of Surface Water Quality in Maryland Assessment Unit ID*: MD-02130904). Section 303(d) of the federal Clean Water Act (CWA) and the EPA's implementing regulations direct each state to identify and list waters, known as water quality limited segments (WQLSs), in which current required controls of a specified substance are inadequate to achieve water quality standards. For each WQLS, the State is required to either establish a TMDL of the specified substance that the waterbody can receive without violating water quality standards, or demonstrate that water quality standards are being met (CFR 2008b).

The Maryland Department of the Environment (MDE) has identified the waters of the Jones Falls watershed on the 2008 Integrated Report as impaired by metals (copper, zinc, and lead) (1996), nutrients – phosphorus (1996), sediments (1996), bacteria (2002), polychlorinated biphenyls (PCBs) - Lake Roland (2002), Chlordane – Lake Roland (1996) and impacts to biological communities (2006) (MDE 2008). The designated use of the Jones Falls mainstem and its tributaries above Lake Roland is Use III (Nontidal Cold Water). The designated use of the Jones Falls mainstem and its tributaries below Lake Roland is Use I (Water Contact Recreation and Protection of Warm Water Nontidal Aquatic Life), except for Stoney Run and its tributaries and the portion of the Jones Falls mainstem between North Avenue and Lake Roland, which are designated as Use IV (Recreational Trout Waters) (COMAR 2008a,b,c,d).

The TMDL established herein by MDE will address the 1996 sediments listing, for which a data solicitation was conducted, and all readily available data from the past five years have been considered. A Water Quality Analysis (WQA) for copper and lead was approved by the EPA in 2004, and a WQA for zinc was approved by the EPA in 2003. A TMDL for fecal bacteria was approved by the EPA in 2008, and a TMDL for chlordane was approved by EPA in 2001. A WQA for nutrients to address the phosphorus listing is scheduled to be submitted to the EPA in 2009. The listings for PCBs and impacts to biological communities will be addressed separately at a future date.

The Jones Falls watershed aquatic health scores, consisting of the Benthic Index of Biotic Integrity (BIBI) and Fish Index of Biotic Integrity (FIBI), indicate that the biological metrics for the watershed exhibit a significant negative deviation from reference conditions based on Maryland's biocriteria listing methodology. The biocriteria listing methodology assesses the overall condition of Maryland's 8-digit (MD 8-digit) watersheds that have multiple sites with failing biological metrics by measuring the percentage of stream miles that are degraded, based on the BIBI and FIBI scores at these sites, and then calculating whether the percentage of degraded stream miles differs significantly from reference conditions (i.e., unimpaired watershed <10% stream miles degraded) (Roth et al. 2005; MDE 2008). The objective of the TMDL established herein is to ensure that there will be no sediment impacts affecting aquatic health, thereby establishing a sediment load that supports the Use I/III/IV designations for the Jones Falls watershed.

Currently in Maryland, there are no specific numeric criteria that quantify the impact of sediment on the aquatic health of nontidal stream systems. Therefore, to determine whether aquatic health is impacted by elevated sediment loads, MDE's recently developed *Biological Stressor Identification* (BSID) methodology was applied. The BSID identifies the most probable cause(s) for observed biological impairments throughout MD's 8-digit watersheds by ranking the likely stressors affecting a watershed using a suite of available physical, chemical, and land use data. The ranking of stressors was conducted via a risk-based, systematic, weight-of-evidence approach. The risk-based approach estimates the strength of association between various stressors and a degraded biological community. The BSID analysis then identifies individual stressors (pollutants) as probable or unlikely causes of the poor biological conditions within a given MD 8-digit watershed and subsequently concludes whether or not these individual stressors or groups of stressors are contributing to the impairment (MDE 2009a).

The BSID analysis for the Jones Falls watershed concludes that biological communities are likely impaired due to flow/sediment related stressors. Five individual stressors (channelization, channel alteration, poor epifaunal substrate, poor bank stability, and high embeddedness) that are associated with sediment related impacts and an altered hydrologic regime were identified as being probable causes of the biological impairment. Furthermore, the degradation of biological communities in the watershed is strongly associated with urban land use and its concomitant effects: altered hydrology, sediment related impacts, and elevated levels of sulfate, chlorides, and conductivity (a measure of the presence of dissolved substances) (MDE 2009b).

In order to quantify the impact of sediment on the aquatic health of non-tidal stream systems, a reference watershed TMDL approach was used and resulted in the establishment of a *sediment loading threshold* (Currey et al. 2006). This threshold is based on a detailed analysis of sediment loads from watersheds that are identified as supporting aquatic life (i.e., reference watersheds) based on Maryland's biocriteria (Roth et al. 1998, 2000; Stribling et al. 1998; MDE 2008). This threshold is then used to determine a watershed specific sediment TMDL.

The computational framework chosen for the Jones Falls watershed TMDL was the Chesapeake Bay Program Phase 5 (CBP P5) watershed model target *edge-of-field* (EOF) land use sediment loading rate calculations combined with a *sediment delivery ratio*. The *edge-of-stream* (EOS) sediment load is calculated per land use as a product of the land use area, land use target loading rate, and loss from the EOF to the main channel. The spatial domain of the CBP P5 watershed model segmentation aggregates to the MD 8-digit watersheds, which is consistent with the impairment listing.

EPA's regulations require TMDLs to take into account seasonality and critical conditions for stream flow, loading, and water quality parameters (CFR 2008b). The intent of this requirement is to ensure that the water quality of the waterbody is protected during times when it is most vulnerable. The biological monitoring data used to determine the reference watersheds integrates the stress effects over the course of time and thus inherently addresses critical conditions. Seasonality is captured in two components. First,

it is implicitly included in biological sampling. Second, the Maryland Biological Stream Survey (MBSS) dataset included benthic sampling in the spring and fish sampling in the summer.

All TMDLs need to be presented as a sum of waste load allocations (WLAs) for point sources and load allocations (LAs) for nonpoint sources generated within the assessment unit, natural background, tributary, and adjacent segment loads. Furthermore, all TMDLs must include a margin of safety (MOS) to account for any lack of knowledge and uncertainty concerning the relationship between loads and water quality (CFR 2008a,b). It is proposed that the estimated variability around the reference watershed group used in this analysis already accounts for such uncertainty, and therefore the MOS is implicitly included.

The Jones Falls Total Baseline Sediment Load is 9,104.9 tons per year (ton/yr), which can be further subdivided into a nonpoint source baseline load (Nonpoint Source BL_{JF}) and two types of point source baseline loads: National Pollutant Discharge Elimination System (NPDES) regulated stormwater (NPDES Stormwater BL_{JF}) and regulated process water (Process Water BL_{JF}) (see Table ES-1).

Table ES-1: Jones Falls Baseline Sediment Loads (ton/yr)

Total Baseline Load (ton/yr)	=	Nonpoint Source BL_{JF}	+	NPDES Stormwater BL_{JF}	+	Process Water BL_{JF}
9,104.9	=	1,022.0	+	8,080.5	+	2.4

The Jones Falls Average Annual TMDL of Sediment/Total Suspended Solids (TSS) is 7,109.3 tons per year. The Load Allocation (LA_{JF}) is 1,022.0 tons per year, the NPDES Stormwater Waste Load Allocation (NPDES Stormwater WLA_{JF}) is 6,084.9 tons per year, and the Process Water Waste Load Allocation (Process Water WLA_{JF}) is 2.4 tons per year (see Table ES-2). This TMDL will ensure that the sediment loads and resulting effects are at a level to support the Use I/III/IV designations for the Jones Falls watershed, and more specifically, at a level the watershed can sustain without causing any sediment related impacts to aquatic health. The TMDL, however, will not completely resolve the impairment to biological communities within the watershed. Since the BSID watershed analysis identifies other possible stressors (i.e., chlorides, sulfate, conductivity) as impacting the biological conditions, this impairment remains to be fully addressed through the Integrated Report listing process and the TMDL development process, such that all impairing substances identified as impacting biological communities in the watershed are reduced to levels that will meet water quality standards, as established in future TMDLs for those substances (MDE 2009a).

Table ES-2: Jones Falls Average Annual TMDL of Sediment/Total Suspended Solids (ton/yr)

TMDL (ton/yr)	=	LA_{JF}	+	NPDES Stormwater WLA_{JF}	+	Process Water WLA_{JF}	+	MOS
7,109.3	=	1,022.0	+	6,084.9	+	2.4	+	Implicit

Table ES-3: Jones Falls Baseline Load, TMDL, and Total Reduction Percentage

Baseline Load (ton/yr)	TMDL (ton/yr)	Total Reduction (%)
9,104.9	7,109.3	21.9

In addition to the TMDL value, a Maximum Daily Load (MDL) is also presented in this document. The calculation of the MDL, which is derived from the TMDL average annual loads, is explained in Appendix C and presented in Table C-1.

Once the EPA has approved this TMDL, and it is known what measures must be taken to reduce pollution levels, implementation of best management practices (BMPs) is expected to take place primarily via the municipal separate storm sewer system (MS4) permitting process for medium and large municipalities. MDE intends for the required reduction to be implemented in an iterative process that first addresses those sources with the largest impact to water quality, with consideration given to ease and cost of implementation.

Maryland has several well-established programs to draw upon, including the Water Quality Improvement Act of 1998 (WQIA) and the Federal Nonpoint Source Management Program (§ 319 of the Clean Water Act). Several potential funding sources available for local governments for implementation are available, such as the Buffer Incentive Program (BIP), the State Water Quality Revolving Loan Fund, and the Stormwater Pollution Cost Share Program.

1.0 INTRODUCTION

This document, upon approval by the U.S. Environmental Protection Agency (EPA), establishes a Total Maximum Daily Load (TMDL) for sediment in the Jones Falls watershed (basin number 02131904) (2008 *Integrated Report of Surface Water Quality in Maryland* Assessment Unit ID: MD-02130904). Section 303(d)(1)(C) of the federal Clean Water Act (CWA) and the EPA's implementing regulations direct each state to develop a TMDL for each impaired water quality limited segment (WQLS) on the State's Integrated Report, taking into account seasonal variations, critical conditions, and a protective margin of safety (MOS) to account for uncertainty (CFR 2008b). A TMDL reflects the total pollutant loading of the impairing substance a waterbody can receive and still meet water quality standards.

TMDLs are established to determine the pollutant load reductions needed to achieve and maintain water quality standards. A water quality standard is the combination of a designated use for a particular body of water and the water quality criteria designed to protect that use. Designated uses include activities such as swimming, drinking water supply, protection of aquatic life, and shellfish propagation and harvest. Water quality criteria consist of narrative statements and numeric values designed to protect the designated uses. Criteria may differ among waters with different designated uses.

The Maryland Department of the Environment (MDE) has identified the waters of the Jones Falls watershed on the 2008 Integrated Report as impaired by metals (copper, zinc, and lead) (1996), nutrients – phosphorus (1996), sediments (1996), bacteria (2002), polychlorinated biphenyls (PCBs) - Lake Roland (2002), Chlordane – Lake Roland (1996) and impacts to biological communities (2006) (MDE 2008). The designated use of the Jones Falls mainstem and its tributaries above Lake Roland is Use III (Nontidal Cold Water). The designated use of the Jones Falls mainstem and its tributaries below Lake Roland is Use I (Water Contact Recreation and Protection of Warm Water Nontidal Aquatic Life), except for Stoney Run and its tributaries and the portion of the Jones Falls mainstem between North Avenue and Lake Roland, which are designated as Use IV (Recreational Trout Waters) (COMAR 2008a,b,c,d).

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The objective of the TMDL established herein is to ensure that there will be no sediment impacts affecting aquatic health, thereby establishing a sediment load that supports the Use I/III/IV designations for the Jones Falls watershed. Currently in Maryland, there are no specific numeric criteria that quantify the impact of sediment on the aquatic health of nontidal stream systems. Therefore, to determine whether aquatic health is impacted by

elevated sediment loads, MDE's recently developed *Biological Stressor Identification* (BSID) methodology was applied.

The BSID identifies the most probable cause(s) for observed biological impairments throughout Maryland's 8-digit (MD 8-digit) watersheds by ranking the likely stressors affecting a watershed using a suite of available physical, chemical, and land use data. The ranking of stressors was conducted via a risk-based, systematic, weight-of-evidence approach. The risk-based approach estimates the strength of association between various stressors and a degraded biological community. The BSID analysis then identifies individual stressors (pollutants) as probable or unlikely causes of the poor biological conditions within a given MD 8-digit watershed and subsequently concludes whether or not these individual stressors or groups of stressors are contributing to the impairment (MDE 2009a).

In order to quantify the impact of sediment on the aquatic health of non-tidal stream systems, a reference watershed TMDL approach was used and resulted in the establishment of a *sediment loading threshold* (Currey et al. 2006). This threshold is based on a detailed analysis of sediment loads from watersheds that are identified as supporting aquatic life (i.e., reference watersheds) based on Maryland's biocriteria (Roth et al. 1998, 2000; Stribling et al. 1998; MDE 2008). This threshold is then used to determine a watershed specific sediment TMDL.

2.0 SETTING AND WATER QUALITY DESCRIPTION

2.1 General Setting

Location

The Jones Falls is a free flowing stream that originates in Baltimore County, Maryland and flows 18 miles in a southeastern direction intul it empties into the tidal Patapsco River. The watershed is located in the Patapsco River sub-basin of the Chesapeake Bay watershed within Baltimore County and Baltimore City, and covers approximately 58 square miles (see Figure 1). An impoundment is located at Lake Roland, just north of the Baltimore County/City boundary. Several tributaries drain to the Jones Falls mainstem, including Moores Branch, Roland Run, Towson Run, Western Run, and Stoney Run. There are no "high quality", or Tier II, stream segments (Benthic Index of Biotic Integrity (BIB)/Fish Index of Biotic Integrity (FIBI) aquatic health scores > 4 (scale 1 – 5)) located within the watershed requiring the implementation of Maryland's antidegradation policy. Also, approximately 0.3% of the watershed is covered by water (i.e., streams, ponds, etc.). The total population in the Jones Falls watershed is approximately 309,000 (US Census Buerau 2000).

Geology/Soils

The Jones Falls watershed lies within the Piedmont and Atlantic Coastal Plain geologic provinces of central Maryland. The Piedmont province is characterized by gentle to steep rolling topography, low hills, and ridges (DNR 2008; MGS 2008; MDE 2000). The surficial geology is characterized by crystalline rocks of volcanic origin consisting of schist and gneiss. These formations are resistant to short term erosion and often determine the limits of stream bank and streambed. The formations decrease in elevation from northwest to southeast and eventually extend beneath the younger sediments of the Coastal Plain. The fall line represents the transition between the Atlantic Coastal Plain province and the Piedmont province. The Atlantic Coastal Plain surficial geology is characterized by thick, unconsolidated marine sediments deposited over the crystalline rock of the piedmont province. The deposits include clays, silts, sands, and gravels. The surface elevations range from approximately 680 feet to sea level at the head of tide. Stream channels of the sub-watersheds are well incised in the Eastern Piedmont, and exhibit relatively straight reaches and sharp bends, reflecting their tendency to following zones of fractured or weathered rock. The stream channels broaden abruptly as they flow down across the fall line into the soft, flat Coastal Plain sediments (CES 1995).

Above the Baltimore City/County boundary, the Jones Falls watershed lies predominantly in the Baile soil series. Soils in this series are very deep, poorly drained, exhibit slow to moderately slow permeability, and occur on upland depressions and slopes. The secondary soil series in the Baltimore County area of the watershed is the Hatboro soil series, which has similar characteristics as the Baile soil series and is often found in flood plains (USDA 1977).

In Baltimore City the primary soil series is the Lehigh series. This series is characterized by deep and somewhat poorly drained soil with slow permeability. The secondary soil

series present in the lower Jones Falls watershed is the Beltsville soil series, which is distinguished by being moderately well drained and often found in upland regions of the coastal plain geologic province (USDA 1998).

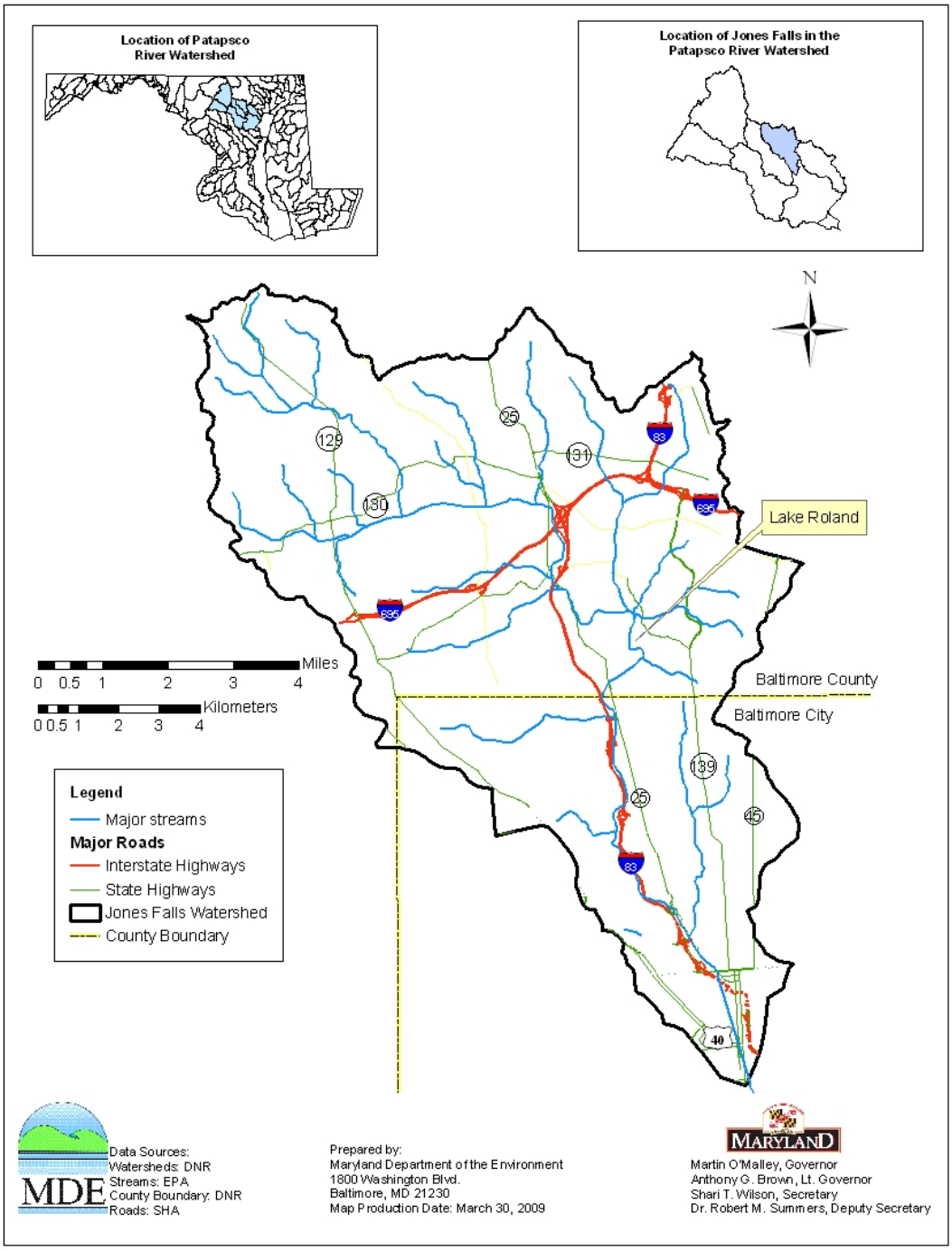

Figure 1: Location Map of the Jones Falls Watershed in Baltimore City and Baltimore County, Maryland

2.1.1. Land Use

Land Use Methodology

The land use framework used to develop this TMDL was originally developed for the Chesapeake Bay Program Phase 5 (CBP P5) watershed model.[1] The CBP P5 land use Geographic Information System (GIS) framework was based on two distinct layers of development. The first GIS layer was developed by the Regional Earth Science Applications Center (RESAC) at the University of Maryland and was based on satellite imagery (Landsat 7-Enhanced Thematic Mapper (ETM) and 5-Thematic Mapper (TM)) (Goetz et al. 2004). This layer did not provide the required level of accuracy that is especially important when developing agricultural land uses. In order to develop accurate agricultural land use calculations, the CBP P5 used county level U.S. Agricultural Census data as a second layer (USDA 1982, 1987, 1992, 1997, 2002).

Given that land cover classifications based on satellite imagery are likely to be least accurate at edges (i.e., boundaries between covers), the RESAC land uses bordering agricultural areas were analyzed separately. If the agricultural census data accounted for more agricultural use than the RESAC's data, appropriate acres were added to agricultural land uses from non-agricultural land uses. Similarly, if census agricultural land estimates were smaller than RESAC's, appropriate acres were added to non-agricultural land uses.

Adjustments were also made to the RESAC land cover to determine developed land uses. RESAC land cover was originally based on the United States Geological Survey (USGS) protocols used to develop the 2000 National Land Cover Database. The only difference between the RESAC and USGS approaches was RESAC's use of town boundaries and road densities to determine urban land covered by trees or grasses. This approach greatly improved the accuracy of the identified urban land uses, but led to the misclassification of some land adjacent to roads and highways as developed land. This was corrected by subsequent analysis. To ensure that the model accurately represented development over the simulation period, post-processing techniques that reflected changes in urban land use have been applied.

The result of this approach is that CBP P5 land use does not exist in a single GIS coverage; instead it is only available in a tabular format. The CBP P5 watershed model is comprised of 25 land uses. Most of these land uses are differentiated only by their nitrogen and phosphorus loading rates. The land uses are divided into 14 classes with distinct sediment erosion rates. Table 1 lists the CBP P5 generalized land uses, detailed land uses, which are classified by their erosion rates, and the acres of each land use in the Jones Falls watershed. Details of the land use development methodology have been summarized in the report entitled *Chesapeake Bay Phase 5 Community Watershed Model* (US EPA 2008).

[1] The EPA Chesapeake Bay Program developed the first watershed model in 1982. There have been many upgrades since the first phase of this model. The CBP P5 was developed to estimate flow, nutrient, and sediment loads to the Bay.

Jones Falls Watershed Land Use Distribution

The Jones Falls watershed consists primarily of urban land use (73.9%), with a small amount of forest land use (22.5%). There are also very small amounts of crop (2.7%) and pasture (0.9%). A detailed summary of the watershed land use areas is presented in Table 1, and a land use map is provided in Figure 2.

Table 1: Land Use Percentage Distribution for the Jones Falls Watershed

General Land Use	Detailed Land Use	Area (Acres)	Percent	Grouped Percent of Total
Crop	Animal Feeding Operations	22.4	0.1	
	Hay	284.6	0.8	
	High Till	165.3	0.4	
	Low Till	539.4	1.5	
	Nursery	1.3	0.0	2.7
Extractive	Extractive	14.2	0.0	0.0
Forest	Forest	8,270.4	22.2	
	Harvested Forest	83.5	0.2	22.5
Pasture	Pasture	334.8	0.9	
	Trampled_Pasture	0.9	0.0	0.9
Urban	Urban: Barren (Construction)	91.8	0.2	
	Urban: Impervious	7,496.0	20.2	
	Urban: Pervious	19,886.1	53.5	73.9
Total		37,190.6	100.0	100.0

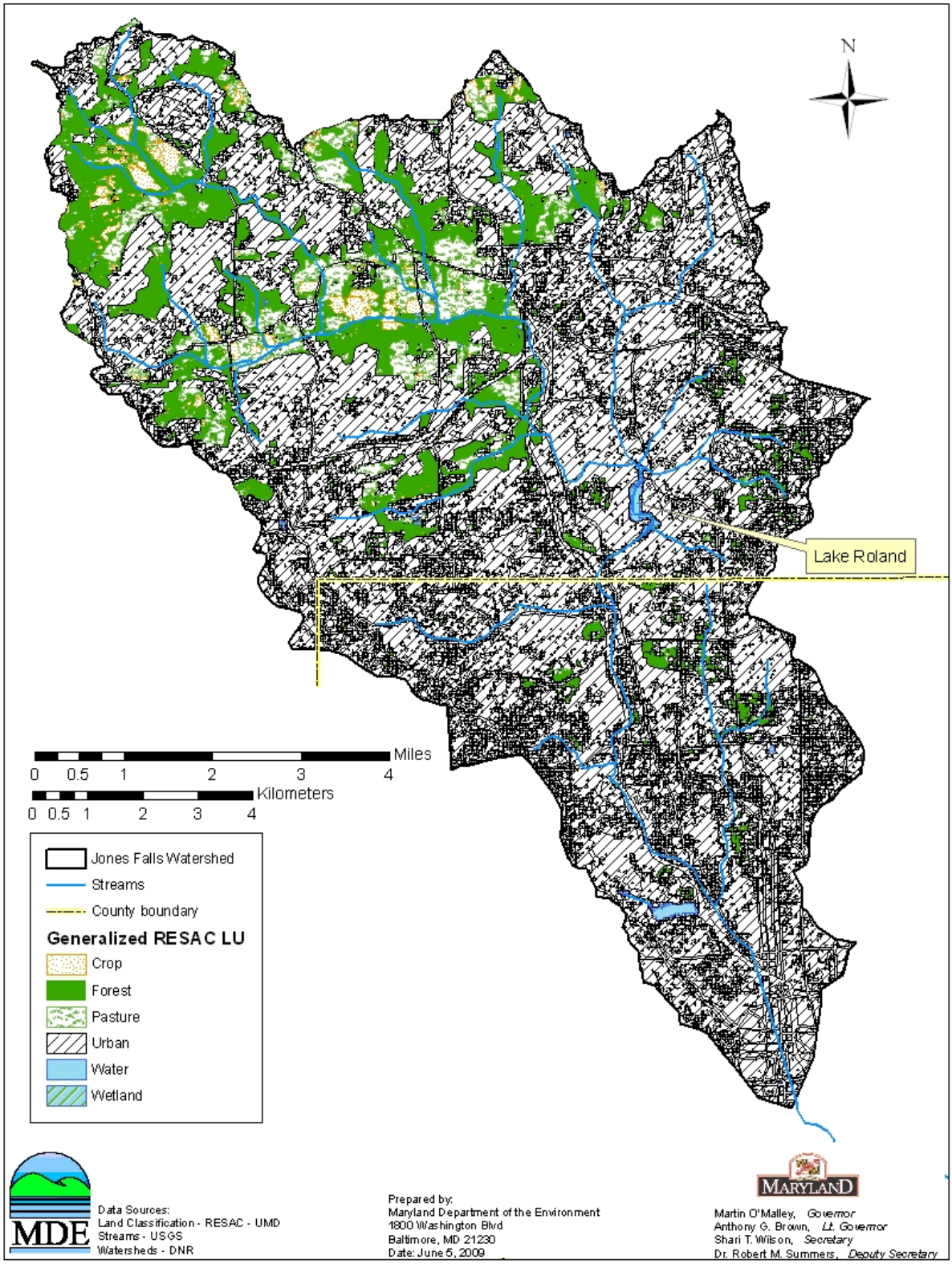

Figure 2: Land Use of the Jones Falls Watershed

2.2 Source Assessment

The Jones Falls Watershed Total Baseline Sediment Load can be subdivided into nonpoint and point source loads. This section summarizes the methods used to derive each of these distinct source categories.

2.2.1 Nonpoint Source Assessment

In this document, the nonpoint source loads account for sediment loads from unregulated stormwater runoff within the Jones Falls watershed. This section provides the background and methods for determining the nonpoint source baseline loads generated within the Jones Falls watershed (Nonpoint Source BL_{JF}).

General load estimation methodology

Nonpoint source sediment loads generated within the Jones Falls watershed are estimated based on the *edge-of-stream (EOS) calibration target loading rates* from the CBP P5 model. This approach is based on the fact that not all of the *edge-of-field* (EOF) sediment load is delivered to the stream or river (some of it is stored on fields down slope, at the foot of hillsides, or in smaller rivers or streams that are not represented in the model). To calculate the actual EOS loads, a *sediment delivery ratio* (the ratio of sediment reaching a basin outlet compared to the total erosion within the basin) is used. Details of the methods used to calculate sediment load have been summarized in the report entitled *Chesapeake Bay Phase 5 Community Watershed Model* (US EPA 2008).

Edge-of-Field Target Erosion Rate Methodology

EOF target erosion rates for agricultural land uses and forested land use were based on erosion rates determined by the Natural Resource Inventory (NRI). NRI is a statistical survey of land use and natural resource conditions conducted by the Natural Resources Conservation Service (NRCS) (USDA 2006). Sampling methodology is explained by Nusser and Goebel (1997).

Estimates of average annual erosion rates for pasture and cropland are available on a county basis at five-year intervals, starting in 1982. Erosion rates for forested land uses are not available on a county basis from NRI; however, for the purpose of the CBP Phase 2 watershed model, NRI calculated average annual erosion rates for forested land use on a watershed basis. These rates are still being used as targets in the CBP P5 model.

The average value of the 1982 and 1987 surveys was used as the basis for EOF target loads. The erosion rates from this period do not reflect best management practices (BMPs) or other soil conservation policies introduced in the wake of the effort to restore the Chesapeake Bay. To compensate for this, a BMP factor was included in the loading estimates using best available “draft” information from the CBP P5. Rates for urban pervious, urban impervious, and barren land were based on a combination of best professional judgment, literature analysis, and regression analysis. Table 2 lists erosion rates specific to the Jones Falls watershed.

Table 2: Summary of EOF Erosion Rate Calculations

Land Use	Data Source	Baltimore County (tons/acre/year)	Baltimore City (tons/acre/year)
Forest	Phase 2 NRI	0.46	0.46
Harvested Forest[1]	Average Phase 2 NRI (x 10)	3	3
Natural Grass	Average NRI Pasture (1982-1987)	1.5	1.5
Pasture	Pasture NRI (1982-1987)	1.29	1.29
Trampled pasture[2]	Pasture NRI (x 9.5)	12.26	12.26
Animal Feeding Operations[2]	Pasture NRI (x 9.5)	12.26	12.26
Hay[2]	Crop NRI (1982-1987) (x 0.32)	3.18	3.18
High Till Without Manure[2]	Crop NRI (1982-1987) (x 1.25)	12.42	12.42
High Till With manure[2]	Crop NRI (1982-1987) (x 1.25)	12.42	12.42
Low till With Manure[2]	Crop NRI (1982-1987) (x 0.75)	7.45	7.45
Pervious Urban	Intercept Regression Analysis	0.74	0.74
Extractive	Best professional judgment	10	10
Barren	Literature survey	20	20
Impervious	100% Impervious Regression Analysis	5.18	5.18

Notes: [1]Based on an average of NRI values for the Chesapeake Bay Phase 5 segments.
[2]NRI score data adjusted based on land use.

Sediment Delivery Ratio: The base formula for calculating *sediment delivery ratio*s in the CBP P5 model is the same as the formula used by the NRCS (USDA 1983).

$$DF = 0.417762 * A^{-0.134958} - 0.127097 \qquad \text{(Equation 2.1)}$$

where
DF (delivery factor) = the sediment delivery ratio
A = drainage area in square miles

In order to account for the changes in sediment loads due to distance traveled to the stream, the CBP P5 model uses the *sediment delivery ratio*. Land use specific *sediment delivery ratio*s were calculated for each river segment using the following procedure:

(1) mean distance of each land use from the river reach was calculated;

(2) *sediment delivery ratio*s for each land use were calculated (drainage area in Equation 2.1 was assumed to be equal to the area of a circle with radius equal to the mean distance between the land use and the river reach).

Edge-of-Stream Loads

Edge-of-stream loads are the loads that actually enter the river reaches (i.e., the mainstem of a watershed). Such loads represent not only the erosion from the land but all of the intervening processes of deposition on hillsides and sediment transport through smaller rivers and streams.

Streambank Erosion

Many studies have documented the relationship between high amounts of connected impervious surfaces, increases in storm flows, and stream degradation in the form of streambank erosion (Schueler 1994; Arnold and Gibbons 1996). In many urbanized watersheds, small stream channels have been replaced by sewer pipes. As a result, impervious surfaces such as rooftops, parking lots, and road surfaces are now directly connected to the main stream channel via the storm sewer system. During a storm event, this causes a greater amount of precipitation to flow more rapidly into a given stream channel once it reaches the surface. Furthermore, less water infiltrates into the ground both during and after a storm event, thereby limiting the amount of groundwater recharge to a stream. This altered urban hydrology typically causes abnormally high flows in streams during storms and abnormally low flows during dry periods. The high flows occurring during storm events increase sheer stress and cause excessive erosion of streambanks and streambeds, which leads to degraded stream channel conditions for biological communities (MDE 2007).

Two methods of estimating streambank erosion were presented in the *Total Maximum Daily Loads of Sediment/Total Suspended Solids for the Anacostia River Basin, Montgomery and Prince George's Counties, Maryland and The District of Columbia*. The first estimate uses the Anacostia Hydrological Simulation Program – FORTRAN (HSPF) watershed model in conjunction with the Penn State University streambank

erosion equation (Evans et al. 2003). The analysis estimated that approximately 73% of the total annual sediment load within the Anacostia River watershed could be attributed to streambank erosion (MDE 2007).

The second method analyzes the long term relationship between flow and total suspended solids (TSS) concentrations to quantify the effects of an altered urban hydrology on watershed sediment loads. Changes in hydrology in the Anacostia River watershed were characterized using daily flow data from the USGS gage stations. The long-term changes over time in the flow duration curves (FDCs) for each of these stations was quantified using a type of statistical analysis known as "quantile regression." The portion of the FDC representing the highest flows was determined to have increased significantly over time, consistent with hydrologic alteration from increased impervious surfaces. Also, a "sediment rating curve" (i.e., the relationship between suspended sediment concentration and flow) was computed and combined with the FDCs to estimate annual sediment loads before and after increased development (i.e., altered hydrology). The results of the analysis indicate that approximately 75% of the total annual sediment load in the Anacostia River watershed is due to alterations in hydrology (MDE 2007).

Using CBP P5 urban sediment EOF target values, MDE developed a formula for estimating the percent of erosional sediment resultant from streambank erosion (i.e., that portion of the total urban sediment load attributed to stream bank erosion) based on the amount of impervious land within a watershed. The equation uses the urban sediment loading factors to estimate the proportion of the urban sediment load from stream bank erosion. The assumption is that as impervious surfaces increase, the upland sources decrease, flow increases, and the change in sediment load results from increased streambank erosion. While this formula only represents an empirical approximation, it is consistent with results from the Anacostia River Sediment TMDL and recognizes that stream bank erosion can be a significant portion of the total sediment load. The formula is as follows:

$$\%E = \frac{I * L_I}{I * L_I + (1 - I)L_P} \qquad \text{(Equation 2.2)}$$

where:
% E = percent erosional sediment resultant from streambank erosion
I = percent impervious
L_I = Impervious urban land use EOF load
L_P = Pervious urban land use EOF load

The relationship demonstrated in equation 2.2 is expressed graphically in Figure 3. Using the equation, the Anacostia River watershed (23% impervious) would equate to approximately a 68% erosional sediment load resultant from streambank erosion. Per Table 1, approximately 20% of the Jones Falls watershed is covered by impervious surfaces. This would equate to approximately a 64% erosional sediment load resultant from streambank erosion.

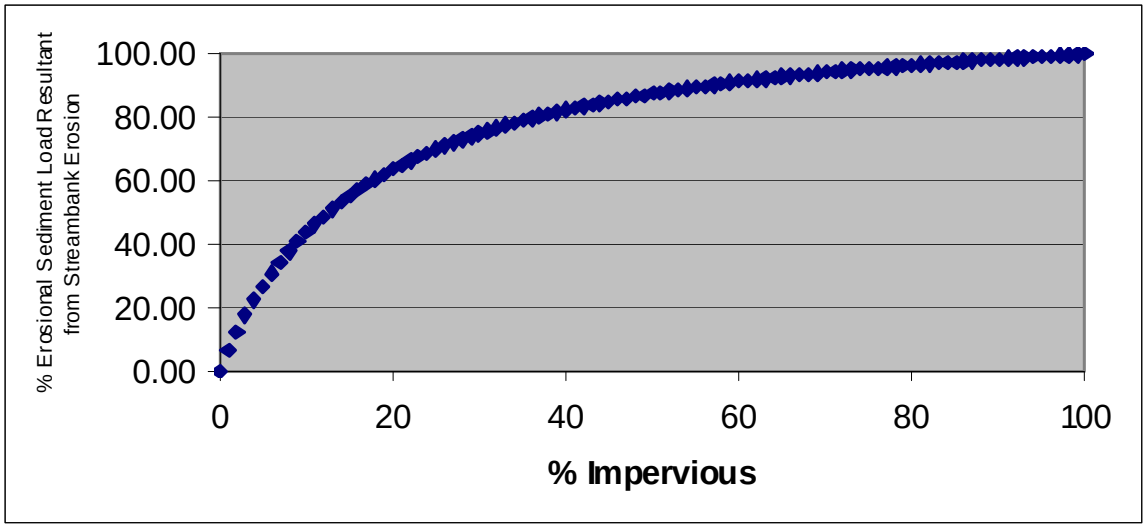

Figure 3: Percent Impervious vs. Percent Erosional Sediment Load Resultant from Streambank Erosion

For this TMDL, erosional sediment resultant from streambank erosion represents an aggregate load within the total urban impervious EOF loads as described in the report *Chesapeake Bay Phase V Community Watershed Model* (US EPA 2008) and is not explicitly reported.

2.2.2 Point Source Assessment

A list of 23 active permitted point sources that contribute to the sediment load in the Jones Falls watershed was compiled using MDE's Environmental Permit Service Center (EPSC) database. The types of permits identified individual municipal, individual municipal separate storm sewer systems (MS4s), general mineral mining, general industrial stormwater, and general MS4s. The permits can be grouped into two categories, process water and stormwater. The process water category includes those loads generated by continuous discharge sources whose permits have TSS limits. The stormwater category includes all National Pollutant Discharge Elimination System (NPDES) regulated stormwater discharges. Other permits that do not meet these conditions are considered *de minimis* in terms of the total sediment load.

The sediment loads for the 2 process water permits (Process Water BL_{JF}) are calculated based on their TSS limits and corresponding flow information. The 21 NPDES Phase I or Phase II stormwater permits identified throughout the Jones Falls watershed are regulated based on BMPs and do not include TSS limits. In the absence of TSS limits, the NPDES regulated stormwater baseline load (NPDES Stormwater BL_{JF}) is calculated using methods described in Section 2.2.1 and watershed specific urban land use sediment delivery factors. A detailed list of the permits appears in Appendix B.

2.2.3 Summary of Baseline Loads

Table 3 summarizes the Jones Falls Baseline Sediment Load, reported in tons per year (ton/yr) and presented in terms of nonpoint and point source loadings.

Table 3: Jones Falls Baseline Sediment Loads (ton/yr)

Total Baseline Load (ton/yr)	=	**Nonpoint Source BL_{GF}**	+	**NPDES Stormwater BL_{GF}**	+	**Process Water BL_{GF}**
9,104.9	=	1,022.0	+	8,080.5	+	2.4

Table 4 presents a breakdown of the Jones Falls Total Baseline Sediment Load, detailing loads per land use. The largest portion of the sediment load is from urban land (89%). The remainder of the sediment load is from crop land (6%) and forest (4%), with small amounts from other land uses.

Table 4: Detailed Baseline Sediment Budget Loads Within the Jones Falls Watershed

General Land Use	**Description**	**Load (Ton/Yr)**	**Percent**	**Grouped Percent of Total**
Crop	Animal Feeding Operations	22.5	0.2	
	Hay	72.5	0.8	
	High Till	157.2	1.7	
	Low Till	322.0	3.5	
	Nursery	1.3	0.0	6.3
Extractive	Extractive	15.1	0.2	0.2
Forest	Forest	372.0	4.1	
	Harvested Forest	24.4	0.3	4.4
Pasture	Pasture	34.0	0.4	
	Trampled Pasture	1.1	0.0	0.4
Urban[1]	Urban: Barren (Construction)	89.8	1.0	
	Urban: Impervious	6148.0	67.5	
	Urban: Pervious	1842.7	20.2	88.7
	Process Water	2.4	0.03	0.03
	Total	9,104.9	100.0	100.0

Note: [1] The urban land use load represents the permitted stormwater load.

2.3 Water Quality Characterization

The Jones Falls watershed was originally listed on Maryland's 1996 303(d) List as impaired by elevated sediments from nonpoint sources, with supporting evidence cited in Maryland's 1996 305(b) report. The 1996 305(b) report did not directly state that elevated sediments were a concern, and it has been determined that the sediment listing was based on best professional judgment (MDE 2004; DNR 1996).

Currently in Maryland, there are no specific numeric criteria for suspended sediments. Therefore, to determine whether aquatic health is impacted by elevated sediment loads, MDE's recently developed biological stressor identification methodology was applied. The primary goal of the BSID analysis is to identify the most probable cause(s) for observed biological impairments throughout MD's 8-digit watersheds (MDE 2009a).

The BSID analysis applies a case-control, risk-based, weight-of-evidence approach to identify potential causes of biological impairment. The risk-based approach estimates the strength of association between various stressors and a degraded biological community. The BSID analysis then identifies individual stressors (pollutants) as probable or unlikely causes of the poor biological conditions within a given MD 8-digit watershed and subsequently reviews ecological plausibility/concludes whether or not these individual stressors or groups of stressors are contributing to the impairment (MDE 2009a).

The primary dataset for BSID analysis is round two Maryland Department of Natural Resources (DNR) Maryland Biological Stream Survey (MBSS) data (collected between 2000-2004) because it provides a broad spectrum of paired data variables, which allow for a more comprehensive stressor analysis. The MBSS is a robust statewide probability-based sampling survey for assessing the biological conditions of wadeable, non-tidal streams (Klauda et al. 1998; Roth et al. 2005). It uses a fixed length (75 m) randomly selected stream segment for collecting site level information within a primary sampling unit (PSU), also defined as a watershed. The randomly selected stream segments, from which field data are collected, are selected using either stratified random sampling with proportional allocation, or simple random sampling (Cochran 1977). The random sample design allows for unbiased estimates of overall watershed conditions. Thus, the dataset facilitated case-control analyses because 1) in-stream biological data are paired with chemical, physical, and land use data variables that could be identified as possible stressors and 2) it uses a probabilistic statewide monitoring design.

The BSID analysis groups the individual stressors (physical and chemical variables) into three generalized parameters in order to assess how the resulting impacts of these stressors can alter the biological community and structure. The three generalized parameters include: sediment, habitat, and water chemistry. Identification of a sediment/flow stressor as contributing to the biological impairment is based on the results of the individual stressor associations within both the sediment and habitat parameters that reveal the effects of sediment related impacts or an altered hydrologic regime (MDE 2009a).

In addition to the MBSS round two data applied within the BSID analysis, data from the Maryland DNR Core/Trend Program was also used for water quality characterization in the TMDL. The program collected benthic macroivertebrate data between 1976 and 2006. This data was used to calculate four benthic community measures: total number of taxa, the Shannon Weiner diversity index, the modified Hilsenhoff biotic integrity index, and percent Ephemeroptera, Plecoptera, and Trichoptera (EPT). DNR has extensive monitoring data for two stations on the mainstem of the Jones Falls through the Core/Trend program. One station is located at North Avenue and the other at Falls Road (See Figure 4 and table 5) (DNR 2007).

Jones Falls Watershed Monitoring Stations

A total of 24 water quality monitoring stations were used to characterize the Jones Falls Watershed. Twenty-two biological/physical habitat monitoring stations from the MBSS program round one and two data collection were used to characterize the Jones Falls Watershed in Maryland's 2008 Integrated Report. The BSID analysis used the 12 biological/physical habitat monitoring stations from the MBSS program round two data collection. Additionally, two biological monitoring stations from the Maryland Core/Trend monitoring network were applied within the TMDL analysis. All stations are presented in Figure 4 and listed in Table 5.

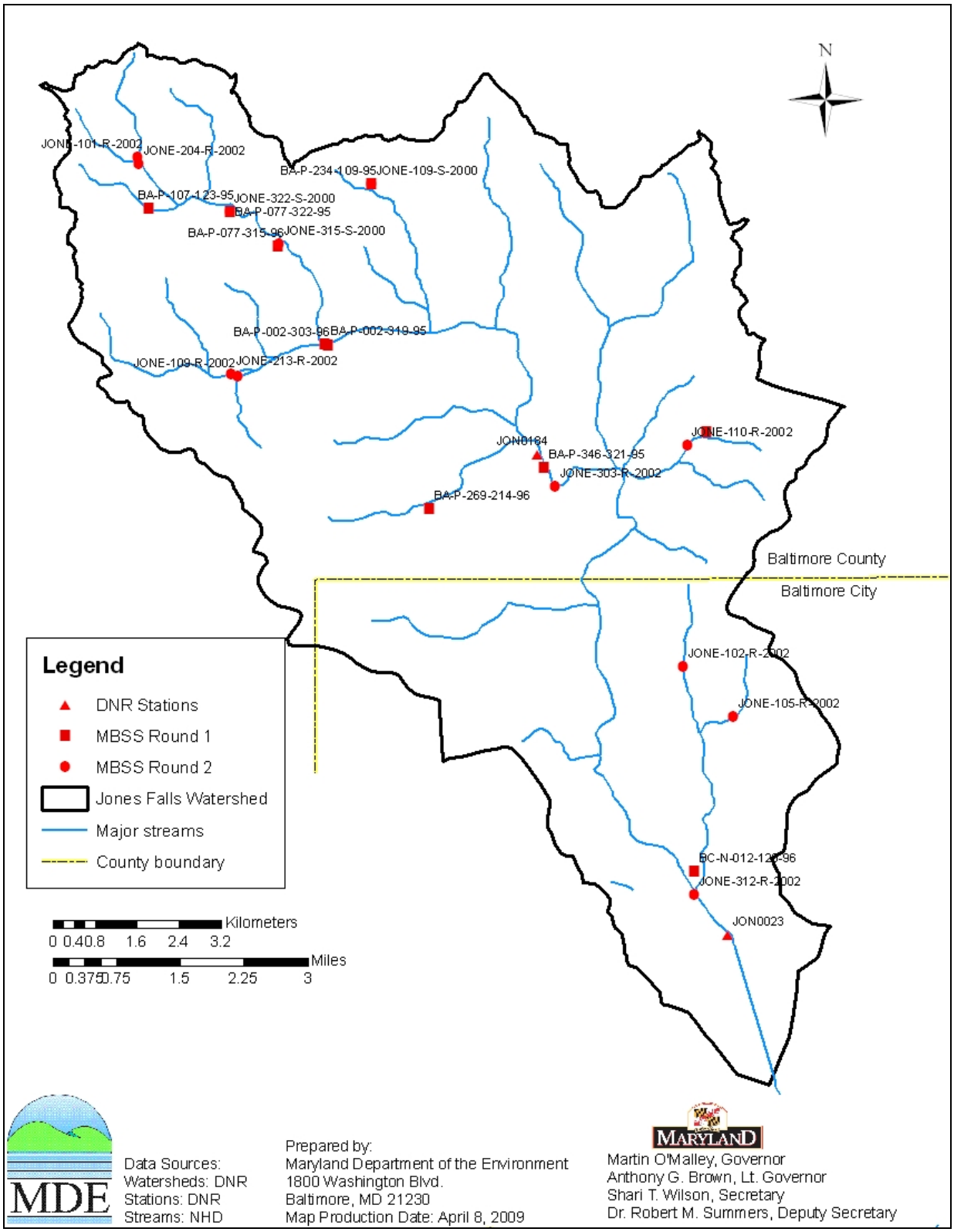

Figure 4: Monitoring Stations in the Jones Falls Watershed

Table 5: Monitoring Stations in the Jones Falls Watershed

Site Number	Sponsor	Site Type	Site Name	Latitude (dec degrees)	Longitude (dec degrees)
BA-P-002-303-96	MD DNR	MBSS, Round 1	JONES FALLS	39.4120	76.7080
BA-P-002-319-95	MD DNR	MBSS, Round 1	JONES FALLS	39.4122	76.7087
BA-P-074-106-96	MD DNR	MBSS, Round 1	TOWSON RUN UT1	39.3970	76.6250
BA-P-077-315-96	MD DNR	MBSS, Round 1	NORTH BR	39.4290	76.7190
BA-P-077-322-95	MD DNR	MBSS, Round 1	NORTH BR	39.4348	76.7296
BA-P-107-123-95	MD DNR	MBSS, Round 1	NORTH BR	39.4354	76.7475
BA-P-234-109-95	MD DNR	MBSS, Round 1	DIPPING POND RUN	39.4395	76.6984
BA-P-269-214-96	MD DNR	MBSS, Round 1	MOORE'S BR	39.3840	76.6860
BA-P-346-321-95	MD DNR	MBSS, Round 1	JONES FALLS	39.3910	76.6607
BC-N-012-120-96	MD DNR	MBSS, Round 1	STONY RUN	39.3220	76.6280
JONE-101-R-2002	MD DNR	MBSS, Round 2	NORTH BR UT 1_UT1	39.4442	76.7498
JONE-102-R-2002	MD DNR	MBSS, Round 2	STONY RUN	39.3569	76.6303
JONE-105-R-2002	MD DNR	MBSS, Round 2	STONY RUN UT	39.3483	76.6192
JONE-109-R-2002	MD DNR	MBSS, Round 2	JONES FALLS UT 1	39.4067	76.7280
JONE-109-S-2000	MD DNR	MBSS, Round 2	DIPPING POND RUN UT1	39.4395	76.6984
JONE-110-R-2002	MD DNR	MBSS, Round 2	TOWSON RUN	39.3947	76.6292
JONE-204-R-2002	MD DNR	MBSS, Round 2	NORTH BR UT 1	39.4431	76.7496
JONE-213-R-2002	MD DNR	MBSS, Round 2	JONES FALLS	39.4071	76.7294
JONE-303-R-2002	MD DNR	MBSS, Round 2	JONES FALLS	39.3879	76.6584
JONE-312-R-2002	MD DNR	MBSS, Round 2	JONES FALLS	39.3180	76.6282
JONE-315-S-2000	MD DNR	MBSS, Round 2	NORTH BR JONES FALLS	39.4293	76.7188
JONE-322-S-2000	MD DNR	MBSS, Round 2	NORTH BR JONES FALLS	39.4348	76.7296
JON0023	MD DNR	TREND	North Avenue	39.1840	76.3715
JON0184	MD DNR	CORE	Falls Road	39.2336	76.3944

2.4 Water Quality Impairment

The designated use of the Jones Falls mainstem and its tributaries above Lake Roland is Use III (Nontidal Cold Water). The designated use of the Jones Falls mainstem and its tributaries below Lake Roland is Use I (Water Contact Recreation and Protection of Warm Water Nontidal Aquatic Life), except for Stoney Run and its tributaries and the portion of the Jones Falls mainstem between North Avenue and Lake Roland, which are designated as Use IV (Recreational Trout Waters) (COMAR 2008a,b,c,d). The water quality impairment of the Jones Falls watershed addressed by this TMDL is caused by an elevated sediment load beyond a level that the watershed can sustain without causing any sediment related impacts to aquatic health, where aquatic health is based on benthic and fish Index of Biotic Integrity (IBI) scores, as demonstrated via the BSID analysis for the watershed.

The Jones Falls watershed is listed on Maryland's 2008 Integrated Report as impaired for impacts to biological communities. Greater than 36% of the stream miles in the Jones Falls watershed are assessed as having degraded biological conditions (when compared to regional reference indices). The biological impairment listing is based on the combined results of MBSS round one (1995-1997) and round two (2000-2004) data, which includes twenty-two stations. Eight of the twenty-two stations have degraded BIBI/FIBI scores significantly lower than 3.0 (MDE 2008). As mentioned in Section 2.3, however, only MBSS round 2 data were used in the BSID analysis. See Figure 4 and Table 5 for station locations and information.

The results of the BSID analysis for the Jones Falls watershed are presented in a report entitled *Watershed Report for Biological Impairment of the Jones Falls Watershed in Baltimore City and Baltimore County, Maryland Biological Stressor Identification Analysis Results and Interpretation* (MDE 2009b). The report states that the degradation of biological communities in the Jones Falls watershed is strongly associated with urban land use and its concomitant effects: altered hydrology, sediment related impacts, and elevated levels of sulfate, chlorides, and conductivity (a measure of the presence of dissolved substances).

The BSID analysis has determined that the biological impairment in the Jones Falls watershed is due in part to flow/sediment related stressors. Specifically, the analysis confirmed that individual stressors within the sediment and habitat parameter groupings were contributing to the biological impairment in the watershed. Also, the analysis identified the following stressors within the sediment and habitat parameter groupings as having a statistically significant association with impaired biological communities at the respective percentage of degraded sites: channelization (51%), channel alteration (marginal to poor: 59%; poor: 48%), epifaunal substrate (poor: 38%), poor bank stability index (35%), and high embeddedness (52%). Overall, sediment and flow stressors within the sediment and habitat parameter groupings were identified at approximately 93% and 95%, respectively, of the degraded sites throughout the watershed (MDE 2009b). Therefore, since sediment is identified as a stressor to the biological communities in the Jones Falls watershed, a TMDL is required.

As a supplement to the MBSS round two data used in the BSID analysis, the biological monitoring results from the two Maryland DNR Core/trend stations along the mainstem of the Jones Falls indicate that mainstem water quality can be classified as poor to fair/good based on percent EPT, taxa number, biotic index, and diversity index (see Table 6). Statistical analysis of the long term Core/Trend data indicates since 1977, that no change has occurred (DNR 2007). The poor water quality status for Station JON0023 is consistent with the results of the MBSS data at the nearby upstream station, JONE-312-R-2002. Additionally, the fair/good water quality status for Station JON0184 is consistent with the results of the MBSS data at the nearby downstream stations, BA-P-346-321-95 and JON-303-R-2002.

Table 6: Jones Falls Core/Trend Data

Site Number	Current Water Quality Status	Trend Since 1970's
JON0023	POOR	NO CHANGE
JON0184	FAIR/GOOD	NO CHANGE

3.0 TARGETED WATER QUALITY GOAL

The objective of the sediment TMDL established herein is to reduce sediment loads, and subsequent effects on aquatic health, in the Jones Falls watershed to levels that support the Use I/III/IV designations (Water contact recreation, and protection of Nontidal Warmwater Aquatic Life) (Nontidal Coldwater) (Recreational Trout Waters) (COMAR 2008a,b,c,d). Assessment of aquatic health is based on Maryland's biocriteria protocol, which evaluates both the amount and diversity of the benthic and fish community through the use of the IBI (Roth et al. 1998, 2000; Stribling et al. 1998; MDE 2008).

Reductions in sediment loads are expected to result from decreased watershed and streambed erosion, which will then lead to improved benthic and fish habitat conditions. Specifically, sediment load reductions are expected to result in an increase in the number of benthic sensitive species present, an increase in the available and suitable habitat for a benthic community, a possible decrease in fine sediment (fines), and improved stream habitat diversity, all of which will result in improved water quality.

The TMDL, however, will not completely resolve the impairment to biological communities within the watershed. Since the BSID watershed analysis identifies other possible stressors (i.e., chlorides, sulfate, conductivity) as impacting the biological conditions, this impairment remains to be fully addressed through the Integrated Report listing process and the TMDL development process, such that all impairing substances identified as impacting biological communities in the watershed are reduced to levels that will meet water quality standards, as established in future TMDLs for those substances (MDE 2009a).

4.0 TOTAL MAXIMUM DAILY LOADS AND SOURCE ALLOCATION

4.1 Overview

This section describes how the sediment TMDL and the corresponding allocations were developed for the Jones Falls watershed. Section 4.2 describes the analysis framework for estimating sediment loading rates and the assimilative capacity of the watershed stream system. Section 4.3 summarizes the scenarios that were used in the analysis and presents results. Section 4.4 discusses critical conditions and seasonality. Section 4.5 explains the calculations of TMDL loading caps. Section 4.6 details the load allocations, and Section 4.7 explains the rationale for the margin of safety. Finally, Section 4.8 summarizes the TMDL.

4.2 Analysis Framework

Since there are no specific numeric criteria that quantify the impact of sediment on the aquatic health of nontidal stream systems, a reference watershed approach will be used to establish the TMDL. Furthermore, as the BSID analysis established a link between biological impairment and sediment related stressors, the reference watershed approach will utilize a biological endpoint.

Watershed Model

The watershed model framework chosen for the Jones Falls watershed TMDL was the CBP P5 long-term average annual watershed model EOS loading rates. The spatial domain of the CBP P5 watershed model segmentation aggregates to the MD 8-digit watersheds, which is consistent with the impairment listing. The EOS loading rates were used because actual time variable CBP P5 calibration and scenario runs are currently being developed and are not yet available. These target-loading rates are used to calibrate the land use EOS loads within the CBP P5 model and thus should be consistent with future CBP modeling efforts.

The nonpoint source and NPDES stormwater baseline sediment loads generated within the Jones Falls watershed are calculated as the sum of corresponding land use EOS loads within the watershed and represent a long-term average loading rate. Individual land use EOS loads are calculated as a product of the land use area, land use target loading rate, and loss from the EOF to the main channel. The loss from the EOF to the main channel is the *sediment delivery ratio* and is defined as the ratio of the sediment load reaching a basin outlet to the total erosion within the basin. A *sediment delivery ratio* is estimated for each land use type based on the proximity of the land use to the main channel. Thus, as the distance to the main channel increases, more sediment is stored within the channels (i.e., *sediment delivery ratio* decreases). Details of the data sources for the unit loading rates can be found in Section 2.2 of this report.

The Jones Falls watershed was evaluated as one watershed TMDL segment (see Figure 5). This one TMDL segment consists of two CBP P5 segments, one in Baltimore County and one in Baltimore City.

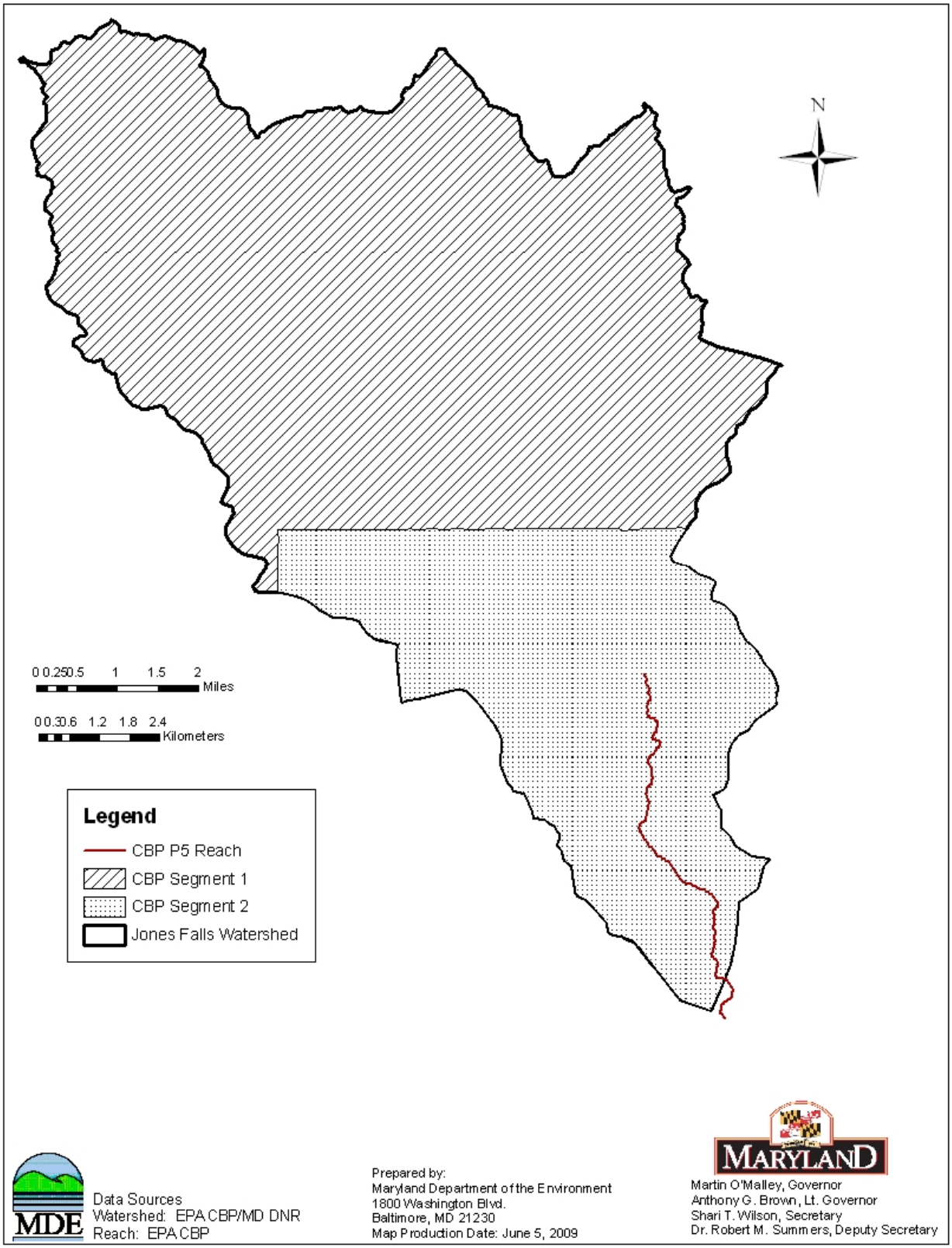

Figure 5: Jones Falls Watershed TMDL Segmentation

Reference Watershed Approach

Currently in Maryland, there are no specific numeric criteria that quantify the impact of sediment on the aquatic health of non-tidal stream systems. Therefore, in order to quantify the impact of sediment on the aquatic health of non-tidal stream systems, a reference watershed TMDL approach was used and resulted in the establishment of a *sediment loading threshold* for watersheds within the Highland and Piedmont physiographic regions (Currey et al. 2006). Reference watersheds were determined based on Maryland's biocriteria methodology. The biocriteria methodology assesses biological impairment at the 8-digit watershed scale based on the percentage of MBSS monitoring stations, translated into watershed stream miles, that are degraded. Individual monitoring station impairment is determined based on BIBI/FIBI scores lower than the Minimum Allowable IBI Limit (MAL), which is calculated based on the average annual allowable IBI value of 3.0 (on a scale of 1 to 5). Applying the MAL threshold helps avoid classification errors when assessing biological impairment (Roth et al. 1998, 2000; Stribling et al. 1998; MDE 2008).

Comparison of watershed sediment loads to loads from reference watersheds requires that the watersheds be similar in physical and hydrological characteristics. To satisfy this requirement, Currey et al. (2006) selected reference watersheds only from the Highland and Piedmont physiographic regions (see appendix A for the list of reference watersheds). This region is consistent with the non-coastal region that was identified in the 1998 development of FIBI and subsequently used in the development of BIBI (Roth et al. 1998; Stribling et al. 1998).

To reduce the effect of the variability within the Highland and Piedmont physiographic regions, the watershed sediment loads were then normalized by a constant background condition, the all forested watershed condition. This new normalized term, defined as the *forest normalized sediment load* (Y_n), represents how many times greater the current watershed sediment load is than the *all forested sediment load*. A similar approach was used by EPA Region 9 for sediment TMDLs in California (e.g., Navarro River or Trinity River TMDLs), where the loading capacity was based on an analysis of the amount of human-caused sediment delivery that can occur in addition to natural sediment delivery, without causing adverse impacts to aquatic life. The *forest normalized sediment load* for this TMDL is calculated as the current watershed sediment load divided by the *all forested sediment load*. The equation for the *forest normalized sediment load* is as follows:

$$Y_n = \frac{y_{ws}}{y_{for}} \qquad \text{(Equation 4.1)}$$

where:

Y_n = forest normalized sediment load
y_{ws} = current watershed sediment load (ton/yr)
y_{for} = all forested sediment load (ton/yr)

Nine reference watersheds were selected from the Highland/Piedmont region. Reference watershed *forest normalized sediment loads* were calculated using CBP P5 2000 land use in order to maintain consistency with MBSS sampling years. The median and 75th percentile of the reference watershed *forest normalized sediment loads* were calculated and found to be 3.3 and 4.2 respectively. These values are in close agreement with more complex methods used to determine the *sediment loading threshold* in previous nontidal sediment TMDLs. Therefore, the median value of 3.3 was established as the *sediment loading threshold* as an environmentally conservative approach to develop this TMDL (see Appendix A for more details).

The *forest normalized sediment load* for the Jones Falls watershed (estimated as 4.2) was calculated using CBP P5 2005 landuse, to best represent current conditions. A comparison of the Jones Falls watershed *forest normalized sediment load* to the *forest normalized reference sediment load* (also referred to as the *sediment loading threshold*) demonstrates that it exceeds the *sediment loading threshold*, indicating that it is receiving loads that are above the maximum allowable load that the watershed can sustain and still meet water quality standards.

4.3 Scenario Descriptions and Results

The following analyses allow a comparison of baseline conditions (under which water quality problems exist) with future conditions, which project the water quality response to various simulated sediment load reductions. The analyses are grouped according to baseline conditions and future conditions associated with TMDLs.

Baseline Conditions

The baseline conditions are intended to provide a point of reference by which to compare the future scenario that simulates conditions of a TMDL. The baseline conditions typically reflect an approximation of nonpoint source loads during the monitoring time frame, as well as estimated point source loads based on discharge data for the same period.

The Jones Falls watershed baseline sediment loads are estimated using the CBP P5 target EOS land use sediment loading rates with 2005 land use. Watershed loading calculations, based on the CBP P5 segmentation scheme, are represented by two CBP P5 model segments within the watershed. The sediment loads from these segments are combined to represent the baseline condition. The point source sediment loads are estimated based on the existing permit information. Details of these loading source estimates can be found in Section 2.2 and Appendix B of this report.

Future (TMDL) Conditions

This scenario represents the future conditions of maximum allowable sediment loads whereby there will be no sediment related impacts to aquatic health. In the TMDL calculation, the allowable load for the impaired watershed is calculated as the product of the *sediment loading threshold* (determined from watersheds with a healthy biological community) and the Jones Falls *all forested sediment load* (see Section 4.2). The resulting load is considered the maximum allowable load the watershed can sustain without causing any sediment related impacts to aquatic health.

The TMDL loading and associated reductions are averaged at the MD 8-digit watershed scale, which is consistent with the original listing scale. It is important to recognize that some subwatersheds may require higher reductions than others, depending on the distribution of the land use.

The formula for estimating the TMDL is as follows:

$$TMDL = \sum_{i=1}^{n} Yn_{ref} \cdot y_{forest_i} \qquad \text{(Equation 4.2)}$$

where
TMDL = allowable load for impaired watershed (ton/yr)
Yn_{ref} = sediment loading threshold = forest normalized reference sediment load (3.3)
y_{forest_i} = all forested sediment load for segment *i* (ton /yr)
i = CBP P5 model segment
n = number of CBP P5 model segments in watershed

The Jones Falls watershed allowable sediment load is estimated using equation 4.2.

4.4 Critical Condition and Seasonality

EPA's regulations require TMDLs to take into account seasonality and critical conditions for stream flow, loading, and water quality parameters (CFR 2008b). The intent of this requirement is to ensure that the water quality of the waterbody is protected during times when it is most vulnerable. The biological monitoring data used to determine the reference watersheds integrates the stress effects over the course of time and thus inherently addresses critical conditions. Seasonality is captured in two components. First, it is implicitly included through the use of the biological monitoring data. Second, the MBSS dataset included benthic sampling in the spring and fish sampling in the summer.

4.5 TMDL Loading Caps

This section presents the Jones Falls watershed average annual sediment TMDL. This load is considered the maximum allowable long-term average annual load the watershed can sustain without causing any sediment related impacts to aquatic health.

The long-term average annual TMDL was calculated based on Equation 4.2 and set at a load 3.3 times the all forested condition. In order to attain the TMDL loading cap calculated for the watershed, reductions will be applied to the predominant controllable sources. If only these predominant (generally the largest) sources are controlled, water quality standards can be achieved in the most effective, efficient, and equitable manner. Urban land was identified as the most extensive predominant controllable source in the watershed.

Currently, MDE requires that large and medium MS4s retrofit 10% of existing urban land area where there is failing or no stormwater management every permit cycle (5 years). This level of restoration has been determined to be the current maximum feasible, regulated stormwater reduction scenario. Therefore, the reductions applied within this TMDL analysis are consistent with this 10% retrofit goal to existing urban land every 5 years with an estimated 65% TSS reduction efficiency from future stormwater BMPs (Claytor and Schueler 1997; Baldwin et al. 2007; Baish and Caliri 2009).

If the TMDL still is not achieved after applying the current maximum feasible urban stormwater reductions, then constant reductions will be applied to the remaining predominant controllable sources (i.e., significant contributors of sediment to the stream system), independent of jurisdiction. In addition to urban land, predominant sources typically include high till crops, low till crops, hay, pasture, and harvested forest, but additional sources might need to be controlled in order to ensure that the TMDL is attained.

The Jones Falls Baseline Load and TMDL are presented in Table 7.

Table 7: Jones Falls Baseline Load and TMDL

Baseline Load (ton/yr)	TMDL (ton/yr)	Total Reduction (%)
9,104.9	7,109.3	21.9

4.6 Load Allocations Between Point and Nonpoint Sources

Per EPA regulation, all TMDLs need to be presented as a sum of waste load allocations (WLAs) for point sources and load allocations (LAs) for nonpoint source loads generated within the assessment unit, as well as natural background, tributary, and adjacent segment loads (CFR 2008a). Consequently, the Jones Falls watershed TMDL allocations are presented in terms of WLAs (i.e., point source loads identified within the watershed) and LAs (i.e., the nonpoint source loads within the watershed). The State reserves the right to allocate the TMDL among different sources in any manner that is reasonably calculated to protect aquatic life from sediment related impacts.

As described in Section 4.5, reductions were only applied to the regulated urban stormwater sources. Furthermore, reductions were only applied to urban areas developed prior to 1985 (i.e., approximate areas with no stormwater management). This is consistent with MS4 permit requirements for retrofitting existing urban areas at a rate of 10% every 5 years. The reduction in sediment loads associated with retrofitting 10% of existing urban areas every 5 years, with an estimated 65% TSS reduction efficiency, represents the current maximum feasible reduction scenario from the urban land use within the watershed.

In this watershed, in addition to urban land, crop and pasture were identified as the predominant controllable sources; however, no reductions were applied to these sources, since the TMDL is achieved when the current maximum feasible reductions are applied to the regulated urban stormwater sources in the watershed. Forest is the only non-controllable source, as it represents the most natural condition in the watershed, and no reductions were applied to permitted process water sources because at 0.03% of the total load, such controls would produce no discernable water quality benefit.

Table 8 summarizes the TMDL results for the Jones Falls watershed, derived by applying the current maximum feasible reductions to the applicable urban sediment sources. The reductions associated with the current maximum feasible scenario result in sediment

loading reductions greater than those needed to achieve the TMDL. Thus, the TMDL results in Table 8 represent a feasible reduction scenario from the applicable urban sediment sources, determined using the current maximum feasible reduction scenario as a basis. The TMDL results in an overall reduction of 22% for the Jones Falls watershed. For more detailed information regarding the Jones Falls Watershed TMDL nonpoint source LA, please see the technical memorandum to this document entitled "*Significant Sediment Nonpoint Sources in the Jones Falls Watershed*".

Table 8: Jones Falls TMDL Reductions by Source Category

Baseline Load Source Categories		**Baseline Load** (ton/yr)	**TMDL Components**	**TMDL** (ton/yr)	**Reduction** (%)
Nonpoint Source		1,022.0	**LA**	1,022.0	0.0
Point Source	Urban	8,080.5	**WLA**	6,084.9	24.7
	Permits	2.4		2.4	0.0
TOTAL		**9,104.9**		**7,109.3**	**21.9**

The WLA of the Jones Falls watershed is allocated to two permitted source categories, Process Water WLA and Stormwater WLA. The categories are described below.

Process Water WLA

Process Water permits with specific TSS limits and corresponding flow information are assigned to the WLA. In this case, detailed information is available to accurately estimate the WLA. If specific TSS limits are not explicitly stated in the process water permit, then TSS loads are expected to be *de minimis*. If loads are *de minimis*, then they pose little or no risk to the aquatic environment and are not a significant source.

Process Water permits with specific TSS limits include:

- Individual municipal facilities
- General mineral mining facilities

There are 2 process water sources with explicit TSS limits, which include 1 municipal source and 1 mineral mine. The total estimated TSS load from all of the process water sources is based on current permit limits and is equal to 2.4 ton/yr. As mentioned above, no reductions were applied to this source because at 0.03% of the total load, such controls would produce no discernable water quality benefit. For a detailed list of the 2 process water sources including information on their permit limits, please see Appendix B. For information regarding the allocations to individual process water point sources, please see the technical memoranda to this document entitled "*Significant Sediment Point Sources in the Jones Falls Watershed*".

Stormwater WLA

Per EPA requirements, "stormwater discharges that are regulated under Phase I or Phase II of the NPDES stormwater program are point sources that must be included in the WLA

portion of a TMDL" (US EPA 2002). Phase I and II permits can include the following types of discharges:

- Small, medium, and large MS4s – these can be owned by local jurisdictions, municipalities, and state and federal entities (e.g., departments of transportation, hospitals, military bases),
- Industrial facilities permitted for stormwater discharges, and
- Small and large construction sites.

EPA recognizes that available data and information are usually not detailed enough to determine WLAs for NPDES regulated stormwater discharges on an outfall-specific basis (US EPA 2002). Therefore, NPDES regulated stormwater loads within the Jones Falls watershed will be expressed as a single NPDES stormwater WLA. Upon approval of the TMDL, "NPDES-regulated municipal stormwater and small construction storm water discharges effluent limits should be expressed as BMPs or other similar requirements, rather than as numeric effluent limits" (US EPA 2002).

The Jones Falls NPDES stormwater WLA is based on reductions applied to the sediment load from the urban land use of the watershed derived from the current maximum feasible stormwater reduction scenario and may include legacy or other sediment sources. Some of these sources may also be subject to controls from other management programs. The Jones Falls NPDES stormwater WLA requires an overall reduction of 24.7% (see Table 8).

As stormwater assessment and/or other program monitoring efforts result in a more refined source assessment, MDE reserves the right to revise the current NPDES stormwater WLA provided the revisions are reasonably calculated to protect aquatic life from sediment related impacts.

For more information on the methods used to calculate the baseline urban sediment load, see Section 2.2.2. For a detailed list of all of the NPDES regulated stormwater discharges within the watershed, please see Appendix B, and for information regarding the NPDES stormwater WLA distribution amongst these discharges, please see the technical memorandum to this document entitled "*Significant Sediment Point Sources in the Jones Falls Watershed*".

4.7 Margin of Safety

All TMDLs must include a margin of safety to account for any lack of knowledge and uncertainty concerning the relationship between loads and water quality (CFR 2008b). It is proposed that the estimated variability around the reference watershed group used in this analysis already accounts for such uncertainty. Analysis of the reference group *forest normalized sediment loads* indicates that approximately 75% of the reference watersheds have a value of less than 4.2. Also, 50% of the reference watersheds have a value less than 3.3. Based on this analysis the *forest normalized reference sediment load* (also referred to as the *sediment loading threshold*) was set at the median value of 3.3 (Currey et al. 2006). This is considered an environmentally conservative estimate, since 50% of

the reference watersheds have a load above this value, which when compared to the 75% value, results in an implicit margin of safety of approximately 18%.

4.8 Summary of Total Maximum Daily Loads

The average annual Jones Falls watershed TMDL is summarized in Table 9. The TMDL is the sum of the LA, NPDES Stormwater WLA, Process Water WLA, and MOS. The Maximum Daily Load (MDL) is summarized in Table 10 (See Appendix C for more details).

Table 9: Jones Falls Watershed Average Annual TMDL of Sediment/TSS (ton/yr)

TMDL (ton/yr)	=	LA_{JF}	+	NPDES Stormwater WLA_{JF}	+	Process Water WLA_{JF}	+	MOS
7,109.3	=	1,022.0	+	6,084.9	+	2.4	+	Implicit

Table 10: Jones Falls Maximum Daily Loads of Sediment/TSS (ton/day)

MDL (ton/day)	=	LA_{JF}	+	NPDES Stormwater WLA_{JF}	+	Process Water WLA_{JF}	+	MOS
284.3	=	40.9	+	243.4	+	0.02	+	Implicit

5.0 ASSURANCE OF IMPLEMENTATION

This section provides the basis for reasonable assurances that the sediment TMDL will be achieved and maintained. Section 303(d) of the Clean Water Act and current EPA regulations require reasonable assurance that the TMDL load and wasteload allocations can and will be implemented (CFR 2008b). Maryland has several well-established programs to draw upon, including the Water Quality Improvement Act of 1998 (WQIA) and the Federal Nonpoint Source Management Program (§ 319 of the Clean Water Act).

Potential funding sources available for local governments for implementation include the Buffer Incentive Program (BIP), the State Water Quality Revolving Loan Fund, and the Stormwater Pollution Cost Share Program. Details of these programs and additional funding sources can be found at http://www.dnr.state.md.us/bay/services/summaries.html.

Potential BMPs for reducing sediment loads and resulting impacts can be grouped into three general categories. The first is directed toward agricultural lands, the second towards urban (developed) land, and the third applies to all land uses. Since urban land was identified as the most extensive primary, predominant controllable source of sediment within the watershed (i.e., 89% of the total Jones Falls Baseline Sediment Load), and based on current maximum feasible reductions to regulated urban stormwater, the entirety of the required sediment reductions within the Jones Falls watershed are attributed to urban (developed) land use. The various BMPs applicable to reducing urban sediment loads are discussed below.

Sediment from urban areas can be reduced by stormwater retrofits, impervious surface reduction, and stream restoration. Stormwater retrofits include modification of existing stormwater structural practices to address both water quality and flow control. The majority of the sediment reductions required from the urban areas within the Jones Falls watershed are attributed to streambank erosion (see section 2.2.1). Therefore, flow controls must be installed to reduce sheer stress and limit bank erosion in order to address this portion of the urban sediment load. Additionally, impervious surface reduction results in a change in hydrology that could also reduce streambank erosion. In terms of upland urban sediment loads, stormwater retrofit reductions range from as low as 10% for dry detention to approximately 80% for wet ponds, wetlands, infiltration practices, and filtering practices (US EPA 2003). It is anticipated that the implementation of the TMDL will include the array of urban BMPs and practices outlined above. Implementation is expected to occur primarily via the MS4 permitting process for medium and large municipalities, which requires that these jurisdictions retrofit 10% of the existing urban land area every permit cycle, or 5 years.

It has been estimated that the average TSS removal efficiencies for BMPs installed between the years of 1985-2002 and post 2002, which are reflective of the stormwater management regulations in place during these time periods, is 50% and 80%, respectively (Claytor and Schueler 1997; Baldwin et al. 2007; Baish and Caliri 2009). Based on these average TSS reduction efficiencies, BMP specific reduction efficiencies as estimated by CBP, and best professional judgment, MDE estimates that future stormwater retrofits,

which are expected to be implemented as part of the 10% retrofit goal to existing urban land every 5 years, will have approximately a 65% reduction efficiency for TSS, which is subject to change over time. Additionally, any new development in the watershed will be subject to the Stormwater Management Act of 2007 and will be required to use environmental site design (ESD) to the maximum extent practicable.

All non-forested land uses can benefit from improved riparian buffer systems. A riparian buffer reduces the effects of upland sediment sources through trapping and filtering. Riparian buffer efficiencies vary depending on type (grass or forested), land use (urban or agriculture), and physiographic region. The CBP estimates riparian buffer sediment reduction efficiencies in the Jones Falls region to be approximately 50% (US EPA 2006).

In summary, through the use of the aforementioned funding mechanisms and best management practices, there is reasonable assurance that this TMDL can be implemented.

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APPENDIX A – Watershed Characterization Data

Table A-1: Reference Watersheds

MD 8-digit Name	MD 8-digit	Percent stream mile degraded (%)[1,2]	Forest Normalized Sediment Load[3]
Deer Creek	02120202	11	3.9
Broad Creek	02120205	12	4.5
Little Gunpowder Falls	02130804	15	3.3
Prettyboy Reservoir	02130806	16	3.7
Middle Patuxent River	02131106	20	3.2
Brighton Dam	02131108	11	4.2
Sideling Creek	02140510	20	1.9
Fifteen Mile Creek	02140511	4	1.6
Savage River	02141006	7	2.5
Median			**3.3**
75th			**4.2**

Notes: [1]Percent stream miles degraded within an 8-digit watershed is based on the percentage of impaired MBSS stations within the watershed (MDE 2008).
[2]The percent stream miles degraded threshold to determine if an 8-digit watershed is impaired for impacts to biological communities is based on a comparison to reference conditions (MDE 2008).
[3]Forest normalized sediment loads based on Maryland watershed area only (consistent with MBSS random monitoring data).

APPENDIX B – MDE Permit Information

Table B-1: Permit Summary

Permit #	NPDES	Facility	County	City	Type	TMDL
04DP2921	MD0066001	STEVENSON COLLEGE WWTP	BALTIMORE COUNTY	STEVENSON	WMA2	Process Water WLA
00MM0976	MDG490976	ARUNDEL CORPORATION - GREENSPRING QUARRY	BALTIMORE COUNTY	PIKESVILLE	WMA5	Process Water WLA
02SW0105		HEDWIN CORPORATION - ROLAND HEIGHTS	BALTIMORE CITY	BALTIMORE	WMA5SW	Stormwater WLA
02SW0255		WOODBERRY QUARRY LANDFILL	BALTIMORE CITY	BALTIMORE	WMA5SW	Stormwater WLA
02SW0599		PEPSI BOTTLING GROUP, LLC	BALTIMORE CITY	BALTIMORE	WMA5SW	Stormwater WLA
02SW0702		BALTIMORE CITY DPW - NORTHEASTERN SUBSTATION	BALTIMORE CITY	BALTIMORE	WMA5SW	Stormwater WLA
02SW0704		BALTIMORE CITY DPW - MIDDLETOWN FUELING STATION	BALTIMORE CITY	BALTIMORE	WMA5SW	Stormwater WLA
02SW0707		BALTIMORE CITY DPW - FALLSWAY SUBSTATION	BALTIMORE CITY	BALTIMORE	WMA5SW	Stormwater WLA
02SW0747		U.S. POSTAL SERVICE - OLIVER STREET VMF	BALTIMORE CITY	BALTIMORE	WMA5SW	Stormwater WLA
02SW0861		HOLLINS ORGANIC PRODUCTS, INC.	BALTIMORE CITY	BALTIMORE	WMA5SW	Stormwater WLA
02SW1056		VEOLIA TRANSPORTATION - BALTIMORE	BALTIMORE CITY	BALTIMORE	WMA5SW	Stormwater WLA
02SW1156		NORFOLK RAILWAY CORPORATION - FLEXI-FLO TERMINAL	BALTIMORE CITY	BALTIMORE	WMA5SW	Stormwater WLA
02SW1211		COLD SPRING LANDFILL	BALTIMORE CITY	BALTIMORE	WMA5SW	Stormwater WLA
02SW1296		COCKEY'S ENTERPRISES, INC.	BALTIMORE COUNTY	STEVENSON	WMA5SW	Stormwater WLA
02SW1675		MTA - NORTH AVENUE LIGHTRAIL FACILITY	BALTIMORE CITY	BALTIMORE	WMA5SW	Stormwater WLA
02SW1676		MTA - KIRK AVENUE BUS DIVISION	BALTIMORE CITY	BALTIMORE	WMA5SW	Stormwater WLA
02SW1751		SHA - BROOKLANDVILLE SHOP	BALTIMORE COUNTY	BROOKLANDVILLE	WMA5SW	Stormwater WLA

Permit #	NPDES	Facility	County	City	Type	TMDL
02SW1810		POTTS & CALLAHAN, INC. - REPAIR SHOP	BALTIMORE CITY	BALTIMORE	WMA5SW	Stormwater WLA
02SW3029		PALL FILTRATION & SEPARATIONS GROUP - GREENSPRING	BALTIMORE COUNTY	TIMONIUM	WMA5SW	Stormwater WLA
05DP3317	MD0068314	BALTIMORE COUNTY MS4	BALTIMORE COUTNY	COUNTY-WIDE	WMA6	Stormwater WLA
99DP3315	MD0068292	BALTIMORE CITY MS4	BALTIMORE CITY	CITY-WIDE	WMA6	Stormwater WLA
99DP3313	MD0068276	STATE HIGHWAY ADMINSTRATION MS4	ALL PHASE I	STATE-WIDE	WMA6	Stormwater WLA
		MDE GENERAL PERMIT TO CONSTRUCT	ALL	ALL		Stormwater WLA

Notes: [1]TMDL column identifies how the permit was considered in the TMDL allocation.
[2]WWTP = Wastewater Treatment Plant

Table B-2: Individual Municipal Permit Data

Facility name	NPDES #	MDE Permit #	Flow (MGD[1])	Permit Avg. Monthly Conc. (mg/l[2])	Permit Avg. Weekly Conc. (mg/l)
STEVENSON UNIVERSITY WWTP	04DP2921	MD0066001	0.05	30	45

Notes: [1] MGD = Millions of gallons per day
[2] mg/l = Milligram per liter

Table B-3: General Mine Permit Data

Facility name	NPDES #	MDE Permit #	Flow (MGD)	Permit Avg Quarterly Conc. (mg/l)	Permit Daily Max Conc. (mg/l)
ARUNDEL CORPORATION - GREENSPRING QUARRY	00MM0976	MDG490976	0.001	30	60

Table B-4: Stormwater Permits[1]

Permit #	Facility	NPDES Group
02SW0105	HEDWIN CORPORATION - ROLAND HEIGHTS	Phase I
02SW0255	WOODBERRY QUARRY LANDFILL	Phase I
02SW0599	PEPSI BOTTLING GROUP, LLC	Phase I
02SW0702	BALTIMORE CITY DPW - NORTHEASTERN SUBSTATION	Phase I
02SW0704	BALTIMORE CITY DPW - MIDDLETOWN FUELING STATION	Phase I
02SW0707	BALTIMORE CITY DPW - FALLSWAY SUBSTATION	Phase I
02SW0747	U.S. POSTAL SERVICE - OLIVER STREET VMF	Phase I
02SW0861	HOLLINS ORGANIC PRODUCTS, INC.	Phase I
02SW1056	VEOLIA TRANSPORTATION - BALTIMORE	Phase I
02SW1156	NORFOLK RAILWAY CORPORATION - FLEXI-FLO TERMINAL	Phase I
02SW1211	COLD SPRING LANDFILL	Phase I
02SW1296	COCKEY'S ENTERPRISES, INC.	Phase I
02SW1675	MTA - NORTH AVENUE LIGHTRAIL FACILITY	Phase I
02SW1676	MTA - KIRK AVENUE BUS DIVISION	Phase I
02SW1751	SHA - BROOKLANDVILLE SHOP	Phase I
02SW1810	POTTS & CALLAHAN, INC. - REPAIR SHOP	Phase I
02SW3029	PALL FILTRATION & SEPARATIONS GROUP - GREENSPRING	Phase I
05DP3317	BALTIMORE COUNTY MS4	Phase I
99DP3315	BALTIMORE CITY MS4	Phase I
99DP3313	STATE HIGHWAY ADMINSTRATION MS4	Phase I
	MDE GENERAL PERMIT TO CONSTRUCT	Phase I/II

Notes: [1] Although not listed in this table, individual permits from Tables B-2 and B-3 may incorporate stormwater requirements and are accounted for within the NPDES stormwater WLA (specifically the "Other" Regulated Stormwater allocation in the Technical Memoranda *Significant Sediment Point Sources in the Jones Falls Watershed* accompanying this TMDL report) as well additional Phase II permitted MS4s, such as military bases, hospitals, etc.

APPENDIX C – Technical Approach Used to Generate Maximum Daily Loads

Summary

This appendix documents the technical approach used to define maximum daily loads of sediment consistent with the average annual TMDL in the Jones Falls watershed, which is considered the maximum allowable load the watershed can sustain without causing any sediment related impacts to aquatic health. The approach builds upon the modeling analysis that was conducted to determine the sediment loadings and can be summarized as follows.

- The approach defines maximum daily loads for each of the source categories.
- The approach builds upon the TMDL modeling analysis that was conducted to ensure that average annual loading targets do not cause any sediment related impacts to aquatic health.
- The approach converts daily time-series loadings into TMDL values in a manner that is consistent with available EPA guidance on generating daily loads for TMDLs.
- The approach considers a daily load level of a resolution based on the specific data that exists for each source category.

Introduction

This appendix documents the development and application of the approach used to define maximum daily load values. It is divided into sections discussing:

- Basis for approach
- Options considered
- Selected approach
- Results of approach

Basis for approach

The overall approach for the development of daily loads was based upon the following factors:

- **Average Annual TMDL:** The basis of the average annual sediment TMDL is that cumulative high sediment loading rates have negative impacts on the biological community. Thus, the average annual sediment load was calculated so as to not cause any sediment related impacts to aquatic health.
- **CBP P5 Watershed Model Sediment Loads:** There are two spatial calibration points for sediment within the CBP P5 watershed model framework. First, EOS loads are calibrated to long term EOS target loads. These target loads are the loads used to determine an average annual TMDL. Furthermore, the target loads were used in the TMDL because, as calibration targets, they are expected to

remain relatively unchanged during the final calibration stages of the CBP P5 model, and therefore will be the most consistent with the final CBP P5 watershed model sediment loading estimates. Currently, the CBP P5 model river segments are being calibrated to daily monitoring information for watersheds with a flow greater that 100 cfs, or an approximate area of 100 square miles.

- **Draft EPA guidance document entitled "Developing Daily Loads for Load-based TMDLs":** This guidance document provides options for defining maximum daily loads when using TMDL approaches that generate daily output.

The rationale for developing TMDLs expressed as *daily* loads was to accept the existing average annual TMDL, but then develop a method for converting this number to a maximum *daily* load – in a manner consistent with EPA guidance and available information.

Options considered

The draft EPA guidance document for developing daily loads does not specify a single approach that must be adhered to, but rather it contains a range of acceptable options. The selection of a specific method for translating a time-series of allowable loads into the expression of a TMDL requires decisions regarding both the level of resolution (e.g., single daily load for all conditions vs. loads that vary with environmental conditions) and level of probability associated with the TMDL.

This section describes the range of options that were considered when developing methods to calculate Jones Falls Maximum Daily Loads.

Level of Resolution

The level of resolution pertains to the amount of detail used in specifying the maximum daily load. The draft EPA guidance document on daily loads provides three categories of options for level of resolution, all of which are potentially applicable for the Jones Falls watershed:

1. **Representative daily load:** In this option, a single daily load (or multiple representative daily loads) is specified that covers all time periods and environmental conditions.
2. **Flow-variable daily load:** This option allows the maximum daily load to vary based upon the observed flow condition.
3. **Temporally-variable daily load:** This option allows the maximum daily load to vary based upon seasons or times of varying source or water body behavior.

Probability Level

All TMDLs have some probability of being exceeded, with the specific probability being either explicitly specified or implicitly assumed. This level of probability directly or indirectly reflects two separate phenomena:

1. Water quality criteria consist of components describing acceptable magnitude, duration, and frequency. The frequency component addresses how often conditions can allowably surpass the combined magnitude and duration components.
2. Pollutant loads, especially from wet weather sources, typically exhibit a large degree of variability over time. It is rarely practical to specify a "never to be exceeded value" for a daily load, as essentially any loading value has some finite probability of being exceeded.

The draft daily load guidance document states that the probability component of the maximum daily load should be "based on a representative statistical measure" that is dependent upon the specific TMDL and the best professional judgment of the developers. This statistical measure represents how often the maximum daily load is expected/allowed to be exceeded. The primary options for selecting this level of protection would be:

1. **The maximum daily load reflects some central tendency:** In this option, the maximum daily load is based upon the mean or median value of the range of loads expected to occur. The variability in the actual loads is not addressed.
2. **The maximum daily load reflects a level of protection implicitly provided by the selection of some "critical" period**: In this option, the maximum daily load is based upon the allowable load that is predicted to occur during some critical period examined during the analysis. The developer does not explicitly specify the probability of occurrence.
3. **The maximum daily load is a value that will be exceeded with a pre-defined probability:** In this option, a "reasonable" upper bound percentile is selected for the maximum daily load based upon a characterization of the variability of daily loads. For example, selection of the 95th percentile value would result in a maximum daily load that would be exceeded 5% of the time.

Selected Approach

The approach selected for defining a Jones Falls Maximum Daily Load was based upon the specific data that exists for each source category. The approach consists of unique methods for each of the following categories of sources:

- Approach for Nonpoint Sources and Stormwater Point Sources within the Jones Falls watershed
- Approach for Process Water Point Sources within the Jones Falls watershed

<u>Approach for Nonpoint Sources and Stormwater Point Sources within the Jones Falls watershed</u>

The level of resolution selected for the Jones Falls Maximum Daily Load was a representative daily load, expressed as a single daily load for each loading source. This

approach was chosen based upon the specific data that exists for nonpoint sources and stormwater point sources within the Jones Falls watershed. Currently, the best available data is the CBP P5 model daily time series calibrated to long-term average annual loads (per landuse). The CBP reach simulation results are calibrated to daily monitoring information for watershed segments with a flow typically greater that 100 cfs, but they have not been through appropriate peer review. Therefore, it was concluded that it would not be appropriate to apply the absolute values of the reach simulation model results to the TMDL, and the annual loads were used instead. However, it was assumed that the distribution of the daily values was correct, in order to calculate a normalized statistical parameter to estimate the maximum daily loads.

The maximum daily load was estimated based on three factors: a specified probability level, the average annual sediment TMDL, and the coefficient of variation (CV) of the CBP P5 Jones Falls reach simulation daily loads. The probability level (or exceedance frequency) is based upon guidance from EPA (US EPA 1991) where examples suggest that when converting from a long-term average to a daily value, the z-score corresponding to the 99th percentile of the log-normal probability distribution should be used. The average annual sediment TMDL is estimated from the CBP P5 EOS target loads. The calculation of the CV is described below.

The CBP P5 Jones Falls reach simulation consisted of a daily time series beginning in 1985 and extending to the year 2005. The CV was estimated by first converting the daily sediment load values to a log distribution and then verifying that the results approximated the normal distribution (see Figure C-1). Next, the CV was calculated using the arithmetic mean and standard deviation results from the log transformation. The log-transformed values were used to reduce the possible influence of outliers. The resulting CV of 7.2 was calculated using the following equation:

$$CV = \frac{\beta}{\alpha} \qquad \text{(Equation C.1)}$$

where:
CV = coefficient of variation
$\beta = \alpha\sqrt{e^{\sigma^2} - 1}$
$\alpha = e^{(\mu + 0.5*\sigma^2)}$
α = mean (arithmetic)
β = standard deviation (arithmetic)
μ = mean of logarithms
σ =standard deviation of logarithms

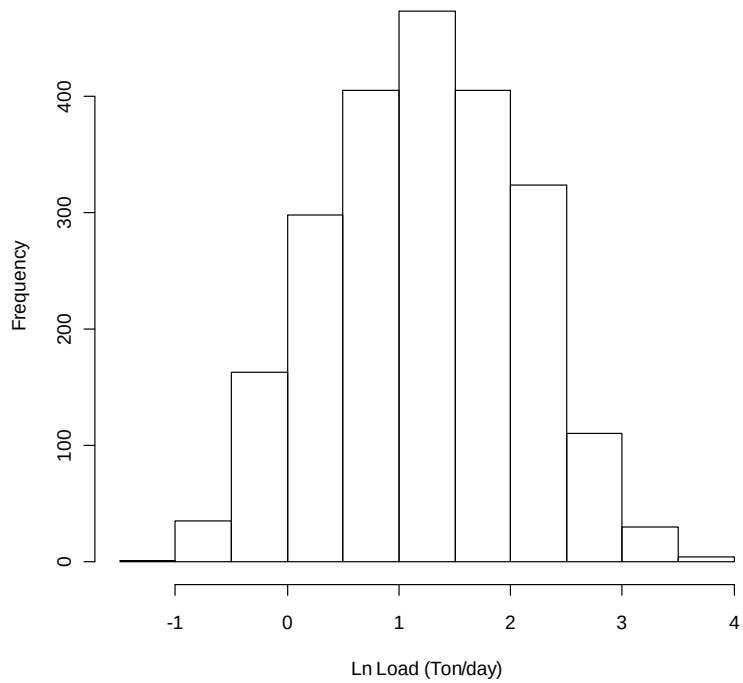

Figure C-1: Histogram of CBP River Segment Daily Simulation Results for the Jones Falls Watershed

The maximum "daily" load for each contributing source is estimated as the long-term average annual load multiplied by a factor that accounts for expected variability of daily loading values. The equation is as follows:

$$MDL = LTA * e^{(z\sigma - 0.5\sigma^2)} \qquad \text{(Equation C.2)}$$

where:
MDL = Maximum daily load
LTA = Long term average (average annual load)
Z = z-score associated with target probability level
$\sigma = \ln(CV^2+1)$
CV = Coefficient of variation based on arithmetic mean and standard deviation

Using a z-score associated with the 99th percent probability, a CV of 7.2, and consistent units, the resulting dimensionless conversion factor from long term average annual loads to a maximum daily load is 14.14. The average annual Jones Falls TMDL of sediment/TSS is reported in ton/year, and the conversion from ton/year to a maximum daily load in ton/day is 0.04 (e.g. 14.14/365)

Approach for Process Water Point Sources within the Jones Falls watershed

The TMDL also considers contributions from other point sources (i.e., sources other than stormwater point sources) in the watershed that have NPDES permits with sediment limits. As these sources are generally minor contributors to the overall sediment load, the TMDL analysis that defined the average annual TMDL did not propose any reductions for these sources and held each of them constant at their existing technology-based NPDES permit monthly (or daily if monthly was not specified) limit for the entire year.

The approach used to determine maximum daily loads for these sources was dependent upon whether a maximum daily load was specified within the permit. If a maximum daily limit was specified, then the reported average flow was multiplied by the daily maximum limit to obtain a maximum daily load. If a maximum daily limit was not specified, the maximum daily loads were calculated based on the guidance provided in the Technical Support Document (TSD) for Water Quality-based Toxics Control (US EPA 1991). The long-term average annual TMDL was converted to maximum daily limits using Table 5-2 of the TSD assuming a coefficient of variation of 0.6 and a 99th percentile probability. This results in a dimensionless multiplication factor of 3.11. The average annual Jones Falls TMDL of sediment/TSS is reported in ton/yr, and the conversion from ton/yr to a maximum daily load in ton/day is 0.0085 (e.g. 3.11/365)

Results of approach

This section lists the results of the selected approach to define the Jones Falls Maximum Daily Loads.

- Calculation Approach for Nonpoint Sources and Stormwater Point Sources within the Jones Falls watershed

LA_{JF} (Ton/day) = Average Annual TMDL LA_{JF} (ton/yr) * .04

Stormwater WLA_{JF} (Ton/day) = Average Annual TMDL Stormwater WLA_{JF} (ton/yr) * .04

- Calculation Approach for Process Water Point Sources within the Jones Falls watershed
  - For permits with a daily maximum limit:

Process Water WLA_{JF} (ton/day) = Permit flow (mgd) * Daily maximum permit limit(mg/l) * 0.0042

  - For permits without a daily maximum limit:

Process Water WLA_{JF} (Ton/day) = Average Annual TMDL WLA_{JF} Other (ton/yr)* 0.0085

Table C-1: Jones Falls Maximum Daily Loads of Sediment/TSS (ton/day)

MDL (ton/day)	=	LA_{JF}	+	NPDES Stormwater WLA_{JF}	+	Process Water WLA_{JF}	+	MOS
284.3	=	40.9	+	243.4	+	0.02	+	Implicit